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COST EFFECTIVENESS STUDY OF WEATHER PROTECTION FOR
SHIPBUILDING OPERATIONS
VOLUME II

TODD SHIPYARDS CORPORATION

**PREPARED FOR
MARITIME ADMINISTRATION**

APRIL 1974

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This report contains data on how weather factors impact adversely on the shipbuilding process. It is comprehensive, not intended for the casual reader, and useful for the purpose of quantifying losses due to weather. It can serve management to determine how much money should be invested in weather protection devices.

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APPENDIX A

THE PRODUCTIVITY MODEL

DESCRIPTION OF THE PRODUCTIVITY MODEL

After a critical review of our notes from the shipyard interviews, the questionnaires, other data, and reports, we constructed Table A-1 which represents the productivity for the various crafts under selected weather categories and working locations. The effect of temperature on productivity in Table A-1 is based on Figure A-1, which is adapted from Figure C-1, Appendix C. Productivity values for some crafts varied from the norm according to the relative adverse effect of the weather category on that craft as indicated by the nature of the work. The values shown in Table A-1 assume no special Weather protection aside from normal clothing to fit the conditions. In-ship workers are assumed to be protected from wind and direct precipitation by ship structures. A special algorithm (Exhibit A) is applied to cover pass-out conditions for precipitation (or for relative humidity for painters and blasters). Exhibits B, C, and D provide explanations of our assumptions, special conditions, and penalties used to develop Table A-1.

Effective temperature (outside) is defined as the dry bulb temperature minus the wind speed in mph. This is a reasonable approximation of the wind chill factor over normal temperature ranges. We applied the wind chill correction to dry bulb temperatures below 80°F. Above 80°F and within the ship, the effective temperature is the dry bulb temperature.

This model is applied to combinations of weather conditions with temperature by multiplying the probabilities of each other weather occurrence with its associated productivity. Under a set of combined weather conditions, the productivity in each temperature range is the product of these separate productivities. The average annual productivity is the total of the separate productivities within each temperature range. With this model, we compute the average annual productivity for each craft and shift and for the entire standard shipyard for each shipyard location. The sample calculation which follows describes this procedure. A listing of the computer program to perform these calculations is given in

TABLE A-1. Estimated Productivity (%) of Shipyard Workers Under Various Weather Conditions

<u>CRAFTS</u>	<u>EFFECTIVE TEMPERATURE (°F)</u>								<u>WIND (MPH)</u>			<u>PRECIPITATION (INCHES)</u>				
	<u><5</u>	<u>5-19</u>	<u>20-29</u>	<u>30-39</u>	<u>40-79</u>	<u>80-89</u>	<u>90-99</u>	<u>100+</u>	<u><12</u>	<u>13-24</u>	<u>25+</u>	<u>None</u>	<u>Trace</u>	<u>.01</u>	<u>.02-.09</u>	<u>.1+</u>
<u>OUTSIDE</u>																
Painters	30	56	75	92	100	84	48	15	100	70	0	100	*	0	0	0
Welders	25	51	70	92	100	79	48	15	100	80	10	100	100	80	0	0
Riggers	25	55	75	92	100	84	53	20	100	90	15	100	100	95	85	40
Fitters	25	51	70	92	100	84	53	20	100	90	20	100	100	95	85	40
Others	30	56	75	92	100	84	53	20	100	95	40	100	100	95	90	50
<u>IN SHIP (Effective Temperature = Dry Bulb Temperature)</u>																
Painters	0	0	0	70	100	79	48	15	100	100	80	100	*	*	*	*
Welders	30	56	75	100	100	74	43	10	100	100	80	100	100	100	95	80
Riggers	30	56	75	92	100	79	48	15	100	100	80	100	100	100	95	80
Fitters	30	56	75	92	100	79	40	15	100	100	80	100	100	100	95	80
Others	30	55	75	92	100	79	40	15	100	100	80	100	100	100	95	80

* Relative humidity is assumed to be the dominant factor affecting the productivity of painters and blasters

TABLE A-1 (continued). Estimated Productivity (%) of Shipyard Workers Under Various Weather Conditions

RELATIVE HUMIDITY			FOG	SHADE CLOUD COVER INDEX 9 a.m. - 6 p.m.	
CRAFTS	<u><90</u>	<u>90-100</u>	<u>Visibility</u> <u><1/16 Mile</u>	<u><3</u> <u>Temp.</u> <u><80° F</u>	<u>8-10</u> <u>Temp.</u> <u><60° F</u>
<u>OUTSIDE</u>					
Painters	100	0	**	70	100
Welders	100	100	**	70	100
Riggers	100	100	50-Day	70	100
Fitters	100	100	30-Night	70	100
Others	100	100	50-Day	70	100
			30-Night	70	100
			**	70	100
<u>IN SHIP</u> (Effective Temperature = Dry Bulb Temperature)					
Painters	100	0	Same as	95	100
Welders	100	100	for	95	100
Riggers	100	100	outside	95	100
Fitters	100	100	crafts	95	100
Others	100	100	"	95	100
			"	95	100

** Not Directly Applicable

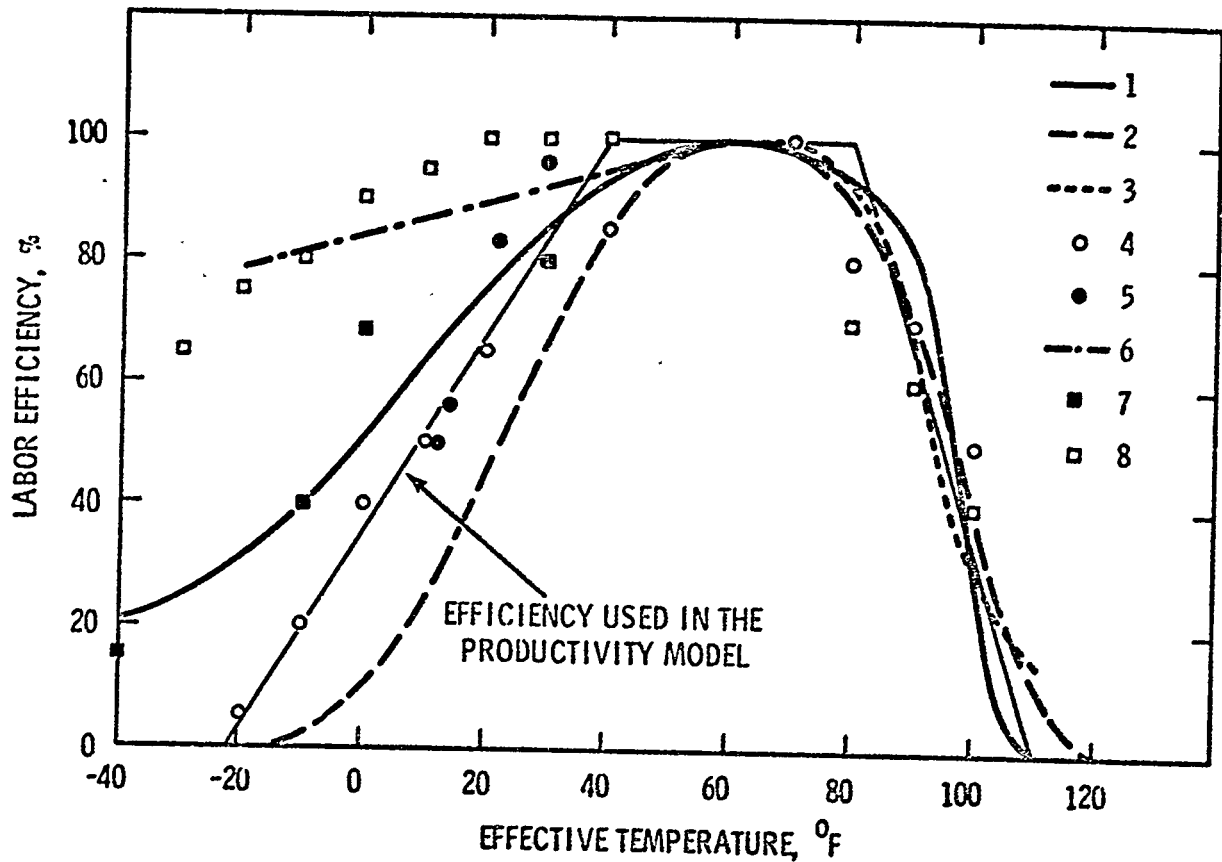


FIGURE A-1. Outdoor Worker Efficiency

LEGEND

1. Doyle, "Controlling Climate Effects", Tool Engr., 1955 (efficiency curve prepared under condition of little or no wind).
2. General Dynamics, Quincy (DX Study).
3. ASHVE Guide and Data Book (men at work 90,000 ft-lb of work per hour).
4. Constructor, May 1972 (welders, pipefitters, carpenters, electricians).
5. Unidentified shipyard estimate (converted from equivalent temperature to effective temperature).
6. Bechtel construction project in Canada (winter) - (converted from wind chill temperature and corrected to 100% efficiency at 60°F).
7. ASHVE Guide and Data Book (Armstrong's data for line-maintenance job).
8. Constructor, May 1972 (laborers, ironworkers, operating engineers).

Appendix L. Improvements in the average productivity for the entire shipyard provide the basis for assessing the cost-effectiveness of various weather protective facilities.

Sample Calculation

Assume: A welder is working outside on day shift in 30 to 39°F effective temperature, (already corrected for the wind chill effect). The frequency of wind at this shipyard is 80% less than 12 mph, 15% between 13 to 24 mph, and 5% above 25mph. The frequency of precipitation is 85% none or trace, 10% at 0.01 in./hr, 3% from 0.02 to 0.09 in./hr, and 2% at 0.1+ in./hr. The welders average productivity in wind alone would be, using these frequencies and the productivity values in Table A-1:

$$0.80 \times 1.00 + 0.15 \times 0.80 + 0.5 \times 0. = 0.92 \text{ Or } 92\%$$

The welders average productivity affected by precipitation alone would be

$$0.85 \times 1.00 + 0.10 \times 0.80 + 0.03 \times 0. + 0.2 \times 0. = 0.93 \text{ Or } 93\%$$

The welders average productivity for the 30 to 39°F effective temperature range would be the product of the productivities for temperature, wind, and precipitation, or

$$0.92 \times 0.92 \times 0.93 = 0.7870 \text{ Or } 79\%$$

If the 30 to 39°F effective temperature occurred 10% of the time for the shipyard location, the average annual outside productivity of welders in this temperature range would be 0.10×0.79 or 0.079. The total annual productivity would be the sum of the productivities for each effective temperature category. This type of calculation is repeated for each shift, each work location, and each craft.

The total shipyard productivity is the sum of craft, shift, and location productivities weighted by the number of craftsmen involved. The total shipyard productivity (when subtracted from unity and multiplied by the annual hours worked) indicates the total manhours of productivity lost because of adverse weather.

Since fog is not assumed to affect welders and since shade is assumed to be effective only at temperatures above 80°F, these conditions were not included in this calculation. Fog and shade, when included, are treated similarly to wind and precipitation.

ABSENTEEISM AND TURNOVER

Although the shipyards attributed some absenteeism and turnover to the weather, these were not believed to be major cost factors. Comments ran from "less than 5% of the absenteeism is caused by weather" to "its just as well they do not show up in bad weather, we would have to send them back home anyway."

On turnover, it was felt by some that poor working conditions caused by bad weather led employees to take other work when available. One shipyard foreman remarked that inside work was preferred by his crew even in good weather.

Since it was not possible to establish the rate or cost of either absenteeism or turnover to weather, these factors were omitted from our model.

An Assessment of Potential Bias in the Model

Our model is intended to provide a simplified approximation of the real situation. Since the real situation is too complex and too little understood to permit an economical exhaustive analysis, several simplifying assumptions were made and several factors were omitted from the model. These assumptions and omitted factors were examined in order to estimate, at least qualitatively their overall affect on our reported results. These factors are listed below according to whether they would tend to increase or decrease the benefits resulting from increased weather protection in the shipyards. On balance, we believe that the tendency toward increased benefits would far outweigh the tendency towards decreased benefits, and therefore, our results probably understated the potential benefits of increased weather protection.

Reasons Why Benefits May Exceed Those Calculated

1. We purposely tried to avoid overestimating productivity losses.
2. We did not include costs attributable to absenteeism and turnover.
3. He did not include potential benefits that might result from the ability to install more automated equipment through covering.
4. We did not include benefits from improved lighting.
5. He did not include benefits resulting from improved accident experience and the reduced potential for work stoppage for safety reasons under adverse conditions.
6. We did not include savings immaterial losses.
7. We did not include potential benefits from reduced maintenance on equipment, and lower capital costs of equipment purchased for inside use which does not have to be weathertight, hence, costs less, and is usually less expensive to install than outside in the weather.
8. We did not include losses resulting from extreme or extended adverse weather conditions. These would tend to be ameliorated with better weather protection.
9. The impact of snow and snow cover on lost production and time spent searching for and/or reproducing material lost in the snow was not included.
10. The savings in eliminating existing space heating and cooling costs were not included.
11. Higher and more consistent quality may result.
12. Smaller structures might be more cost-effective than a complete covering of an area, since more workers may be covered per unit area.
13. Hater and snow removal costs were not included.

Reasons Why Benefits May Be Less Than Those Calculated

1. Real conditions may not resemble the model shipyard.
 - a) worker distribution may be different
 - b) the work load may be too variable
 - c) fixed and variable expenses may be different

2. *Covering may impede work more than estimated.*
3. *Workers may acclimatize to a greater extent than assumed; thus, productivity saving may be overstated.*
4. *Covering costs may be greater than estimated.*
5. *Other factors may have a much greater effect on productivity and overshadow the effects of weather.*
6. *Extreme weather tends to occur less frequently than more moderate weather. Within each weather class, weather occurrences tend to be biased toward the moderate. For instance, the temperature is more frequently between 35°F to 39°F than 30°F to 34°F. In estimating the productivity of a weather class at the midpoint, we may have introduced a slight bias toward lower productivity.*

The Effects of Weather on Productivity as Determined by the Model

After applying the productivity model to the weather conditions near each shipyard location, the results were analyzed to determine the average annual productivity, both outside and in-ship, for each craft and shipyard location (Table A-2). The results were also analyzed to determine the effect of providing protection against specific weather conditions (Tables A-3 through A-7). The factors in these tables show the estimated productivity gain for each outside craft at each shipyard location of providing each type of weather protection. For example, referring to Table A-3, providing wind protection at San Diego would increase the productivity of outside painters by 1.034 or 3.4% (1.034 - 1.000). Tables A-4 through A-7 show the relative productivity increases for the other outside crafts. These factors should be generally applicable to productivity calculations for other weather protective devices, as described in the next section.

APPLICATION OF PRODUCTIVITY MODEL TO A SPECIFIC SHIPYARD

The productivity model may be applied to a specific weather protection facility and shipyard through the use of the factors shown in Tables A-3 through A-7. These factors represent the potential productivity increase

TABLE A-2. Average Annual Productivity by Craft and Work Location

Location	Painters		Welders		Rigger		Fitters		Others	
	Outside	Inship	Outside	Inship	Outside	Inship	Outside	Inship	Outside	Inship
Baltimore	0.581	0.733	0.721	0.923	0.786	0.908	0.775	0.912	0.812	0.916
New Orleans	0.703	0.799	0.795	0.904	0.854	0.910	0.852	0.910	0.877	0.915
Portland, Oregon	0.706	0.802	0.805	0.967	0.875	0.953	0.869	0.955	0.895	0.960
Norfolk, VA	0.656	0.800	0.759	0.934	0.812	0.911	0.805	0.913	0.850	0.932
Portland, Maine	0.461	0.581	0.685	0.904	0.751	0.883	0.737	0.886	0.779	0.892
New York	0.562	0.748	0.705	0.948	0.777	0.929	0.766	0.932	0.811	0.937
Houston	0.620	0.772	0.732	0.887	0.800	0.894	0.798	0.895	0.833	0.899
Seattle	0.590	0.737	0.749	0.970	0.823	0.949	0.814	0.951	0.857	0.961
San Diego	0.930	0.963	0.956	0.989	0.970	0.986	0.970	0.986	0.980	0.991
Mobile	0.653	0.770	0.779	0.913	0.837	0.915	0.835	0.916	0.862	0.920
Boston	0.499	0.711	0.637	0.924	0.717	0.906	0.706	0.909	0.759	0.914
Los Angeles	0.881	0.941	0.928	0.986	0.951	0.982	0.952	0.982	0.967	0.987
Philadelphia	0.610	0.746	0.744	0.930	0.807	0.913	0.796	0.917	0.831	0.921
Galveston	0.633	0.788	0.745	0.898	0.814	0.910	0.812	0.910	0.844	0.913

NOTE: The above table covers only outside and in-ship locations. Crafts located in shops are unaffected by weather and are assumed to have a productivity of 1.0 (100%).

TABLE A-3. Estimated Productivity Gain for Painters Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

Location	<u>Weather Protection Provided</u>				
	Shade	Rain Protection	Dehumidifiers	Wind Protection	Cooling
San Diego	1.004	1.000	1.031	1.034	1.004
Mobile	1.026	1.000	1.196	1.162	1.054
Boston	1.006	1.000	1.135	1.439	1.016
Los Angeles	1.003	1.000	1.054	1.067	1.003
Philadelphia	1.010	1.000	1.117	1.223	1.025
New Orleans	1.011	1.000	1.155	1.142	1.061
Norfolk	1.014	1.000	1.120	1.216	1.032
Portland, Maine	1.004	1.000	1.263	1.262	1.009
New York	1.007	1.000	1.147	1.336	1.012
Houston	1.029	1.000	1.169	1.242	1.071
Seattle	1.002	1.000	1.262	1.255	1.003
Portland, Oregon	1.003	1.000	1.167	1.139	1.008
Baltimore	1.015	1.000	1.137	1.262	1.033
Galveston	1.036	1.000	1.163	1.236	1.057

NOTE: For painters, productivity gains for rain protection are included in the gains for dehumidifiers. It was assumed that rain protection alone gave no productivity gain because relative humidity during rain was above 90%, a stop work condition for

**TABLE A-4. Estimated Productivity Gain for Riggers Normally Assigned to Outside Work
When Protection Is Provided for Each Adverse Weather Condition**

Location	<u>Weather Protection Provided</u>					
	Shade	Rain Protection	Dehumidifiers	Wind Protection	Cooling	Heating
San Diego	1.003	1.005	1.000	1.012	1.004	1.007
Mobile	1.024	1.021	1.000	1.021	1.078	1.032
Boston	1.007	1.024	1.000	1.266	1.014	1.054
Los Angeles	1.004	1.008	1.000	1.028	1.004	1.007
Philadelphia	1.010	1.018	1.000	1.126	1.021	1.048
New Orleans	1.011	1.021	1.000	1.062	1.056	1.012
Norfolk	1.014	1.021	1.000	1.113	1.028	1.040
Portland, Maine	1.004	1.024	1.000	1.169	1.007	1.100
New York	1.006	1.021	1.000	1.198	1.025	1.020
Houston	1.028	1.017	1.000	1.109	1.065	1.012
Seattle	1.001	1.023	1.000	1.150	1.003	1.029
Portland, Oregon	1.002	1.026	1.000	1.081	1.007	1.021
Baltimore	1.013	1.019	1.000	1.151	1.027	1.043
Galveston	1.036	1.012	1.000	1.106	1.057	1.002

NOTE: No productivity allowance was made for humidity control for crafts other than painters. It was assumed that the productivity estimates for each temperature range included the average effects of humidity.

**TABLE A-5. Estimated Productivity Gain for Fitters Normally Assigned to Outside Work
When Protection Is Provided for Each Adverse Weather Condition**

Location	<u>Weather Protection Provided</u>					
	Shade	Rain Protection	Dehumidifiers	Wind Protection	Cooling	Heating
San Diego	1.003	1.005	1.000	1.012	1.004	1.007
Mobile	1.024	1.021	1.000	1.080	1.051	1.009
Boston	1.006	1.025	1.000	1.278	1.013	1.061
Los Angeles	1.003	1.008	1.000	1.027	1.003	1.009
Philadelphia	1.010	1.019	1.000	1.137	1.021	1.051
New Orleans	1.012	1.020	1.000	1.065	1.056	1.011
Norfolk	1.014	1.021	1.000	1.120	1.029	1.041
Portland, Maine	1.004	1.023	1.000	1.179	1.007	1.113
New York	1.009	1.019	1.000	1.210	1.025	1.024
Houston	1.029	1.017	1.000	1.112	1.066	1.010
Seattle	1.001	1.023	1.000	1.162	1.003	1.029
Portland, Oregon	1.002	1.026	1.000	1.087	1.008	1.022
Baltimore	1.013	1.019	1.000	1.193	1.027	1.047
Galveston	1.036	1.013	1.000	1.107	1.057	1.003

NOTE: No productivity allowance was made for humidity control for crafts other than painters. It was assumed that the productivity estimates for each temperature range included the average effects of humidity.

TABLE A-6. Estimated Productivity Gain for Other Crafts Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

Location	<u>Weather Protection Provided</u>					
	Shade	Rain Protection	Dehumidifiers	Wind Protection	Cooling	Heating
San Diego	1.004	1.004	1.000	1.008	1.005	1.000
Mobile	1.024	1.018	1.000	1.055	1.051	1.004
Boston	1.005	1.020	1.000	1.207	1.013	1.051
Los Angeles	1.004	1.007	1.000	1.018	1.004	1.001
Philadelphia	1.010	1.015	1.000	1.102	1.020	1.044
New Orleans	1.011	1.017	1.000	1.042	1.056	1.008
Norfolk	1.014	1.017	1.000	1.088	1.029	1.019
Portland, Maine	1.004	1.019	1.000	1.140	1.006	1.094
New York	1.007	1.017	1.000	1.157	1.022	1.018
Houston	1.028	1.015	1.000	1.073	1.065	1.007
Seattle	1.001	1.020	1.000	1.120	1.003	1.017
Portland, Oregon	1.002	1.022	1.000	1.066	1.008	1.037
Baltimore	1.012	1.017	1.000	1.123	1.027	1.038
Galveston	1.036	1.011	1.000	1.069	1.058	1.000

NOTE: No productivity allowance was made for humidity control for crafts other than painters. It was assumed that the productivity estimates for each temperature range included the average effects of humidity.

**TABLE A-7. Estimated Productivity Gain for Welders Normally Assigned to Outside Work
When Protection Is Provided for Each Adverse Weather Condition**

Location	<u>Weather Protection Provided</u>					
	Shade	Rain Protection	Dehumidifiers	Wind Protection	Cooling	Heating
San Diego	1.004	1.013	1.000	1.023	1.005	1.000
Mobile	1.023	1.048	1.000	1.122	1.063	1.121
Boston	1.005	1.067	1.000	1.364	1.016	1.056
Los Angeles	1.003	1.019	1.000	1.047	1.005	1.002
Philadelphia	1.009	1.052	1.000	1.179	1.027	1.046
New Orleans	1.011	1.047	1.000	1.102	1.072	1.006
Norfolk	1.013	1.052	1.000	1.169	1.036	1.021
Portland, Maine	1.003	1.066	1.000	1.223	1.009	1.106
New York	1.006	1.058	1.000	1.276	1.014	1.030
Houston	1.027	1.040	1.000	1.173	1.082	1.008
Seattle	1.001	1.076	1.000	1.212	1.004	1.018
Portland, Oregon	1.002	1.074	1.000	1.113	1.010	1.027
Baltimore	1.012	1.052	1.000	1.209	1.033	1.043
Galveston	1.035	1.030	1.000	1.170	1.076	1.000

NOTE: No productivity allowance was made for humidity control for crafts other than painters. It was assumed that the productivity estimates for each temperature range included the average effects of humidity.

attributable to each weather condition for each craft, work location, and shipbuilding region. An individual shipyard could estimate the productivity gain a weather protection facility at their shipyard using the following formula.

$$P_g = P_a \times P_b \times P_c \cdots \times P_n - 1$$

where

P_g = fraction productivity gain for each craft and location affected

P_a = fraction gain for that craft and location for a specific weather protection, e.g., wind

P_b = fraction gain for each craft, location, and second weather protection, e.g., shade

P_c = fraction gain for each craft, location, and third weather protection, e.g., rain

P_n = continue for each additional weather protection category

Then, taking the number of craft people protected by the facility

Annual \$ saved each craft and location = $P_g \times$ effective annual wage expense for craft \times number of craft people protected

Total \$ saved Σ \$ saved for each craft and location.

For illustration, assume the weather protection facility is a completely enclosed, unheated and uncooled, building for 35 welders in Baltimore. The building provides shade and complete protection from rain and wind. The estimated productivity gain (using factors for Baltimore from Table A-7) would be

$$\begin{aligned} P_g &= P_{\text{shade}} \times P_{\text{rain}} \times P_{\text{wind}} - 1 \\ &= 1.012 \times 1.052 \times 1.209 - 1 \\ &= 0.287 \text{ (28.7\%)} \end{aligned}$$

Assume the average annual expenditure per welder is \$20,000.

Then, the annual dollar savings for increased productivity for this facility would be (for 35 welders)

$$0.287 \times \$20,000 \times 35 = \$200,000$$

In other words, \$200,000 of additional work could be performed annually by these welders. A greater savings would result if overtime premiums were reduced, and an even greater savings would result if a greater shipbuilding capacity were achievable; i.e., to the extent that the welders were on the critical path. If other crafts were also protected from weather by this facility, the dollars saved would be added for each craft. The total dollars saved annually should be compared with the total annual dollar expenditure for each facility to determine the cost-effectiveness of the facility.

If this analysis appears cost-effective, the estimates of productivity which form the basis for the model (Table A-1) should be re-evaluated for the local situation and the analysis repeated, if lower productivity factors are indicated. Alternatively, new productivity estimates could be entered in the computer program data base, Appendix Land the program could be run to obtain new productivity factors.

EXHIBIT A

ALGORITHM FOR PRECIPITATION COVERING PASS-OUT CONDITIONS AND TRANSFER OF WORKERS TO PROTECTED LOCATIONS

Workers will be passed out only for Precipitation rates greater than .02"/hr or, for painters and blasters only, for relative humidity occurrences greater than 90%. The occurrences of precipitation will be averaged over each shift in the following categories: .01"/hr; .02" - .09"/hr; .1" Or greater/hr.

- (1) All workers will work in .01"/hr precipitation at the reduced productivity rate. No pass-outs.
- (2) For the two precipitation categories of .02" and greater/hr, we will assume that 20% of the workers will be passed out sometime during the shift, and the remaining 80% will work the entire shift at the reduced productivity rate.
 - (a) We will assume that on the average the pass-outs will occur rather uniformly throughout the shift; that is:
 - (i) 1/4 of the time, the workers will be sent home at the beginning of the shift; work - 2 hours pay.
 - (ii) 1/4 of the time, the workers will be sent home after 2 hours; 2 hours work - 4 hours pay.
 - (iii) 1/4 of the time, the workers will be sent home after 4 hours; 4 hours work - 4 hours pay.
 - (iv) 1/4 of the time, the workers will be sent home with 6 hours work and 6 hours pay.

As shown in Table A-8 this can be summarized as 7.2 hours (90%) are paid, on the average, for 7.0 hours (87.5%) work for these occurrences. The productivity during the work periods is, of course, reduced according to Table A-1.

- (b) In those cases where outside productivity would be zero, as for painters and welders, we will assume that 1 hour of each work day is lost transferring 80% of the workers to inside work. We will further assure the same 80% were transferred to inside work at the beginning of the shift in anticipation of precipitation. Table A-8 then becomes for these instances:
 - 7.2 hours pay
 - .6 hours outside work - 100% productivity (average hours of outside work performed by the 20% of the workers before being passed out)
 - 5.6 hours inside work - @ applicable productivity rate

TABLE A-8. Assumed Paid Time and Hours Worked When Precipitation
Rate $>.02"/\text{Hr}$

<u>Fraction of Time</u>	<u>Fraction of Workers</u>	<u>Hours Pay</u>	<u>Weighted Hours Pay</u>	<u>Hours Work</u>	<u>Weighted Hours Work</u>
1/4	.2	2	.1	0	0
	.8	8	1.6	8	1.6
1/4	.2	4	.2	2	.1
	.8	8	1.6	8	1.6
1/4	.2	4	.2	4	.2
	.8	8	1.6	8	1.6
1/4	.2	6	.3	6	.3
	.8	8	1.6	8	1.6
			<hr/> 7.2		<hr/> 7.0

EXHIBIT B

EXPLANATIONS OF SPECIAL CONDITIONS AND PENALTIES WHICH APPLY TO THE PRODUCTIVITY TABLE A-1

(Comparisons are to all other crafts)

- (1) Painters will work outside only when actual temperature is 35°F or above.
- (2) Painters' productivity was penalized additional 5% for temperatures over 90°F because some paints cannot be applied in this temperature range.
- (3) Painters' productivity in wind is penalized additionally because of high paint losses; i.e., more spraying is required to achieve same coating thickness.
- (4) Painter will work outside only when the relative humidity is less than 90%. The effect of fog and other precipitation is included in the relative humidity affect.
- (5) Welders and fitters are penalized 5% when effective temperature is below 29°F caused by more preheating time and the effect of cold steel on the welders comfort.
- (6) Welders are penalized 5% when effective temperature exceeds 80°F for additional fatigues caused by heat radiation from hot steel.
- (7) Riggers are penalized 5% at temperatures <5°F because of reduced service availability of cranes.
- (8) Welders are penalized in wind because of greater difficulty in positioning parts, higher reject rates, and difficulty in maintaining gas shields for MIG and TIG welding.
- (9) Riggers and fitters are penalized in high wind reflecting difficulty in positioning structures, crane operations. Some operations must stop in winds in excess of 20 mph. Nearly all operations stop with winds in excess of 40 mph.
- (10) Extra penalties for welders for precipitation are brought about by extra time for drying joints, interrupted work, or rework. Penalties for other crafts reflect more difficult working conditions.
- (11) Fog directly affects only the crane operations and the riggers and fitters who work more closely with the crane operators.
- (12) The absence of shade tends to increase the effective outside temperature about 10°F causing an additional 30% loss of productivity in the sun when the temperature is above 80°F. We will assume that outside workers are in the shade half of the time.

EXHIBIT C

ASSUMPTIONS OF PRODUCTIVITY FOR WORKERS PROTECTED BY THE SHIP'S STRUCTURE

Workers are generally protected from wind and rain. The effective temperature is the dry bulb temperature. These productivities assume no-additional heating, cooling, or dehumidifying, but assume minimum ventilation to remove fumes from painting and welding.

- (1) At temperatures above 80°F, a 5% penalty is assessed for buildup of heat from men and equipment. Heat from welding is assumed to cause an additional 5% penalty.
- (2) Heat provided by welding increases productivity to 100% in the temperature range of 30-39°F.
- (3) Painters' 70% productivity in 30-39°F temperature range reflects loss of productivity below freezing point, time waiting for temperature to rise, drying surfaces, etc.
- (4) Loss of productivity in high wind and rain is caused by increased difficulty and delays in supplying needed parts, tools, and materials; drafts, dust, leaks, and noise interfering with work and causing uncomfortable or more hazardous working conditions; hesitancy of workers to transfer between work stations involving exposure to the elements; extra work to secure parts and equipment; and general interdependency on some outside work.
- (5) Without drying equipment, relative humidity within ship is assumed to be the same as outside. In many instances, it is worse, particularly below the water line during outfilling.
- (6) Lack of shade is assumed to increase temperature within the ship, reducing productivity further

EXHIBIT D

ASSUMPTIONS TO BE USED IN THE CALCULATIONS

- (1) The annual hourly occurrences of effective temperature and dry bulb temperature will be used for the Productivity measurements for each shift.
- (2) The percentage occurrence of wind will be averaged for each shift.
- (3) The percentage occurrence of precipitation and >90% relative humidity will be averaged for each full shift.
- (4) The annual % frequency of fog will be applied to each shift.
- (5) The correction for lack of shade will be made to that portion of the shift affected. We will assume shade and cloud cover are beneficial from 9 a.m. through 6 p.m. when the dry bulb temperature exceeds 80°F.

APPENDIX B

WEATHER DATA FOR U. S. SHIPYARD LOCATIONS

A summary of annual weather observations near each shipbuilding location is presented in Exhibit A. These tables were taken from a "Summary of Hourly Observation" from the Decennial Census of United States Climate, 1951-1960, U. S. Department of Commerce. Exhibit A also contains precipitation data for Seattle and Mobile covering a five-year period and precipitation data for Newark, New Jersey, which was substituted for the missing precipitation data for New York International.

The tables in Exhibit A are reproduced from the best available copies. These data are not used directly in the computer model. For use in the computer model, these annual data were disaggregated into frequencies of occurrence for the three standard work shifts (Exhibit B). These data (Exhibit B) were input to our computer model and are the same data a shipyard would use.

APPENDIX B, EXHIBIT A

ANNUAL SUMMARIES OF HOURLY WEATHER OBSERVATIONS

A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND IN MONTH Temp °F.	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL OBS.
	0-4 M.P.H.	5-14 M.P.H.	15-24 M.P.H.	25 M.P.H.	26-34 M.P.H.	35-44 M.P.H.	0-4 M.P.H.	5-14 M.P.H.	15-24 M.P.H.	25 M.P.H.	26-34 M.P.H.	35-44 M.P.H.	0-4 M.P.H.	5-14 M.P.H.	15-24 M.P.H.	25 M.P.H.	26-34 M.P.H.	35-44 M.P.H.	0-4 M.P.H.	5-14 M.P.H.	15-24 M.P.H.	25 M.P.H.	26-34 M.P.H.	35-44 M.P.H.	
99/ 95																									1
94/ 90																									14
89/ 85																									58
84/ 80																									149
79/ 75																									275
74/ 70																									407
69/ 65																									627
64/ 60																									780
59/ 55																									808
54/ 50																									760
49/ 45																									748
44/ 40																									772
39/ 35																									839
34/ 30																									820
29/ 25																									599
24/ 20																									408
19/ 15																									293
14/ 10																									190
9/ 5																									109
04/ 00																									60
-01/-05																									29
-05/-10																									15
-11/-15																									5
-16/-20																									1
TOTAL	2	50	196	195	329	806	36	623	1522	900	987	1591	29	277	471	161	140	330	4	17	27	9	11	56	3767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole number, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO. OF DAYS OBS.
	P.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	NOON	
TRACE	31	26	27	25	31	34	34	33	33	35	33	31	32	33	36	37	37	34	33	35	34	34	30	31	50
01 IN	10	12	14	14	11	10	10	10	9	8	8	7	7	7	8	8	9	12	10	9	10	11	11	10	11
02 TO 09 IN	19	18	20	20	21	21	18	19	19	18	17	17	16	16	13	14	18	18	19	17	18	16	18	19	42
10 TO 24 IN	4	4	4	6	5	6	5	5	5	4	4	4	5	5	5	4	3	3	4	4	4	4	3	4	26
25 TO 49 IN	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	21
50 TO 99 IN	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	22
100 TO 199 IN																									8
200 IN AND OVER																									1
TOTAL	65	63	65	65	69	71	68	68	65	66	63	60	61	62	64	66	67	67	66	65	65	67	64	65	183

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT.
	0	100- 999	1000- 4999	5000- 9999	10000- 19999	20000- 29999	30000- 39999	40000- 49999	50000- 59999	60000- 69999	
0 TO 1/8	1.0	0.3	+	+	+	+	+	+	+	+	1.5
3/8 TO 1/2	0.3	0.5	0.1	+	+	+	+	+	+	+	1.0
1/2 TO 3/4	+	0.9	0.5	0.2	+	+	+	+	+	+	1.8
1 TO 2 1/2	+	0.9	2.5	2.0	0.6	0.2	0.2	0.3	0.6	0.6	7.4
3 TO 8		0.1	0.9	2.7	1.5	0.7	0.6	1.2	3.9	11.7	
7 TO 15			0.1	1.0	2.3	2.4	5.1	9.3	5.4	76.6	
20 TO 30											
35 OR MORE											
TOTAL	1.3	2.6	4.0	5.6	4.3	3.3	6.2	10.6	11.5	100	

WIND	TOTAL OBS.
1	1
14	14
58	58
149	149
275	275
407	407
627	627
1	1
3	3
780	780
9	9
808	808
4	4
760	760
10	10
748	748
11	11
772	772
7	7
839	839
7	7
820	820
4	4
599	599
2	2
408	408
4	4
293	293
+	+
190	190
+	+
109	109
60	60
29	29
15	15
5	5
1	1
563767	563767

B
PERCENTAGE FREQUENCIES
OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED IN MILES PER HOUR										TOTAL	AV SPEED
	0-3	4-7	8-12	13-18	19-24	25-31	32-38	39-46	47 OVER			
	0-3	4-7	8-12	13-18	19-24	25-31	32-38	39-46	47 OVER			
N	.4	2.5	3.3	2.1	.4	.1	+	+		8.9	10.5	
NNE	.2	1.1	1.6	1.6	.4	.1	+	+		5.1	11.9	
NE	.1	.8	1.0	.5	.2	.1	+			2.7	10.3	
ENE	.1	.7	1.0	.7	.2	.1	+	+		2.8	11.6	
E	.2	.9	1.5	1.0	.2	.1	+	+		3.9	11.1	
ESE	.1	.7	1.0	.6	.1	+	+	+		2.6	10.1	
SE	.1	.7	.6	.4	.1	+	+	+		2.0	9.5	
SSE	.2	.8	1.5	1.1	.1	.1	+	+	+	3.9	11.2	
S	.3	1.7	3.1	2.8	.5	.1	+	+		8.5	11.3	
SSW	.3	2.2	2.7	1.4	.2	+				6.9	9.5	
SW	.4	2.5	2.5	1.0	.1	+	+			6.6	8.7	
WSW	.5	2.9	2.8	1.7	.4	.1	+			8.4	9.9	
W	.7	3.6	2.7	1.5	.4	.1	+			9.1	9.2	
WNW	.6	3.3	2.6	1.5	.3	.1	+			8.5	9.2	
NW	.6	3.0	2.5	1.6	.3	.1	+	+		8.0	9.3	
NNW	.3	2.2	2.4	1.8	.3	+	+			7.2	10.2	
CALM	4.8									4.8		
TOTAL	10.1	29.8	32.9	21.5	4.3	1.2	.2	+	+	100	9.6	

E
PERCENTAGE FREQUENCIES OF
SKY COVER, WIND, AND
RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M.P.H.)					RELATIVE HUMIDITY (%)						
	0-3	4-7	8-10	0-3	4-7	13-24	25-31	OVER	0-29	30-49	50-69	70-79	80-89	90-100	
	0-3	4-7	8-10	0-3	4-7	13-24	25-31	OVER	0-29	30-49	50-69	70-79	80-89	90-100	
00	42	10	47	15	70	14	1	+	2	15	14	22	47		
01	42	10	48	16	69	15	1		1	15	14	20	50		
02	42	10	48	16	69	14	1		1	13	14	21	52		
03	40	11	49	15	70	14	.1		1	12	13	21	53		
04	37	12	50	15	69	15	1		1	11	13	20	54		
05	36	13	52	16	68	15	1		1	11	13	21	53		
06	36	12	53	15	68	16	1	+	1	14	16	23	46		
07	35	12	53	12	67	19	1	+	3	20	18	21	37		
08	34	12	52	10	63	26	1	+	8	32	18	16	26		
09	35	12	53	7	60	31	2	+	16	37	14	12	20		
10	34	13	53	5	57	36	2	1	23	38	12	10	17		
11	31	16	52	4	53	41	2	2	27	37	10	9	15		
12	30	17	52	3	50	44	3	2	29	36	10	9	14		
13	30	17	52	2	46	47	3	3	31	35	10	8	13		
14	31	18	51	2	48	48	2	3	29	35	11	9	13		
15	31	18	51	2	51	45	2	3	26	36	12	10	14		
16	33	16	51	4	57	38	2	2	20	37	13	11	16		
17	35	14	51	5	64	30	1	1	14	35	17	14	18		
18	35	14	51	8	67	23	1	1	10	31	19	18	22		
19	37	12	50	10	68	20	1	+	27	19	20	27			
20	40	11	49	12	68	18	1	+	4	24	17	21	34		
21	41	11	48	14	68	17	1	+	3	21	16	21	38		
22	42	11	47	15	68	16	1		3	19	16	21	41		
23	43	10	47	16	68	15	1	+	2	17	16	22	44		
AVG	36	13	51	10	63	26	1	1	11	25	14	17	32		

PORTLAND, MAINE
Municipal Airport

A TEMPERATURE AND WIND SPEED—RELATIVE HUMIDITY OCCURRENCES:

WIND DIR SPEED TEMP RH	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL
	SEAS	SW	NE	SE	SW	NE	SE	SW	NE	SE	SW	NE	SE	SW	NE	SE	SW	NE	SE	SW	NE	SE	SW	NE	
104/100																									+
99/ 95																									10
94/ 90																									39
89/ 85																									127
84/ 80																									245
79/ 75																									433
74/ 70																									676
69/ 65																									819
64/ 60																									804
59/ 55																									781
54/ 50																									766
49/ 45																									757
44/ 40																									628
39/ 35																									868
34/ 30																									674
29/ 25																									429
24/ 20																									256
19/ 15																									151
14/ 10																									74
09/ 05																									35
04/ 00																									4
-01/-05																									9
-06/-10																									1
-11/-15																									+
TOTAL	3	34	100	80	100	137	81	774	1643	843	865	838	112	796	991	312	299	330	27	126	94	30	40	107	8767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS WITH
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	NO.	
TOTAL	34	38	39	39	39	41	38	41	40	39	41	37	35	35	37	36	35	35	35	34	38	37	36	34	62
01 IN	10	10	12	12	13	10	11	11	10	10	10	9	10	10	9	11	12	11	12	12	10	12	11	12	16
02 TO 09 IN	17	15	16	17	15	17	20	16	16	17	15	16	16	16	14	16	17	18	17	18	15	15	16	17	38
10 TO 21 IN	6	7	7	5	6	5	4	5	6	5	5	5	5	5	6	6	5	4	5	3	4	5	6	24	
22 TO 49 IN	1	2	1	1	1	1	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	21	
50 TO 99 IN	+	+	+	1	+	+	+	+	+	+	+	+	+	+	1	+	+	+	+	+	+	+	+	11	
100 TO 199 IN																									2
200 IN AND OVER																									2
TOTAL	68	72	74	73	73	74	75	75	74	71	72	68	68	67	67	70	68	71	70	67	69	69	69	69	196

D PERCENTAGE FREQUENCIES OF CEILING—VISIBILITY:

VISIBILITY (MILES)	CEILING FEET									
	0	100-200	200-400	400-600	600-1000	1000-2000	2000-3000	3000-5000	OVER 5000	TOT.
0 TO 1/8	+	+	+	+	+	+	+	+	+	+
3/16 TO 1/4	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1
1 TO 1 1/2			1	2	1	+	+	+	1	5
3 TO 6			1	3	2	1	1	1	0	16
7 TO 13	+	+	+	2	3	3	5	8	56	76
20 TO 30									+	+
35 OR MORE									+	+
TOTAL	+	1	2	6	6	3	6	10	65	100

BOSTON, MASS.
Logan Int. Airport

35 MPH AND OVER						TOTAL OIL
F E B	M A R	A P R	M A Y	J U N	J U L	
						+
						39
		+				127
	1	2				245
2	2	3		+		433
6	2	4		1		1
4	2	5		1	1	676
2	2	5		2	2	819
4	2	5		2	3	804
2	2	6		1	4	781
6	2	7		1	6	766
4	2	5		2	3	757
2	2	11	13	6	4	828
2	2	11	13	3	6	848
8	2	14	13	2	3	874
2	2	19	12	3	4	429
2	2	10	3	2	2	256
+	+	10	3	2	1	151
	1	5			1	74
	2	1	1	+		35
	+					9
						1
0	27	128	94	30	401	8767

AT					NO OF DAYS WITH
8	9	10	11	12	
34	38	37	36	34	62
12	10	12	11	12	16
18	15	15	16	17	38
3	4	5	5	6	24
1	1	1	1	1	21
4	4		4		21
4					11
					2
67	69	69	69	69	96

B-4

HENRY OBSERVATIONS ON WINDS SET																NO.	
JANUARY 1907																	
DIRECTIONS	0	3	6	9	12	15	18	21	24	27	30	33	36	39	42	45	TOTAL
N	+		1		2		2	+		+		+		+		+	5 12.0
NNE	+		1		1		1	+		+		+		+		+	3 13.3
NE	+		1		1		1	1		+		+		+		+	4 14.2
ENE	+		1		1		1	1		+		+		+		+	4 14.1
E	+		1		2		2	+		+		+		+		+	5 12.9
ESE	+		1		2		2	+		+		+		+		+	5 12.0
SE	+		1		2		1	+		+		+		+		+	4 10.8
SSE	+		1		1		1	+		+		+		+		+	3 10.4
S	+		1		2		1	+		+		+		+		+	4 11.0
SSW	+		1		3		2	1		+		+		+		+	7 13.0
SW	+		1		4		5	1		+		+		+		+	12 13.3
WSW	+		1		3		3	1		+		+		+		+	7 13.0
W	+		1		2		3	1		+		+		+		+	8 14.2
NNW	+		1		3		4	2		1		+		+		+	11 14.6
NW	+		1		3		4	2		1		+		+		+	11 15.2
NNW	+		1		2		3	1		+		+		+		+	7 13.6
CALM		1															1
TOTAL	3	12	33	35	12	4	1	+		+	100	13.3					

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M P H.)					RELATIVE HUMIDITY (%)					
	0-3	4-7	8-10	0-3	4-12	12-24	25- 8	0-29	30-49	50-69	70-79	80-89	90-100	
	OVR													
00	43	8	49	4	53	39	3	+	10	34	18	19	20	
01	42	9	49	4	54	38	3	+	9	33	18	19	21	
02	43	9	49	4	55	37	3	+	8	32	17	20	23	
03	42	9	50	4	56	36	4	+	7	31	18	21	23	
04	40	9	51	5	55	37	3	+	7	29	19	21	24	
05	38	9	52	5	56	36	3	+	6	29	20	21	24	
06	37	10	53	4	54	39	3	+	7	32	20	20	22	
07	36	10	54	4	50	42	4	+	10	16	18	18	19	
08	36	11	53	4	46	45	5	+	16	38	18	14	15	
09	36	11	53	3	43	48	6	1	24	38	12	12	13	
10	34	12	53	3	40	51	7	3	30	34	11	10	12	
11	32	15	53	2	38	54	7	4	34	32	10	9	11	
12	31	17	52	2	35	55	8	6	36	30	10	9	10	
13	30	17	53	1	32	59	8	8	36	29	10	9	9	
14	31	17	52	1	31	60	8	8	36	28	9	9	9	
15	31	17	52	1	32	61	6	6	34	28	10	9	9	
16	33	14	53	1	35	58	7	7	32	29	11	10	10	
17	35	13	51	2	39	54	5	5	29	30	12	12	11	
18	37	12	51	2	44	50	4	4	25	32	14	12	14	
19	38	12	50	3	47	46	4	2	21	33	15	15	15	
20	40	11	49	3	48	45	4	1	17	35	15	16	16	
21	40	11	49	4	49	43	4	1	15	35	15	17	17	
22	41	10	49	4	50	43	4	+	13	35	16	18	18	
23	42	9	49	4	52	41	4	+	11	35	16	19	19	
AVG	37	12	51	3	46	46	5		3	26	32	15	16	

A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIRECTION SPEED REL. HUM.	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL OLS		
	N	NE	E	SE	S	SW	SW	W	NW	N	NE	E	SE	S	SW	SW	W	NW	N	NE	E	SE	S	SW		W	NW
04/100																											
99/ 95							3	2	+																		
94/ 90							+	13	4																		
89/ 85							2	28	34																		
84/ 80		1	1				3	47	84																		
79/ 75	+	7	12	12	12	6	5	76	122	88	74	28	+														
74/ 70	1	6	16	15	34	43	7	72	148	105	141	133															
59/ 65	+	6	20	22	31	40	8	61	152	105	129	130															
64/ 60	1	5	15	16	24	30	9	56	125	89	101	102															
59/ 55	+	5	16	16	21	28	6	62	114	79	84	105															
54/ 50	+	5	17	14	18	23	4	55	126	77	76	97															
49/ 45	+	4	18	16	19	22	4	54	128	78	77	104															
44/ 40	+	5	16	14	17	17	2	46	155	91	82	102															
39/ 35	+	5	23	15	16	16	1	44	185	85	78	89															
34/ 30	+	6	19	10	6	8	2	38	149	49	39	44															
29/ 25	+	2	8	4	2	1	1	28	87	19	9	11															
24/ 20	+	3	4	2	1	+	+	27	48	6	3	1															
19/ 15							+	+	1																		
14/ 10								4	6	1	+	+															
19/ 05								2	2	+																	
14/ 00								+	+																		
TOTAL	3	62	196	158	201	234	54	727	1691	904	900	945	56	560	888	284	278	341	10	65	86	24	30	72	3767		

In Table A, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

DATA NOT AVAILABLE

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100-200	200-400	400-600	600-1000	1000-2000	2000-3000	3000-5000	5000-10000	10000
0 TO 1/8	+	+	+	+	+	+	+	+	+	1
3/8 TO 1/2	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1
1 TO 1 1/2	+	+	1	1	1	+	+	+	3	6
3 TO 6	+	+	1	3	2	1	1	2	12	21
7 TO 15	+	+	+	1	3	2	5	7	52	70
20 TO 30										
30 CE ABOVE										
TOTAL	+	1	2	5	5	3	7	9	67	108

A

HR	CS	TOTAL CS
1	2	2
2	4	4
3	3	3
4	8	8
5	6	6
6	7	7
7	11	11
8	14	14
9	9	9
10	8	8
11	6	6
12	2	2
13	2	2
14	2	2
15	2	2
16	2	2
17	2	2
18	2	2
19	2	2
20	2	2
21	2	2
22	2	2
23	2	2
24	2	2
25	2	2
26	2	2
27	2	2
28	2	2
29	2	2
30	2	2
31	2	2
32	2	2
33	2	2
34	2	2
35	2	2
36	2	2
37	2	2
38	2	2
39	2	2
40	2	2
41	2	2
42	2	2
43	2	2
44	2	2
45	2	2
46	2	2
47	2	2
48	2	2
49	2	2
50	2	2
51	2	2
52	2	2
53	2	2
54	2	2
55	2	2
56	2	2
57	2	2
58	2	2
59	2	2
60	2	2
61	2	2
62	2	2
63	2	2
64	2	2
65	2	2
66	2	2
67	2	2
68	2	2
69	2	2
70	2	2
71	2	2
72	2	2
73	2	2
74	2	2
75	2	2
76	2	2
77	2	2
78	2	2
79	2	2
80	2	2
81	2	2
82	2	2
83	2	2
84	2	2
85	2	2
86	2	2
87	2	2
88	2	2
89	2	2
90	2	2
91	2	2
92	2	2
93	2	2
94	2	2
95	2	2
96	2	2
97	2	2
98	2	2
99	2	2
100	2	2

PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	WIND SPEED (MPH)																TOTAL	AVG
	0-5	6-10	11-15	16-20	21-25	26-30	31-35	36-40	41-45	46-50	51-55	56-60	61-65	66-70	71-75	76-80		
N	+	1	3	2	1	+	+	+	+	+	+	+	+	+	+	+	7	11.5
NNE	+	1	2	2	1	+	+	+	+	+	+	+	+	+	+	+	6	11.6
NNE	+	1	2	1	+	+	+	+	+	+	+	+	+	+	+	+	5	11.3
NNE	+	1	1	1	+	+	+	+	+	+	+	+	+	+	+	+	4	10.4
E	+	1	1	1	+	+	+	+	+	+	+	+	+	+	+	+	3	10.7
ESE	+	1	1	1	+	+	+	+	+	+	+	+	+	+	+	+	3	10.5
SE	+	1	1	1	+	+	+	+	+	+	+	+	+	+	+	+	3	11.2
SSE	+	1	2	2	1	+	+	+	+	+	+	+	+	+	+	+	6	12.5
S	+	2	4	3	1	+	+	+	+	+	+	+	+	+	+	+	10	12.2
SSW	+	2	4	3	1	+	+	+	+	+	+	+	+	+	+	+	9	11.4
SW	+	2	3	2	+	+	+	+	+	+	+	+	+	+	+	+	8	10.6
WSW	+	1	3	2	1	+	+	+	+	+	+	+	+	+	+	+	8	12.4
W	+	1	2	2	1	+	+	+	+	+	+	+	+	+	+	+	6	14.0
WNW	+	1	2	3	1	+	+	+	+	+	+	+	+	+	+	+	8	14.5
NW	+	1	2	3	1	+	+	+	+	+	+	+	+	+	+	+	8	14.1
NNW	+	1	2	2	1	+	+	+	+	+	+	+	+	+	+	+	7	12.7
CALM	2	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2	+
TOTAL	6	17	35	28	10	3	+	+	+	+	+	+	+	+	+	+	100	12.0

PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOURS OF DAY	CLOUDS SCALE 0-10			WIND SPEED (MPH)				RELATIVE HUMIDITY (%)							
	0-3	4-7	8-10	0-3	4-7	8-10	11-15	0-29	30-49	50-69	70-79	80-89	90-99	100	
00	46	11	42	9	61	28	2	+	8	30	17	21	24		
01	46	10	44	9	62	27	2	+	7	29	17	21	25		
02	45	11	44	10	61	27	2	+	6	29	17	22	27		
03	46	10	44	11	61	27	2	+	5	28	17	21	28		
04	44	11	45	11	61	26	2	+	5	27	17	22	30		
05	40	12	46	11	62	25	2	+	4	27	18	21	30		
06	37	13	50	10	60	27	2	+	4	29	18	20	28		
07	35	14	51	9	56	32	2	+	6	34	18	20	22		
08	35	13	52	7	52	38	3	+	11	39	16	17	17		
09	35	14	51	6	50	40	4	+	1	40	15	13	14		
10	35	16	50	4	48	44	4	+	1	25	38	14	11	12	
11	33	16	50	3	45	40	4	+	2	30	36	12	9	11	
12	32	18	50	2	43	50	5	+	3	33	34	11	9	10	
13	32	18	50	2	40	53	5	+	4	34	33	11	9	9	
14	31	19	50	2	37	56	5	+	5	32	34	11	9	9	
15	32	18	50	2	38	55	6	+	5	30	35	11	10	9	
16	32	18	51	2	40	54	4	+	4	26	35	13	11	10	
17	33	17	49	2	45	49	4	+	3	22	35	15	13	11	
18	35	14	46	3	49	45	4	+	2	19	34	17	15	14	
19	38	15	47	5	53	39	4	+	1	15	33	18	17	16	
20	41	14	45	6	54	37	3	+	1	13	31	18	19	18	
21	44	13	43	7	57	34	2	+	1	12	30	19	19	20	
22	45	15	42	7	59	32	2	+	1	11	30	19	20	20	
23	43	12	43	8	60	30	2	+	9	30	17	21	22		
AVG	38	14	47	6	52	38	3	+	1	16	33	16	16	10	

NEW YORK, NEW YORK
Int. Airport (Idlewif)

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND SPEED KTS	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL
	0-4	5-14	15-24	25-34	35-44	45-54	5-14	15-24	25-34	35-44	45-54	5-14	15-24	25-34	35-44	45-54	5-14	15-24	25-34	35-44	45-54	5-14	15-24	25-34	
100	1	1	+				1	10					+	+											1
95							1	10					1	2	1										17
90	+	6	2				2	37	16				+	7	4				+						74
85	1	10	11				7	69	83				1	19	19				+						225
80	2	15	25	9	2		6	102	138				4	23	28	7			+	+	+				420
75	2	16	28	25	26	16	11	105	146	86	84	37	5	24	22	11	7	3		+	+	+	+	+	655
70	2	15	31	26	45	60	14	94	148	96	121	120	7	23	25	13	11	10	+	1	1	1	1	1	864
65	2	12	29	29	46	67	11	80	128	93	104	118	6	24	23	9	13	12	1	1	+	+	+	+	808
60	1	10	22	30	43	46	11	74	118	82	84	99	5	34	27	10	15	17	1	1	1	1	2	1	735
55	1	9	23	27	36	41	8	77	113	70	78	97	5	36	34	13	15	19	1	2	1	1	1	1	710
50	+	10	24	20	32	34	5	70	126	61	67	87	4	35	29	14	15	23	1	2	2	1	1	1	663
45	1	11	27	24	29	34	3	71	140	71	64	77	4	46	43	9	15	23	1	4	3	1	1	1	701
40	1	9	29	25	32	35	3	67	159	73	60	81	3	47	60	12	17	33	1	4	2	1	2	3	758
35	+	10	32	30	39	34	1	61	192	88	74	75	2	48	58	15	16	31	1	5	4	1	1	2	818
30		8	35	27	33	29	2	70	164	63	45	49	2	42	50	6	6	15		4	3				654
25		4	18	12	15	6	2	52	100	26	16	6	2	29	32	2	4	4		3	2				335
20		4	9	3	4	4	1	31	64	10	6	1	2	18	20	4	3	2							189
15		1	7	2	2	1	1	17	30	7	3	+	1	13	12	1	2			1	2				100
10		1	2	1	+	+		6	10	1	1	1		4	4	+				+	+				32
05			1	+	1	+		1	2	+	+			3	+										9
TOTAL	14	152	351	292	384	408	91	892	1875	875	815	849	52	474	493	126	140	191	5	31	23	7	10	17	767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS 1941-50
	AM HOUR ENDING AT												PM HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	NOON	
TRAIL	24	25	26	27	26	27	30	30	33	32	31	26	29	29	28	28	27	25	26	27	27	25	26	25	59
01 IN	8	7	7	7	8	7	8	8	6	7	6	8	7	5	6	6	6	7	8	7	9	7	8	7	10
02 TO 09 IN	13	16	15	14	13	16	14	14	13	13	13	12	13	13	14	14	13	13	13	12	14	15	14	32	
10 TO 24 IN	5	5	5	5	6	5	5	3	3	2	3	3	3	3	3	4	3	3	4	4	3	4	4	25	
25 TO 49 IN	1	1	1	1	2	2	1	2	1	1	+	+	+	1	+	1	1	1	1	2	1	1	1	1	19
50 TO 99 IN	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	1	1	+	+	+	+	20
100 TO 199 IN				+								+				+		+	+	+					1
200 IN AND OVER																									1
TOTAL	51	53	54	54	54	56	58	57	57	55	54	50	52	52	51	53	51	50	52	53	52	51	54	52	75

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT
	0	100- 200	200- 400	400- 600	600- 1000	1000- 2000	2000- 4000	4000- 6000	Over 6000		
0 TO 1/8	+	+	+	+	+		+	+	+	1	
3/16 TO 3/8	+	+	+	+	+	+	+	+	+	+	
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1	
1 TO 2 1/2			+	1	2	1	+	+	+	3	
3 TO 6			+	+	3	3	1	2	3	8	
7 TO 15				+	1	2	2	5	7	16	
30 TO 39							+	+	+	28	
33 OR MORE										46	
TOTAL	+	1	2	6	6	3	7	10	66	100	

PHILADELPHIA, PENNA.
Int. Airport

CURRENCES:

WIND	25 MPH AND OVER						TOTAL OBS
	N	NE	E	SE	S	SW	
1							1
17							17
74							74
225							225
420							420
655							655
864							864
808							808
735							735
710							710
663							663
701							701
758							758
818							818
654							654
335							335
149							149
100							100
32							32
9							9
191	5	31	22	7	10	17	178767

1 divided by 10).
if sums exactly
n 0.5.

WIND AT	NO OF DAYS				
	27	27	25	26	25
27	27	27	25	26	25
7	7	9	7	6	7
13	12	14	15	14	32
4	3	4	4	4	25
2	1	1	1	1	19
1	1	1	1	1	20
1	1	1	1	1	8
53	52	51	54	52	175

1
+
1
8
2
2
2

PHILADELPHIA, PENNA.
Int. Airport

B-6

B PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED (IN MPH PER HOUR)																TOTAL	AV SPEED
	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15		
N	+		2	3	2	+											8	9.9
NNE	+		1	2	1	+											6	10.4
NE	+		1	1	1	+											3	11.3
ENE	+		1	2	2	+											6	12.0
E	+		1	2	1	+											4	10.3
ESE	+		1	1	+												3	8.4
SE	+		1	1	+												3	8.0
SSE	+		1	1	+												3	7.9
S	+		2	1	1	+											4	8.8
SSW	+		2	2	1	+											6	10.0
SW	+		2	4	2	+											8	9.7
WSW	+		3	5	2	+											11	9.7
W	+		2	2	1	+											6	9.6
WNW	+		2	3	2	1	+										8	11.6
NW	+		2	2	2	1	+										7	11.7
NNW	+		2	2	2	1	+										7	11.6
CALM	7																7	
TOTAL	11	27	35	21	5	1	+										100	9.6

E PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED IN MPH					RELATIVE HUMIDITY (%)						
	0	4	8	0	4	12	16	20	0	30	50	70	80	90	100
00	46	9	45	15	67	18	1	+	6	27	20	24	22		
01	44	10	45	16	67	17	+		6	26	19	25	25		
02	44	11	45	18	65	17	+		5	25	18	24	28		
03	43	10	46	19	64	16	1		4	23	18	24	31		
04	41	11	48	18	65	17	+	+	4	23	18	23	33		
05	37	13	50	19	63	18	+	+	3	22	18	23	34		
06	34	14	52	19	62	19	1	+	4	23	19	23	31		
07	33	14	53	15	63	21	1	+	5	29	19	22	25		
08	33	14	53	12	60	27	1	+	10	36	18	19	17		
09	33	16	51	11	57	31	1	+	19	39	15	14	13		
10	32	17	51	8	57	33	2	1	28	38	12	10	10		
11	30	20	50	7	54	37	2	3	35	36	10	8	8		
12	29	20	51	5	54	38	2	4	42	32	9	6	7		
13	27	20	53	5	52	41	2	6	45	29	7	6	7		
14	27	23	51	5	52	41	2	7	46	28	7	6	6		
15	27	22	51	5	51	41	2	7	47	27	6	6	7		
16	29	20	50	5	55	39	2	6	44	30	7	7	7		
17	33	19	48	5	61	32	1	4	36	36	8	7	8		
18	36	16	48	6	66	27	1	2	28	41	11	9	9		
19	38	15	47	6	70	23	1	1	20	42	15	11	10		
20	42	13	45	9	70	20	1	1	13	41	19	14	12		
21	44	12	44	10	70	19	1	+	10	36	22	17	14		
22	45	12	43	12	68	19	+	+	9	33	22	20	17		
23	46	10	44	14	67	19	1	+	0	29	22	23	19		
AVG	36	15	49	11	62	26	1	2	20	31	15	15	17		

B

TEMPERATURE AND WIND SPEED—RELATIVE HUMIDITY OCCURRENCES:

WIND SPEED KTS	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL OBS.	
	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS	WIND SPEED KTS		WIND SPEED KTS
14/100																										2
19/ 95																										23
14/ 90																										109
19/ 85																										263
14/ 80																										438
19/ 75																										655
14/ 70																										583
19/ 65																										794
14/ 60																										729
19/ 55																										696
14/ 50																										683
19/ 45																										673
14/ 40																										770
19/ 35																										755
14/ 30																										642
19/ 25																										328
14/ 20																										184
19/ 15																										89
14/ 10																										43
19/ 05																										7
14/ 00																										2
TOTAL	9	107	213	170	234	354	67	919	1013	967	1016	1102	67	507	565	134	136	190	6	62	50	6	9	19	5767	

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	
TRACE	24	24	24	24	23	27	25	30	29	20	24	24	25	26	24	24	23	22	23	23	25	26	25	25	52
01 IN	6	6	6	6	7	6	7	7	6	7	6	6	6	6	6	6	7	6	6	7	6	6	6	6	11
01 TO 09 IN	13	14	15	14	15	14	14	13	13	13	13	12	12	12	14	13	14	14	13	13	13	14	14	13	33
10 TO 39 IN	4	3	4	5	3	4	4	3	3	4	4	3	4	3	4	4	4	4	4	4	4	4	4	4	22
40 TO 99 IN	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	2	1	1	1	22
100 TO 199 IN	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	1	+	+	+	+	1	+	2	+	16
200 IN AND OVER																									8
TOTAL	50	48	49	49	45	53	55	53	54	52	49	49	47	49	49	51	50	50	50	47	51	51	51	51	167

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100-200	200-400	400-600	600-800	800-1000	1000-1200	1200-1500	OVER 1500	100
0 TO 1/8	+	+	+	+	+			+	+	1
3/16 TO 1/4	+	+	+	+	+			+	+	1
1/2 TO 3/4	+	+	+	+	+			+	+	1
1 TO 1 1/2	+	+	1	2	1	+	+	+	+	9
3 TO 6			+	2	2	1	1	2	2	18
7 TO 15			+		2	1	4	6	44	57
20 TO 29					+	+	1	1	15	17
35 OR ABOVE									+	+
TOTAL	+	1	2	4	4	3	6	10	69	100

WIND	TOTAL OBS
23	2
109	23
263	109
438	263
655	438
683	655
794	683
729	794
696	729
683	696
673	683
770	673
755	770
642	755
328	642
184	328
89	184
43	89
7	43
2	7
158767	2

B PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED (IN MPH PER HOUR)										AV SPEED
	0-3	4-7	8-13	14-18	19-24	25-31	32-36	37-44	45-54	TOTAL	
N	+	1	2	1	+	+				5	9.9
NNE	+	1	1	1	+	+	+			3	10.1
NE	+	1	2	1	+	+	+			5	10.5
ENE	+	1	2	1	+	+	+	+		5	10.9
E	+	1	2	1	+	+	+	+		5	9.3
ESE	+	1	1	+	+	+	+	+		3	8.8
SE	+	1	2	1	+	+	+	+		4	9.5
SSE	+	1	2	1	+	+	+	+		4	10.8
S	+	2	3	1	+	+	+	+		7	9.8
SSW	+	1	2	1	+	+	+	+		6	10.6
SW	+	2	3	1	+	+	+	+		8	9.9
WSW	+	2	3	1	+	+	+	+		6	9.9
W	+	2	4	2	1	+	+	+		9	11.2
WNW	+	2	3	3	2	1	+	+		11	13.3
NW	+	2	4	3	1	+	+	+		10	12.2
NNW	+	1	2	1	+	+	+	+		5	11.3
CALM	3									3	
TOTAL	7	24	39	27	6	2	+	+	+	100	10.4

E PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M.P.H.)				RELATIVE HUMIDITY (%)					
	0-3	4-7	8-10	0-3	4-12	13-24	25-31	0-29	30-49	50-69	70-79	80-89	90-100
00	49	11	40	8	72	19	1	+	5	25	18	25	26
01	49	11	40	9	72	19	1	+	4	24	16	25	28
02	48	11	41	9	71	19	1	+	4	22	16	24	32
03	49	9	42	9	72	18	1		3	21	18	24	33
04	46	11	43	9	71	19	1		3	20	18	25	35
05	43	13	44	10	71	18	1		2	20	17	25	36
06	39	14	47	10	71	18	1		2	21	18	25	34
07	37	14	49	9	69	21	1		3	25	19	24	29
08	37	14	49	10	63	26	1	+	7	34	20	19	20
09	38	15	47	9	57	32	2	1	16	40	16	13	15
10	37	17	46	7	55	36	3	2	27	39	12	9	12
11	33	20	47	6	51	40	3	2	35	36	10	7	10
12	31	22	46	5	51	41	3	4	40	33	8	6	8
13	31	22	47	5	49	42	4	6	43	31	7	6	7
14	31	23	47	4	46	44	4	7	43	30	7	5	7
15	33	22	45	4	48	44	4	8	42	30	7	5	6
16	36	18	46	4	52	41	3	7	40	31	8	7	8
17	35	16	45	4	59	35	2	5	33	36	9	7	9
18	41	15	44	5	65	28	1	3	26	40	13	9	11
19	42	14	43	6	68	25	1	1	20	41	15	12	12
20	45	13	41	7	68	24	1	+	14	37	19	16	14
21	48	13	40	7	69	22	1	+	9	34	20	19	17
22	48	11	40	7	71	20	1	+	8	30	20	22	20
23	49	11	40	8	71	20	1	+	6	28	19	24	23
AVG	41	15	44	7	63	28	2	2	16	30	15	16	19

BALTIMORE, MARYLAND
Friendship Int. Airpor

B-7

A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND SPEED MPH	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL OCC	
	WIND DIR	0-20	21-40	41-60	61-80	81-100	WIND DIR	0-20	21-40	41-60	61-80	81-100	WIND DIR	0-20	21-40	41-60	61-80	81-100	WIND DIR	0-20	21-40	41-60	61-80	81-100		
104/100																										1
99/ 99	+	2	+				1	12	1				+	3												1
94/ 90	+	9	6	+			1	40	52	+			+	10	12											126
89/ 89	+	10	31	4			1	47	136	17			+	1	12	32										297
84/ 80	+	10	34	27	11		3	54	161	104	34	1	1	21	34	17										524
79/ 79	+	10	28	33	58	61	5	56	154	122	142	79	2	19	54	30	24	10	+	1	1	1	1	1	4	914
74/ 70	1	7	24	32	73	149	5	47	137	108	157	138	3	19	63	44	35	18	+	2	2	2	2	2	2	1079
69/ 65	1	7	20	29	62	94	4	49	123	90	114	102	5	29	59	38	52	29	+	2	2	2	2	2	2	920
64/ 60	1	6	15	22	51	67	5	54	103	77	99	103	3	28	51	36	38	41	+	2	2	2	2	2	2	820
59/ 55	+	7	14	20	33	60	5	59	103	74	96	97	5	33	54	29	33	30	1	2	2	2	2	2	2	757
54/ 50	1	7	19	16	34	41	4	64	115	60	71	77	3	36	44	19	24	21	+	2	2	2	2	2	2	668
49/ 45	+	7	23	23	32	48	2	59	134	66	70	75	3	44	54	19	22	20	+	2	2	2	2	2	2	724
44/ 40	1	5	27	29	30	40	3	44	139	70	72	69	2	42	61	21	24	39	+	2	2	2	2	2	2	727
39/ 35	+	6	23	29	27	34	+	33	114	58	48	39	+	33	56	13	15	20		2	2	2	2	2	2	558
34/ 30	+	9	17	17	21	19	+	27	78	32	25	17	+	26	50	9	6	12		2	2	2	2	2	2	371
29/ 25	1	12	10	12	8			17	33	10	5	1	1	22	26	6	3	2	+	1	1	1	1	1	1	175
24/ 20		4	4	5	1			4	13	5	2	+	+	11	8	1	+		+	1	1	1	1	1	1	61
19/ 15		1	2	1				1	1	1	1			3	2				+	1	1	1	1	1	1	14
14/ 10														1												1
TOTAL	6	97	304	298	454	623	39	662	1598	894	944	863	28	394	669	283	290	245	3	24	31	14	15	66	3767	

In Table A occurrences are for the average year (10-year total divided by 10).
In Table C occurrences are for the average year (5-year total divided by 5).
Values are rounded to the nearest whole number, but not adjusted to make their
sums exactly equal to column or row totals. "+" indicates more than 0 but
less than 0.5.

C 1/56 - 12/60 OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO. OF DAYS
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	1200	1	2	3	4	5	6	7	8	9	10	11	12	
TRACE	26	36	26	23	23	23	25	24	27	24	24	27	25	23	22	24	25	24	24	26	26	26	27	27	47
01 IN	9	6	6	5	5	5	5	4	6	6	5	7	7	7	7	7	6	5	6	5	6	6	7	7	11
02 TO 05 IN	11	11	12	13	17	14	14	12	12	11	12	12	13	11	14	14	15	13	12	12	11	12	13	15	33
10 TO 24 IN	2	2	4	5	3	3	3	4	3	4	3	3	4	3	5	5	5	4	4	4	5	5	5	5	23
25 TO 40 IN	1	1	2	1	2	1	1	1	2	1	1	1	1	1	2	2	3	1	2	1	2	1	1	1	20
50 TO 99 IN		1	+	+			1	+		1			2	+	1	+	1	+	1	1	+	+	+	+	17
100 TO 199 IN	+			1												1	+	+		1	+				11
200 IN AND OVER																									3
TOTAL	52	52	52	53	49	49	49	49	49	47	46	50	47	46	50	53	53	53	52	52	52	51	52	166	

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT.
	0	100-123	200-299	300-599	600-999	1000-1999	2000-2999	3000-4999	5000-9999	OVER 9999	
0 TO 1/8	.2	.2	+	+	+	+		+		.1	.6
3/8 TO 3/4	+	.3	+	+				+		.1	.4
1/2 TO 3/4		.5	.2	.1	+			+		.1	.8
1 TO 2 1/2		.5	.9	1.0	.3	.1	.2	.2	1.2	.4	4.2
3 TO 6		.1	.7	3.0	2.1	1.0	1.5	2.4	3.8	1.3	18.8
7 TO 15		+	+	.5	2.3	1.9	3.7	5.5	1.0	3.3	15.3
20 TO 30											
35 OR MORE											
TOTAL	.2	1.1	1.2	4.9	4.7	3.1	5.4	8.0	7.0	6.6	100

NORFOLK, VIRGINIA
Municipal Airport

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR. SPEED	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL OBS.
	0-4 S.W.	0-4 S.E.	0-4 E.	0-4 N.E.	0-4 N.	0-4 S.W.	5-14 S.W.	5-14 S.E.	5-14 E.	5-14 N.E.	5-14 N.	5-14 S.W.	15-24 S.W.	15-24 S.E.	15-24 E.	15-24 N.E.	15-24 N.	15-24 S.W.	25 S.W.	25 S.E.	25 E.	25 N.E.	25 N.	25 S.W.	
1/100							1	1																	2
1/ 95	+	4	+				1	15	2																30
1/ 90		13	14				4	71	80				1	11	14										208
1/ 85	+	1	4	4			6	69	261	41	2		2	19	63	10	1		+	+		+			536
1/ 80	1	1	9	20	30	25	6	65	170	179	109	8	3	20	58	33	7	+	+	+	1	1	1	1	750
1/ 75	1	6	13	20	92	167	6	47	122	114	272	312	5	15	48	45	35	13	+	+	2	3	2	1	1341
1/ 70	3	6	9	15	48	228	16	53	96	88	171	456	7	25	37	33	47	64	1	+	1	3	4	1	61411
1/ 65	3	7	9	11	27	92	17	53	86	80	123	318	11	30	34	25	34	69	1	1	2	2	1	1	51038
1/ 60	3	8	8	8	18	71	15	56	95	67	97	261	9	35	28	20	31	46	+	1	2	1	1	1	882
1/ 55	2	7	11	10	18	44	11	57	96	65	85	152	11	29	28	18	21	28	+	1	1	1	1	1	698
1/ 50	1	6	11	10	18	28	10	49	107	60	73	102	10	27	35	17	18	20	+	1	2	1	+	1	506
1/ 45	1	4	11	14	18	17	5	39	93	64	66	56	5	22	31	17	17	18	1	3	2	2	1	1	377
1/ 40	+	2	7	8	16	14	3	28	70	52	51	22	2	20	29	18	17	9	+	2	3	1	1	+	214
1/ 35		2	4	7	10	8	1	15	46	32	27	10	1	9	15	10	7	7	+	1	2	1	1	+	109
1/ 30			2	4	3	3	+	9	31	15	11	4	+	7	11	4	1	1		+	1	1	+	+	49
1/ 25																									7
1/ 20			2	3	2	+		3	16	5	1	+		2	7	2	1	+			+	+	+	+	3
1/ 15			+							1	+			+	1	+	+				+	+	+	+	7
ITAL	16	67	165	147	297	675	102	633	1374	866	1090	1697	67	273	439	250	237	274	4	10	19	18	13	17	767

In Table A, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C

OCCURRENCES OF PRECIPITATION AMOUNTS:

DATA NOT AVAILABLE

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT
	0	100-200	200-400	400-600	600-800	800-1000	1000-1500	1500-2000	2000-3000	OVER 3000	
0 TO 1/8	+	+	+	+	+	+	+	+	+	+	1
3/16 TO 3/8	+	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	+	1
1 TO 2 1/2										1	2
3 TO 4										4	9
7 TO 15	+	+	+	3	4	4	5	4	66		87
20 TO 30											
35 OR MORE											
TOTAL	+	2	2	5	5	5	6	5	71		100

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23 M.P.H. AND OVER						TOTAL OAS.
10-15	16-20	21-25	26-30	31-35	36-40	
						2
						30
						208
						536
						750
						13341
						61411
						50338
						1 882
						1 698
						1 609
						1 506
						377
						214
						109
						49
						7
						363

**B PERCENTAGE FREQUENCIES
OF WIND DIRECTION AND SPEED:**

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED (IN AMPS PER HOUR)										AV SPEED
	0-3	4-7	8-12	13-15	16-24	25-31	32-38	39-44	47 OVER	TOTAL	
N	+	2		3	2	+	+	+		11	12.3
NNE	+	1	2	1	+	+	+	+		6	10.5
NE	+	3	4	1	+	+	+			8	9.3
ENE	+	1	2	1	+	+	+			4	9.6
E	+	2	3	1	+	+				6	9.7
ESE	+	1	1	1	+	+	+	+		3	10.6
SE	+	2	3	1	+	+	+			7	10.0
SSE	+	2	3	1	+	+				7	9.7
S	+	3	3	2	1	+	+	+	+	10	10.5
SSW	+	1	2	2	1	+	+			6	12.3
SW	+	2	2	1	+	+	+	+		6	10.1
WSW	+	1	1	+	+	+	+			3	9.5
W	+	2	2	1	+	+	+			5	8.9
WNW	+	1	1	1	+	+	+			3	10.2
NW	+	2	2	1	1	+	+	+		6	11.0
NNW	+	1	2	1	1	+	+			5	12.5
CALM	5									5	
TOTAL	7	28	38	20	6	1	+	+	+	100	10.0

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M.P.H.)				RELATIVE HUMIDITY (%)					
	0-3	4-7	8-10	0-3	4-12	13-24	25-8	0-29	30-49	50-69	70-79	80-89	90-100
								OVER					
00	54	12	34	11	73	15	+	+	3	12	11	22	52
01	53	13	35	11	73	15	1		2	11	11	20	55
02	51	13	36	12	72	15	+		2	10	11	19	57
03	49	14	37	11	73	15	1		1	10	11	19	59
04	49	13	38	11	72	17	+		1	10	11	19	59
05	44	16	40	11	73	15	1		1	9	11	19	60
06	40	17	43	8	75	16	1		1	10	12	23	53
07	39	17	44	5	71	23	+		2	15	18	31	33
08	37	19	44	4	63	22	1	+	7	25	26	22	19
09	36	20	44	4	56	37	1	1	15	37	23	14	12
10	34	23	43	4	58	39	2	2	21	42	16	10	8
11	31	25	44	4	55	40	2	4	26	42	13	8	7
12	29	26	45	3	53	42	2	7	29	39	11	8	6
13	28	27	45	3	50	45	2	8	31	36	11	8	6
14	29	26	45	3	50	45	2	9	30	34	11	8	7
15	31	24	45	2	49	47	2	9	28	33	12	9	8
16	34	22	44	2	53	43	1	7	25	33	15	12	8
17	36	19	45	3	65	32	1	2	18	33	18	16	12
18	38	18	44	4	75	20	+	1	11	28	22	22	16
19	42	17	41	9	77	16	+	+	6	20	21	28	25
20	45	17	38	9	75	15	1	+	5	16	16	30	33
21	48	16	36	10	74	16	+	+	4	14	14	29	39
22	51	15	34	12	73	15	+	+	3	13	13	27	44
23	53	14	34	12	71	16	+	+	3	13	12	25	48
AVG	41	18	41	7	66	26	1	2	11	23	15	19	30

MOBILE
Bates |

TEMPERATURE AND WIND SPEED—RELATIVE HUMIDITY OCCURRENCES:

WD	0-4 MPH						5-9 MPH						10-14 MPH						15-19 MPH AND OVER						TOTAL
	1	2	3	4	5	6	1	2	3	4	5	6	1	2	3	4	5	6	1	2	3	4	5	6	
100																									12
95	+	1					+	7	3																229
90	+	6	11				1	57	138																620
85	+	5	31	11			1	60	341																979
80	+	4	21	51	70		2	43	206	237	180														1671
75	+	3	17	33	180	300	4	43	146	134	305	302													189
70	1	5	15	20	76	197	8	46	105	98	186	238													987
65	1	7	12	18	55	129	7	58	91	75	131	252													850
60	1	6	16	15	50	100	6	57	98	70	117	185													692
55	1	7	17	21	43	66	4	45	94	64	82	109													621
50	+	5	19	20	45	46	2	39	87	61	68	78													449
45	1	4	12	19	40	32	1	29	61	45	46	31													282
40	+	3	7	13	31	20	+	15	40	25	27	12													128
35		1	6	8	12	12		7	23	13	7	3													47
30			2	3	6	6		2	7	4	2	1													9
25																									2
20																									+
15																									
TOTAL	5	58	185	232	613	917	36	507	440	911	1157	1227	21	235	529	232	198	170	2	13	33	18	16	118	767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								TOTAL
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	END	
TRACE	16	14	16	18	16	17	20	18	17	18	20	22	27	26	27	24	22	21	22	19	17	17	16	14	50
01 IN	4	4	5	3	4	4	2	3	3	4	4	6	5	4	7	7	6	6	5	4	4	2	4	4	11
02 TO 09 IN	6	5	6	6	6	6	6	7	8	9	10	11	12	12	13	13	11	10	9	9	8	7	7	8	28
10 TO 24 IN	2	3	2	3	3	3	3	3	3	4	3	4	5	6	5	5	5	4	3	4	2	2	3	2	19
25 TO 49 IN	1	1	2	1	2	1	1	2	2	2	2	3	2	2	3	2	1	2	2	1	1	1	1	1	18
50 TO 99 IN	+	1	1	1	+	1	1	+	1	1	1	1	2	1	1	1	1	1	1	1	+	1	1	1	18
100 TO 199 IN													1	1											5
200 IN AND OVER																									5
TOTAL	29	28	31	31	32	31	33	32	33	37	41	48	52	52	55	51	47	45	41	37	33	30	31	29	60

D PERCENTAGE FREQUENCIES OF CEILING—VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100-300	300-499	500-999	1000-1499	1500-2499	2500-4999	5000-9999	OV9999	TOTAL
0 TO 1/8	+	+	+	+	+	+	+	+	+	1
3/8 TO 1/2	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1
1 TO 2 1/2	+	+	1	+	+	+	+	+	1	2
3 TO 6				1	1	2	2	1	6	8
7 TO 15			+	+	2	4	3	4	72	88
20 TO 30										
35 OR MORE										
TOTAL	+	1	1	3	5	5	4	5	77	100

NEW ORLEANS, LA.
Moisant Int. Airport

DITY OCCURRENCES:

25 MPH AND OVER										TOTAL
1	2	3	4	5	6	7	8	9	10	
7	+					1	+			12
40	11	+				2	2	+		229
46	40	18				3	5	4		620
33	37	34	+			1	2	2	4	979
17	25	32	+			1	2	1	1	1671
15	17	22	1			2	3	1	1	189
15	17	22	+			3	3	1	1	987
19	19	21	+			2	4	1	2	850
18	14	11				2	5	2	1	692
15	11	7	+			2	5	2	1	621
5	4	2				1	3	1	1	449
1	2	1				+	1	+		282
1	1									128
+										47
										9
										2
										+
232	198	170	2	13	33	18	16	11	7	767

ear total divided by 10).
make their sums exactly
less than 0.5.

OUNTS:

OF THE DAY										NO. OF DAYS
1	2	3	4	5	6	7	8	9	10	
22	21	22	19	17	17	16	14	11	50	
7	6	6	5	4	4	2	4	4	11	
3	11	10	9	9	8	2	7	8	28	
5	5	4	3	4	2	2	3	2	19	
2	1	2	2	1	1	1	+	1	18	
1	1	1	1	1	+	1	1	1	18	
+	+	+	+	+	+	+	+	+	12	
+	+	+	+	+	+	+	+	+	5	
1	47	45	41	37	33	30	31	29	160	

OF

NO.	OVER	NO.
+	+	1
+	+	1
+	+	1
+	1	2
1	4	8
4	72	88
9	77	100

NEW ORLEANS, LA.
Moisant Int. Airport

B-10

PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

WIND DIRECTION	WIND SPEED (M.P.H.)															
	0-3	4-7	8-10	11-14	15-18	19-24	25-30	31-36	37-42	43-48	49-54	55-60	61-66	67-72	73-78	79-84
N	+	1	2	2	1	+	+	+								6
NNE	+	1	2	2	1	+	+	+								6
NCE	+	2	3	2	+	+	+	+								8
ENE	+	2	3	2	+	+	+	+								8
E	+	2	7	1	+	+	+	+								6
ESE	+	2	1	1	+	+	+	+								4
SE	+	2	2	1	+	+	+	+								5
SSE	+	3	3	2	+	+	+	+								8
S	+	3	3	2	+	+	+	+								9
SSW	+	2	3	1	+	+	+	+								7
SW	+	2	1	1	+	+	+	+								4
WSW	+	1	1	+	+	+	+	+								3
W	+	1	1	+	+	+	+	+								3
WNW	+	1	1	1	+	+	+	+								3
INW	+	1	1	1	+	+	+	+								4
INNW	+	1	2	2	1	+	+	+								6
CALM	12															12
TOTAL	16	27	32	19	5	1	+	+	+	+	+	+	+	+	+	100

PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M.P.H.)				RELATIVE HUMIDITY (%)							
	0-3	4-7	8-10	0-3	4-12	13-24	25-30	0-29	30-49	50-69	70-79	80-89	90-99	100	
00	55	13	32	24	60	15	1		2	10	11	33	44		
01	55	13	32	29	56	14	1	+	2	10	8	31	50		
02	53	12	34	31	54	14	1		2	9	8	27	54		
03	52	13	35	33	52	14	1		1	9	8	25	57		
04	51	13	36	34	51	14	1		1	8	8	23	60		
05	47	15	38	34	51	14	1		1	8	8	23	60		
06	43	17	41	30	54	15	1		1	8	9	25	57		
07	42	17	41	18	63	10	1		1	11	16	38	34		
08	40	19	41	9	63	27	1		3	20	30	27	20		
09	38	21	41	5	59	35	1	+	7	36	29	17	12		
10	37	23	40	3	57	39	1	+	11	48	21	11	8		
11	37	23	40	2	55	41	2		1	16	52	15	9	7	
12	37	22	40	2	53	43	2		1	20	51	13	8	6	
13	36	23	41	2	53	43	2		2	25	47	12	9	5	
14	36	21	42	3	55	41	2		3	27	43	12	9	6	
15	36	21	44	2	59	37	1		4	27	43	12	9	6	
16	36	19	45	4	62	33	1		3	25	40	15	10	7	
17	36	19	45	8	66	25	1		1	19	38	21	14	8	
18	38	18	44	13	68	18	1		1	12	35	25	19	9	
19	42	18	40	17	68	14	1	+	5	25	28	27	15		
20	47	17	36	19	65	15	1	+	4	16	25	35	20		
21	51	15	35	20	64	15	1	+	4	12	19	39	26		
22	53	15	33	20	64	16	1		3	11	16	40	31		
23	54	14	32	22	63	15	1	+	3	10	13	37	37		
AVG	44	17	39	16	59	24	1	1	9	25	16	23	27		

TEMPERATURE AND WIND SPEED--RELATIVE HUMIDITY OCCURRENCES:

RELATIVE HUMIDITY (%)	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL OCC.
	0-4	5-14	15-24	25	26-35	36-45	0-4	5-14	15-24	25	26-35	36-45	0-4	5-14	15-24	25	26-35	36-45	0-4	5-14	15-24	25	26-35	36-45	
100	+						1						+												1
95	+	7					36	3					8	1											36
90	+	15	15				74	106					28	83											327
85	1	10	30	4	+		54	253	55	2			27	197	23	1			+	1	9	3			677
80	1	6	17	25	35	7	42	135	186	196	21		25	117	71	25	2		1	1	15	9	2		949
75	1	4	10	17	87	145	11	34	87	101	362	400	7	26	99	70	34	1	2	14	14	12			1611
70	2	5	8	11	27	79	16	39	64	69	149	313	10	32	64	55	89	96	2	3	13	8	9		172
65	2	6	6	5	16	49	16	44	67	55	120	294	12	36	49	29	55	100	2	3	4	3	4		980
60	2	6	7	5	10	41	13	48	68	52	102	218	10	44	40	22	30	43	1	4	3	1	1		772
55	2	7	5	4	8	26	9	55	70	48	88	166	7	42	47	19	29	34	2	6	4	2	1		681
50	1	5	7	5	8	17	5	43	84	46	71	107	4	32	45	22	23	31	1	4	5	2	1		570
45	1	2	6	5	7	12	3	31	78	52	58	57	2	22	42	26	21	16	1	3	5	2	1		452
40		2	4	4	6	5	2	18	50	42	37	33	1	13	24	18	14	13	+	2	1	1	2		291
35	+		2	1	2	3		6	22	17	22	15	+	6	11	8	7	15		1	2	+	+		141
30			1	1	1	1		2	12	8	9	6		4	6	2	4	6		1	1	+	+		64
25									1					1											18
20																									4
15																									2
TOTAL	13	76	117	88	209	384	91	527	103	733	1216	1633	58	343	828	366	369	391	10	31	77	44	34	26	1767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES		FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO. OF DAYS WITHIN MONTH
		A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
		1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	12	
TRACE		14	15	15	15	17	15	19	23	20	16	21	25	27	25	23	19	19	16	15	14	15	15	13	14	53
01 IN		4	5	4	5	5	5	3	4	4	4	5	5	6	6	7	6	0	4	4	3	3	4	4	4	10
02 TO 09 IN		5	5	6	6	7	7	7	7	9	9	8	9	11	11	11	10	10	9	7	6	6	5	6	6	29
10 TO 24 IN		2	2	3	3	3	2	2	3	3	3	4	3	4	4	4	4	2	2	3	3	2	2	2	19	
25 TO 49 IN		+	1	1	1	1	1	2	1	1	1	1	1	2	1	2	2	1	+	1	1	+	1	1	1	15
50 TO 94 IN		+	+	+	+	1	1	1	1	1	+	1	1	1	1	1	1	1	+	+	+	+	+	+	+	13
100 TO 149 IN					+	+		+		+			+		+	+	1	+		1						8
150 IN AND OVER																										4
TOTAL		26	28	29	31	33	31	34	39	37	36	39	44	50	48	46	44	41	35	29	27	27	25	26	27	151

City Office Data

Table C data obtained from tipping bucket rain gage located at the Federal Bldg., Franklin and Fannin Streets (Houston City Office), at an elevation of 152 feet.

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100-200	200-400	400-600	600-1000	1000-2000	2000-4000	4000-7000	OVER 7000	TOT
0 TO 1/8	+	+	+	+	+	+	+	+	+	1
3/16 TO 3/8	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1
1 TO 1 1/2				1	1	+	+	+	+	4
3 TO 4				1	2	1	1	1	5	10
7 TO 15		+	+	2	5	5	7	5	59	84
20 TO 30										
35 OR MORE										+
TOTAL	+	1	2	5	6	6	9	6	66	100

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR SPEED (MPH)	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL OBS	
	SEAS	SW	NE	SE	SW	NE	SEAS	SW	NE	SE	SW	NE	SEAS	SW	NE	SE	SW	NE	SEAS	SW	NE	SE	SW	NE		
7/ 45																										62
7/ 90																										849
7/ 85																										1763
7/ 80																										1144
7/ 75																										1006
7/ 70																										1042
7/ 65																										1000
7/ 60																										717
7/ 55																										557
7/ 50																										336
7/ 45																										178
7/ 40																										77
7/ 35																										27
7/ 30																										6
7/ 25																										2
7/ 20																										1
7/ 15																										1
TOTAL	4	19	94	125	153	123	7	204	1213	1430	1474	1213	13	164	594	601	643	443	5	44	71	42	40	66	3767	

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole number, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS WITH
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	NO.	
TRACE	10	11	10	12	12	16	17	15	25	22	22	21	18	17	15	18	18	16	16	14	15	13	12	11	41
01 IN	4	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	3	4	4	4	4	4	9
02 TO 10 IN	5	4	5	6	8	7	9	10	8	8	9	8	6	7	6	7	6	5	5	4	4	4	4	4	24
10 TO 24 IN	2	2	3	3	3	3	2	4	3	3	3	3	3	2	3	2	2	1	1	2	2	1	2	1	18
25 TO 49 IN	1	1	1	1	1	1	2	1	1	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	15
50 TO 100 IN	+	+	1	+	+	1	+	1	1	+	1	+	+	+	+	1	+	+	+	+	+	+	+	+	13
100 TO 149 IN	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	7
150 IN AND OVER	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	2
TOTAL	22	22	23	26	29	32	35	39	43	41	38	37	33	32	29	31	31	27	26	24	24	23	21	26	266

*City Office

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY MILES	CEILING (FEET)									
	0	100-200	200-400	400-600	600-1000	1000-2000	2000-4000	4000-7000	OVER 7000	TOT
0 TO 1/8	.2	.3	+	+	+	+	+	+	+	.7
3/16 TO 1/4	.1	.3	+	+	+	+	+	+	+	.8
1/2 TO 3/4	+	.2	.1	+	.1	+	+	+	+	.7
1 TO 2 1/2	+	.3	.3	.2	.2	.1	.1	.1	.1	1.7
3 TO 6	.2	.2	.1	.1	.1	.1	.1	.1	.1	7.2
7 TO 15		.1	.4	2.0	5.3	3.4	3.7	4.6	5.8	38.8
20 TO 30										
35 OR MORE										+
TOTAL	.5	1.5	1.5	4.5	6.6	4.1	4.4	5.2	7.2	100

GALVESTON, TEXAS
Municipal Airport

DITY OCCURRENCES:

MPH			25 MPH AND OVER								TOTAL OBS
F	E	S	SE	SW	W	WNW	WSW	W	WNW	WSW	
1	15	+	+	1	2	+	649				62
121	148	10	1	1	2	5	1763				1
63	130	47	+	1	2	5	1144				1
52	88	83	1	4	3	3	1006				1
44	77	98	+	4	5	5	1042				1
45	57	84	+	8	7	4	1000				1
33	45	45	+	8	15	4	717				1
36	37	31	1	8	12	7	557				1
26	21	15	1	5	13	8	336				1
18	14	12	1	3	8	4	176				1
7	9	6	+	1	4	2	77				1
2	1	4		1	1	1	27				1
1	+	1					6				1
1	+						2				1
+	+						1				1
601	643	443	5	46	71	42	46	46	3767		

10-year total divided by 10).
adjusted to make their sums
e than 0 but less than 0.5.

OUNTS:

R OF THE DAY											NO OF EYES DOWN
P M HOUR ENDING AT											
1	2	3	4	5	6	7	8	9	10	11	
8	10	16	16	14	15	13	12	11	41		
4	4	3	3	4	3	4	4	4	9		
7	6	5	5	4	4	4	6	4	24		
2	2	1	1	2	2	2	1	2	18		
1	1	1	1	1	1	+	+	+	15		
1	+	+	+	+	+	+	+	+	13		
1	+	+							7		
1	31	27	26	24	24	24	23	21	126		

OF

NO	OVER	TOT
+	.2	.7
+	.2	.8
+	.2	.7
+	.3	1.7
+	2.7	7.2
+	4.8	10.8
+	+	+
+	272.3	100

GALVESTON, TEXAS
Municipal Airport

B-12

PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED (IN MPH PER HOUR)												TOTAL	%
	0-3	4-7	8-12	13-18	19-24	25-31	32-38	39-46	47-54	55-62	63-70	71-78		
N	.2	.8	1.7	2.0	1.3	.5	.1	+	+	+	+	+	6.7	13
NNE	.1	.6	1.7	1.8	1.0	.3	.1	+	+	+	+	+	5.6	14
NE	.2	.8	2.2	1.9	.6	.2	+	+	+	+	+	+	5.9	12
ENE	.1	.6	1.4	1.3	.5	.1	+	+	+	+	+	+	4.0	12
E	.2	.9	2.2	1.9	.6	.1	+	+	+	+	+	+	5.9	12
ESE	.1	1.1	3.7	3.3	.6	.1	+	+	+	+	+	+	8.9	12
SE	.2	1.7	6.0	4.0	.6	.1	+	+	+	+	+	+	12.3	11
SSE	.1	1.4	6.1	4.9	.6	+	+	+	+	+	+	+	13.2	12
S	.3	1.6	6.1	5.1	.9	.1	+	+	+	+	+	+	14.0	12
SSW	.1	.7	2.4	2.5	.7	.1	+	+	+	+	+	+	6.4	12
SW	.2	.7	1.5	1.1	.4	.1	+	+	+	+	+	+	4.1	11
WSW	.1	.5	.8	.3	.1	+	+	+	+	+	+	+	1.8	9
W	.1	.9	.7	.3	.1	+	+	+	+	+	+	+	1.6	10
WNW	.1	.4	.8	.5	.2	.1	+	+	+	+	+	+	2.1	12
NW	.1	.9	.9	.8	.5	.2	+	+	+	+	+	+	3.1	13
NNW	.1	.3	.7	.8	.7	.4	.1	+	+	+	+	+	3.0	16
CALM	1.1												1.1	
TOTAL	3.5	12.6	39.0	32.5	9.5	2.3	.5	.1	+	+	+	+	100	12

PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M.P.H.)				RELATIVE HUMIDITY (%)							
	0-3	4-7	8-10	0-3	4-12	13-24	25-31	0-29	30-49	50-69	70-79	80-89	90-99	100	
00	49	18	33	4	57	36	3	+	2	14	25	31	28		
01	48	19	33	5	56	36	3	+	2	14	23	32	29		
02	47	19	34	6	56	35	3	+	2	13	23	32	30		
03	45	19	36	6	58	34	3	+	1	13	22	33	31		
04	45	19	36	6	58	33	3	+	1	12	22	33	33		
05	40	22	38	6	59	32	3	+	1	11	19	35	34		
06	35	23	42	6	58	33	3	+	1	11	20	35	34		
07	33	22	44	6	55	36	3	+	1	12	25	33	29		
08	33	24	44	4	51	42	3	+	2	18	28	30	23		
09	31	25	44	2	48	46	3	+	4	25	29	25	17		
10	31	26	44	2	45	50	3	+	6	31	29	22	12		
11	32	25	43	2	43	53	3	+	7	35	28	20	9		
12	33	24	43	1	41	55	3	+	1	9	36	27	19	8	
13	34	24	42	1	40	56	3	+	1	10	37	26	18	8	
14	35	23	42	1	40	56	3	+	1	11	38	24	19	7	
15	37	20	43	1	42	55	3	+	1	12	36	25	19	8	
16	38	19	43	1	45	51	3	+	1	10	35	24	19	10	
17	38	18	46	2	51	45	3	+	1	9	31	25	20	14	
18	37	19	44	2	54	41	2	+	7	27	27	21	17		
19	39	20	41	4	57	37	3	+	5	22	27	25	21		
20	42	20	38	4	57	36	2	+	4	20	26	28	22		
21	45	20	34	4	58	35	2	+	3	18	26	29	24		
22	47	20	33	4	57	37	3	+	3	16	26	29	26		
23	48	19	33	5	56	36	3	+	3	16	25	30	27		
AVG	39	21	40	3	52	42	3	+	5	22	25	26	21		

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND SPEED MPH	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL CUA																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
	0-4 MPH	5-9 MPH	10-14 MPH	15-19 MPH	20-24 MPH	25-29 MPH	30-34 MPH	35-39 MPH	40-44 MPH	45-49 MPH	50-54 MPH	55-59 MPH	60-64 MPH	65-69 MPH	70-74 MPH	75-79 MPH	80-84 MPH	85-89 MPH	90-94 MPH	95-99 MPH	100-104 MPH	105-109 MPH	110-114 MPH	115-119 MPH		120-124 MPH	125-129 MPH	130-134 MPH	135-139 MPH	140-144 MPH	145-149 MPH	150-154 MPH	155-159 MPH	160-164 MPH	165-169 MPH	170-174 MPH	175-179 MPH	180-184 MPH	185-189 MPH	190-194 MPH	195-199 MPH	200-204 MPH	205-209 MPH	210-214 MPH	215-219 MPH	220-224 MPH	225-229 MPH	230-234 MPH	235-239 MPH	240-244 MPH	245-249 MPH	250-254 MPH	255-259 MPH	260-264 MPH	265-269 MPH	270-274 MPH	275-279 MPH	280-284 MPH	285-289 MPH	290-294 MPH	295-299 MPH	300-304 MPH	305-309 MPH	310-314 MPH	315-319 MPH	320-324 MPH	325-329 MPH	330-334 MPH	335-339 MPH	340-344 MPH	345-349 MPH	350-354 MPH	355-359 MPH	360-364 MPH	365-369 MPH	370-374 MPH	375-379 MPH	380-384 MPH	385-389 MPH	390-394 MPH	395-399 MPH	400-404 MPH	405-409 MPH	410-414 MPH	415-419 MPH	420-424 MPH	425-429 MPH	430-434 MPH	435-439 MPH	440-444 MPH	445-449 MPH	450-454 MPH	455-459 MPH	460-464 MPH	465-469 MPH	470-474 MPH	475-479 MPH	480-484 MPH	485-489 MPH	490-494 MPH	495-499 MPH	500-504 MPH	505-509 MPH	510-514 MPH	515-519 MPH	520-524 MPH	525-529 MPH	530-534 MPH	535-539 MPH	540-544 MPH	545-549 MPH	550-554 MPH	555-559 MPH	560-564 MPH	565-569 MPH	570-574 MPH	575-579 MPH	580-584 MPH	585-589 MPH	590-594 MPH	595-599 MPH	600-604 MPH	605-609 MPH	610-614 MPH	615-619 MPH	620-624 MPH	625-629 MPH	630-634 MPH	635-639 MPH	640-644 MPH	645-649 MPH	650-654 MPH	655-659 MPH	660-664 MPH	665-669 MPH	670-674 MPH	675-679 MPH	680-684 MPH	685-689 MPH	690-694 MPH	695-699 MPH	700-704 MPH	705-709 MPH	710-714 MPH	715-719 MPH	720-724 MPH	725-729 MPH	730-734 MPH	735-739 MPH	740-744 MPH	745-749 MPH	750-754 MPH	755-759 MPH	760-764 MPH	765-769 MPH	770-774 MPH	775-779 MPH	780-784 MPH	785-789 MPH	790-794 MPH	795-799 MPH	800-804 MPH	805-809 MPH	810-814 MPH	815-819 MPH	820-824 MPH	825-829 MPH	830-834 MPH	835-839 MPH	840-844 MPH	845-849 MPH	850-854 MPH	855-859 MPH	860-864 MPH	865-869 MPH	870-874 MPH	875-879 MPH	880-884 MPH	885-889 MPH	890-894 MPH	895-899 MPH	900-904 MPH	905-909 MPH	910-914 MPH	915-919 MPH	920-924 MPH	925-929 MPH	930-934 MPH	935-939 MPH	940-944 MPH	945-949 MPH	950-954 MPH	955-959 MPH	960-964 MPH	965-969 MPH	970-974 MPH	975-979 MPH	980-984 MPH	985-989 MPH	990-994 MPH	995-999 MPH	1000-1004 MPH	1005-1009 MPH	1010-1014 MPH	1015-1019 MPH	1020-1024 MPH	1025-1029 MPH	1030-1034 MPH	1035-1039 MPH	1040-1044 MPH	1045-1049 MPH	1050-1054 MPH	1055-1059 MPH	1060-1064 MPH	1065-1069 MPH	1070-1074 MPH	1075-1079 MPH	1080-1084 MPH	1085-1089 MPH	1090-1094 MPH	1095-1099 MPH	1100-1104 MPH	1105-1109 MPH	1110-1114 MPH	1115-1119 MPH	1120-1124 MPH	1125-1129 MPH	1130-1134 MPH	1135-1139 MPH	1140-1144 MPH	1145-1149 MPH	1150-1154 MPH	1155-1159 MPH	1160-1164 MPH	1165-1169 MPH	1170-1174 MPH	1175-1179 MPH	1180-1184 MPH	1185-1189 MPH	1190-1194 MPH	1195-1199 MPH	1200-1204 MPH	1205-1209 MPH	1210-1214 MPH	1215-1219 MPH	1220-1224 MPH	1225-1229 MPH	1230-1234 MPH	1235-1239 MPH	1240-1244 MPH	1245-1249 MPH	1250-1254 MPH	1255-1259 MPH	1260-1264 MPH	1265-1269 MPH	1270-1274 MPH	1275-1279 MPH	1280-1284 MPH	1285-1289 MPH	1290-1294 MPH	1295-1299 MPH	1300-1304 MPH	1305-1309 MPH	1310-1314 MPH	1315-1319 MPH	1320-1324 MPH	1325-1329 MPH	1330-1334 MPH	1335-1339 MPH	1340-1344 MPH	1345-1349 MPH	1350-1354 MPH	1355-1359 MPH	1360-1364 MPH	1365-1369 MPH	1370-1374 MPH	1375-1379 MPH	1380-1384 MPH	1385-1389 MPH	1390-1394 MPH	1395-1399 MPH	1400-1404 MPH	1405-1409 MPH	1410-1414 MPH	1415-1419 MPH	1420-1424 MPH	1425-1429 MPH	1430-1434 MPH	1435-1439 MPH	1440-1444 MPH	1445-1449 MPH	1450-1454 MPH	1455-1459 MPH	1460-1464 MPH	1465-1469 MPH	1470-1474 MPH	1475-1479 MPH	1480-1484 MPH	1485-1489 MPH	1490-1494 MPH	1495-1499 MPH	1500-1504 MPH	1505-1509 MPH	1510-1514 MPH	1515-1519 MPH	1520-1524 MPH	1525-1529 MPH	1530-1534 MPH	1535-1539 MPH	1540-1544 MPH	1545-1549 MPH	1550-1554 MPH	1555-1559 MPH	1560-1564 MPH	1565-1569 MPH	1570-1574 MPH	1575-1579 MPH	1580-1584 MPH	1585-1589 MPH	1590-1594 MPH	1595-1599 MPH	1600-1604 MPH	1605-1609 MPH	1610-1614 MPH	1615-1619 MPH	1620-1624 MPH	1625-1629 MPH	1630-1634 MPH	1635-1639 MPH	1640-1644 MPH	1645-1649 MPH	1650-1654 MPH	1655-1659 MPH	1660-1664 MPH	1665-1669 MPH	1670-1674 MPH	1675-1679 MPH	1680-1684 MPH	1685-1689 MPH	1690-1694 MPH	1695-1699 MPH	1700-1704 MPH	1705-1709 MPH	1710-1714 MPH	1715-1719 MPH	1720-1724 MPH	1725-1729 MPH	1730-1734 MPH	1735-1739 MPH	1740-1744 MPH	1745-1749 MPH	1750-1754 MPH	1755-1759 MPH	1760-1764 MPH	1765-1769 MPH	1770-1774 MPH	1775-1779 MPH	1780-1784 MPH	1785-1789 MPH	1790-1794 MPH	1795-1799 MPH	1800-1804 MPH	1805-1809 MPH	1810-1814 MPH	1815-1819 MPH	1820-1824 MPH	1825-1829 MPH	1830-1834 MPH	1835-1839 MPH	1840-1844 MPH	1845-1849 MPH	1850-1854 MPH	1855-1859 MPH	1860-1864 MPH	1865-1869 MPH	1870-1874 MPH	1875-1879 MPH	1880-1884 MPH	1885-1889 MPH	1890-1894 MPH	1895-1899 MPH	1900-1904 MPH	1905-1909 MPH	1910-1914 MPH	1915-1919 MPH	1920-1924 MPH	1925-1929 MPH	1930-1934 MPH	1935-1939 MPH	1940-1944 MPH	1945-1949 MPH	1950-1954 MPH	1955-1959 MPH	1960-1964 MPH	1965-1969 MPH	1970-1974 MPH	1975-1979 MPH	1980-1984 MPH	1985-1989 MPH	1990-1994 MPH	1995-1999 MPH	2000-2004 MPH	2005-2009 MPH	2010-2014 MPH	2015-2019 MPH	2020-2024 MPH	2025-2029 MPH	2030-2034 MPH	2035-2039 MPH	2040-2044 MPH	2045-2049 MPH	2050-2054 MPH	2055-2059 MPH	2060-2064 MPH	2065-2069 MPH	2070-2074 MPH	2075-2079 MPH	2080-2084 MPH	2085-2089 MPH	2090-2094 MPH	2095-2099 MPH	2100-2104 MPH	2105-2109 MPH	2110-2114 MPH	2115-2119 MPH	2120-2124 MPH	2125-2129 MPH	2130-2134 MPH	2135-2139 MPH	2140-2144 MPH	2145-2149 MPH	2150-2154 MPH	2155-2159 MPH	2160-2164 MPH	2165-2169 MPH	2170-2174 MPH	2175-2179 MPH	2180-2184 MPH	2185-2189 MPH	2190-2194 MPH	2195-2199 MPH	2200-2204 MPH	2205-2209 MPH	2210-2214 MPH	2215-2219 MPH	2220-2224 MPH	2225-2229 MPH	2230-2234 MPH	2235-2239 MPH	2240-2244 MPH	2245-2249 MPH	2250-2254 MPH	2255-2259 MPH	2260-2264 MPH	2265-2269 MPH	2270-2274 MPH	2275-2279 MPH	2280-2284 MPH	2285-2289 MPH	2290-2294 MPH	2295-2299 MPH	2300-2304 MPH	2305-2309 MPH	2310-2314 MPH	2315-2319 MPH	2320-2324 MPH	2325-2329 MPH	2330-2334 MPH	2335-2339 MPH	2340-2344 MPH	2345-2349 MPH	2350-2354 MPH	2355-2359 MPH	2360-2364 MPH	2365-2369 MPH	2370-2374 MPH	2375-2379 MPH	2380-2384 MPH	2385-2389 MPH	2390-2394 MPH	2395-2399 MPH	2400-2404 MPH	2405-2409 MPH	2410-2414 MPH	2415-2419 MPH	2420-2424 MPH	2425-2429 MPH	2430-2434 MPH	2435-2439 MPH	2440-2444 MPH	2445-2449 MPH	2450-2454 MPH	2455-2459 MPH	2460-2464 MPH	2465-2469 MPH	2470-2474 MPH	2475-2479 MPH	2480-2484 MPH	2485-2489 MPH	2490-2494 MPH	2495-2499 MPH	2500-2504 MPH	2505-2509 MPH	2510-2514 MPH	2515-2519 MPH	2520-2524 MPH	2525-2529 MPH	2530-2534 MPH	2535-2539 MPH	2540-2544 MPH	2545-2549 MPH	2550-2554 MPH	2555-2559 MPH	2560-2564 MPH	2565-2569 MPH	2570-2574 MPH	2575-2579 MPH	2580-2584 MPH	2585-2589 MPH	2590-2594 MPH	2595-2599 MPH	2600-2604 MPH	2605-2609 MPH	2610-2614 MPH	2615-2619 MPH	2620-2624 MPH	2625-2629 MPH	2630-2634 MPH	2635-2639 MPH	2640-2644 MPH	2645-2649 MPH	2650-2654 MPH	2655-2659 MPH	2660-2664 MPH	2665-2669 MPH	2670-2674 MPH	2675-2679 MPH	2680-2684 MPH	2685-2689 MPH	2690-2694 MPH	2695-2699 MPH	2700-2704 MPH	2705-2709 MPH	2710-2714 MPH	2715-2719 MPH	2720-2724 MPH	2725-2729 MPH	2730-2734 MPH	2735-2739 MPH	2740-2744 MPH	2745-2749 MPH	2750-2754 MPH	2755-2759 MPH	2760-2764 MPH	2765-2769 MPH	2770-2774 MPH	2775-2779 MPH	2780-2784 MPH	2785-2789 MPH	2790-2794 MPH	2795-2799 MPH	2800-2804 MPH	2805-2809 MPH	2810-2814 MPH	2815-2819 MPH	2820-2824 MPH	2825-2829 MPH	2830-2834 MPH	2835-2839 MPH	2840-2844 MPH	2845-2849 MPH	2850-2854 MPH	2855-2859 MPH	2860-2864 MPH	2865-2869 MPH	2870-2874 MPH	2875-2879 MPH	2880-2884 MPH	2885-2889 MPH	2890-2894 MPH	2895-2899 MPH	2900-2904 MPH	2905-2909 MPH	2910-2914 MPH	2915-2919 MPH	2920-2924 MPH	2925-2929 MPH	2930-2934 MPH	2935-2939 MPH	2940-2944 MPH	2945-2949 MPH	2950-2954 MPH	2955-2959 MPH	2960-2964 MPH	2965-2969 MPH	2970-2974 MPH	2975-2979 MPH	2980-2984 MPH	2985-2989 MPH	2990-2994 MPH	2995-2999 MPH	3000-3004 MPH	3005-3009 MPH	3010-3014 MPH	3015-3019 MPH	3020-3024 MPH	3025-3029 MPH	3030-3034 MPH	3035-3039 MPH	3040-3044 MPH	3045-3049 MPH	3050-3054 MPH	3055-3059 MPH	3060-3064 MPH	3065-3069 MPH	3070-3074 MPH	3075-3079 MPH	3080-3084 MPH	3085-3089 MPH	3090-3094 MPH	3095-3099 MPH	3100-3104 MPH	3105-3109 MPH	3110-3114 MPH	3115-3119 MPH	3120-3124 MPH	3125-3129 MPH	3130-3134 MPH	3135-3139 MPH	3140-3144 MPH	3145-3149 MPH	3150-3154 MPH	3155-3159 MPH	3160-3164 MPH	3165-3169 MPH	3170-3174 MPH	3175-3179 MPH	3180-3184 MPH	3185-3189 MPH	3190-3194 MPH	3195-3199 MPH	3200-3204 MPH	3205-3209 MPH	3210-3214 MPH	3215-3219 MPH	3220-3224 MPH	3225-3229 MPH	3230-3234 MPH	3235-3239 MPH	3240-3244 MPH	3245-3249 MPH	3250-3254 MPH	3255-3259 MPH	3260-3264 MPH	3265-3269 MPH	3270-3274 MPH	3275-3279 MPH	3280-3284 MPH	3285-3289 MPH	3290-3294 MPH	3295-3299 MPH	3300-3304 MPH	3305-3309 MPH	3310-3314 MPH	3315-3319 MPH	3320-3324 MPH	3325-3329 MPH	3330-3334 MPH	3335-3339 MPH	3340-3344 MPH	3345-3349 MPH	3350-3354 MPH	3355-3359 MPH	3360-3364 MPH	3365-3369 MPH	3370-3374 MPH	3375-3379 MPH	3380-3384 MPH	3385-3389 MPH	3390-3394 MPH	3395-3399 MPH	3400-3404 MPH	3405-3409 MPH	3410-3414 MPH	3415-3419 MPH	3420-3424 MPH	3425-3429 MPH	3430-3434 MPH	3435-3439 MPH	3440-3444 MPH	3445-3449 MPH	3450-3454 MPH	3455-3459 MPH	3460-3464 MPH	3465-3469 MPH	3470-3474 MPH	3475-3479 MPH	3480-3484 MPH	3485-3489 MPH	3490-3494 MPH	3495-3499 MPH	3500-3504 MPH	3505-3509 MPH	3510-3514 MPH	3515-3519 MPH	3520-3524 MPH	3525-3529 MPH

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS WITH
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	NOON	
TRACE	11	12	12	13	12	14	11	12	11	10	9	8	7	7	6	6	7	7	7	8	7	7	10	30	
0.01 IN	3	4	3	4	4	3	3	2	3	4	2	1	1	1	3	2	2	1	2	3	2	3	3	3	6
0.02 TO 0.09 IN	3	4	6	6	5	4	5	4	4	3	2	2	2	2	2	3	3	4	4	4	4	4	4	4	14
0.10 TO 0.19 IN	1	1	1	1	1	1	1	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	10
0.20 TO 0.29 IN	+	+	+	+	+		+	+	+	+	+	+	1	+	+	+	+	+	+	+	+	+	+	+	6
0.30 TO 0.39 IN					+						+						+								4
0.40 TO 0.49 IN																									1
0.50 TO 0.59 IN																									1
0.60 IN AND OVER																									+
TOTAL	18	21	23	24	22	22	20	20	19	17	14	13	11	11	12	12	12	13	13	14	15	15	14	17	70

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT
	0	100-200	200-400	400-600	600-800	800-1000	1000-1500	1500-2000	2000-2500	OVER 2500	
0 TO 1/8	+	+	+	+	+					+	1
1/8 TO 1/4	+	+	+	+	+	+				+	+
1/4 TO 1/2	+	+	+	+	+	+	+			+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+		+	4
3/4 TO 1	+	+	+	+	+	+	+	+	+	+	13
1 TO 1 1/2											
1 1/2 TO 2											
2 TO 3											
3 TO 4											
4 TO 5											
5 TO 6											
6 TO 7											
7 TO 8											
8 TO 9											
9 TO 10											
10 TO 11											
11 TO 12											
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18 TO 19											
19 TO 20											
20 TO 21											
21 TO 22											
22 TO 23											
23 TO 24											
24 TO 25											
25 TO 26											
26 TO 27											
27 TO 28											
28 TO 29											
29 TO 30											
30 OR MORE											
TOTAL	+	1	1	1	6	15	7	5	2	62	100

ITY OCCURRENCES:

J.M.		25 MPH AND OVER								TOTAL C.S.
25	30	35	40	45	50	55	60	65	70	
+										29
2	+									126
5	2	1								1016
10	5	4								1956
11	13	12								12244
2	2	3								11736
+	+	1								843
+										328
										59
										4
31	23	20								28767

ar total divided by 10).
ake their sums exactly
ess than 0.5.

COUNTS:

OF THE DAY										NO OF DAYS WITH
H HOUR ENDING AT										
5	6	7	8	9	10	11	12	13	14	
7	7	7	7	8	7	7	10	30		30
2	1	2	3	2	3	3	3	6		6
3	4	4	4	4	3	4	4	14		14
+	1	1	+	1	1	1	1	10		10
+	+	+	+					6		6
								1		1
								+		+
12	13	13	14	15	15	14	17	70		

F

OVER	FOR
+	1
+	+
+	1
+	1
+	4
+	7
1	39
+	62
+	9
+	12
+	6
2	62
	100

B PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED IN MILES PER HOUR																TOTAL	PERCENT
	0-3	4-7	8-12	13-17	18-24	25-31	32-39	40-47	48-54	55-61	62-69	70-77	78-84	85-91	92-99	100-107		
N	3	3	1	+													7	4
NNE	3	3	+	+													7	4
NNE	4	4	+	+	+												8	4
ENE	2	2	+	+	+												4	4
E	2	1	+	+	+												3	4
ESE	1	1	+	+	+												2	4
SE	1	1	+	+	+												2	5
SSE	+	1	1	+	+	+	+										2	7
S	1	2	2	1	+	+	+										5	7
SSW	1	3	3	1	+	+	+										8	8
SW	1	3	3	1	+	+	+										8	7
WSW	1	3	3	1	+	+	+										8	8
W	1	3	3	1	+	+	+										8	7
WNW	1	3	5	1	+	+	+										10	8
NW	1	3	4	1	+	+	+										8	7
NNW	1	3	2	+	+	+	+										7	6
CALM	6																6	6
TOTAL	28	38	28	6	+	+	+										100	6

E PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOURS OF DAY	CLOUDS SCALE 0-10			WIND SPEED (IN P.M.)				RELATIVE HUMIDITY (%)							
	0-3	4-7	8-10	0-3	4-7	12-24	25-31	0-29	30-49	50-69	70-79	80-89	90-99	100	
00	40	6	52	48	50	2		1	4	11	23	47	14		
01	38	7	55	49	49	2		1	5	12	21	45	17		
02	36	7	57	49	49	2		1	5	11	20	44	19		
03	36	6	58	49	49	2	+	1	5	12	19	43	20		
04	35	6	59	49	49	2		1	5	11	20	42	21		
05	35	6	59	49	49	2	+	1	5	12	20	41	20		
06	33	8	59	48	50	2	+	2	6	13	24	39	17		
07	32	10	56	45	53	2		2	7	20	30	31	10		
08	37	12	51	34	62	4	+	3	8	31	34	19	4		
09	46	12	42	19	76	5	+	5	10	44	29	10	2		
10	54	13	34	10	81	9	+	8	12	56	19	5	1		
11	58	13	28	3	83	14	+	9	13	62	13	3	+		
12	60	14	26	1	80	18	+	9	14	65	10	2	1		
13	62	14	24	1	77	22	+	9	14	67	8	1	1		
14	62	14	24	1	79	20	+	8	14	67	8	2	1		
15	61	14	24	1	83	16	+	7	13	67	11	2	1		
16	61	13	25	2	88	10		5	11	61	18	4	1		
17	60	13	27	6	88	5	+	4	8	46	32	9	1		
18	58	14	28	16	81	3		3	6	25	45	19	2		
19	55	13	32	23	74	2	+	2	6	17	38	34	3		
20	52	12	36	30	68	2	+	1	5	15	33	41	5		
21	49	11	40	38	60	2	+	1	5	13	29	45	6		
22	46	10	44	42	57	2	+	1	4	13	24	47	9		
23	43	9	48	46	52	2	+	1	4	12	24	47	12		
AVG	48	11	41	28	66	6	+	4	8	32	23	26	8		

A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR SPEED (MPH)	0-4 MPH						5-14 MPH						15-24 MPH						25 MPH AND OVER						TOTAL COL
	0-4	5-14	15-24	25-34	35-44	45-54	55-64	65-74	75-84	85-94	95-104	105-114	115-124	125-134	135-144	145-154	155-164	165-174	175-184	185-194	195-204	205-214	215-224	225-234	235-244
109/109	+						+																		+
104/100							1																		+
99/ 95	1						2	+						1											+
94/ 90	2						3	2						+											7
89/ 85	4	2	+				10	9	2					1	1	+									28
84/ 80	9	4	3	+			26	21	45					1	3	5									117
79/ 75	11	7	17	2	+		40	40	206	12				3	4	37									380
74/ 70	15	13	44	36	25	1	42	54	393	143	25	1		4	8	66	11	+		1	+				881
69/ 65	14	27	68	132	223	22	47	75	390	315	220	19		9	13	61	17	2	1	1	1	+			1654
64/ 60	13	39	92	174	444	141	46	87	302	323	346	73		8	17	51	19	6	3	2	3	3	1	+	2193
59/ 55	11	39	90	156	371	201	33	81	177	208	294	143		9	17	28	13	10	14	2	4	4	1	1	12704
54/ 50	5	31	71	76	185	164	17	60	94	75	118	105		5	13	13	5	5	7	1	2	3	1	1	18054
49/ 45	3	13	44	39	73	59	9	28	50	30	40	28		1	5	3	1	2	2	+	1	+			428
44/ 40	1	6	13	15	18	11	1	7	12	10	9	4					+	+	1	+					107
39/ 35		1	2	2	1	1		2	1	1	+	+													10
34/ 30			+																						+
TOTAL	88	182	444	631	1340	601	277	466	1670	1144	1051	372	42	80	263	66	27	25	6	11	11	2	2	2	2767

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS OBSERVED
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11	END	
TOTAL	8	10	11	11	15	14	13	13	11	6	9	8	6	7	6	7	6	8	8	8	7	7	7	8	27
0.1 IN.	2	3	3	3	2	3	3	3	1	2	3	1	2	2	3	2	2	1	2	3	2	2	2	2	4
0.2 TO 0.4 IN.	4	4	3	4	4	4	4	3	3	3	2	3	4	3	3	3	3	3	4	3	4	5	5	4	10
0.5 TO 0.9 IN.	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	7	
1.0 TO 1.9 IN.	+	+	1	1	1	+	+	+	+	+	1	+	+	1	+	+	+	+	+	+	1	+	+	1	6
2.0 TO 2.9 IN.																									5
3.0 TO 3.9 IN.																									1
4.0 TO 4.9 IN.																									1
5.0 TO 5.9 IN.																									1
6.0 TO 6.9 IN.																									1
7.0 TO 7.9 IN.																									1
8.0 TO 8.9 IN.																									1
9.0 TO 9.9 IN.																									1
10.0 TO 10.9 IN.																									1
11.0 TO 11.9 IN.																									1
12.0 TO 12.9 IN.																									1
13.0 TO 13.9 IN.																									1
14.0 TO 14.9 IN.																									1
15.0 TO 15.9 IN.																									1
16.0 TO 16.9 IN.																									1
17.0 TO 17.9 IN.																									1
18.0 TO 18.9 IN.																									1
19.0 TO 19.9 IN.																									1
20.0 TO 20.9 IN.																									1
21.0 TO 21.9 IN.																									1
22.0 TO 22.9 IN.																									1
23.0 TO 23.9 IN.																									1
24.0 TO 24.9 IN.																									1
TOTAL	17	18	20	19	23	22	21	19	17	14	15	14	13	13	13	14	13	14	14	14	14	15	16	16	61

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOTAL
	0	100	200	300	400	500	600	700	800	900	
0 TO 1/8	1	+	+	+	+	+	+	+	+	+	1
3/16 TO 1/4	+	1	+	+	+	+	+	+	+	+	1
1/2 TO 3/4			1	+	+	+	+	+	+	+	2
1 TO 2 1/2				1	2	+	+	+	+	6	13
3 TO 4					1	4	1	+	+	17	26
7 TO 15					1	3	3	3	1	37	48
20 TO 30						+	+	+	+	5	6
35 (FM 40) TO 40							+	+	+	2	2
TOTAL	1	1	2	7	10	4	4	7	6	100	

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1 MPH			25 MPH AND OVER							TOTAL O/G
1-10	11-20	21-30	31-40	41-50	51-60	61-70	71-80	81-90		
									4	
									1	
									4	
									7	
									28	
1									117	
3									380	
7	11	+		1		+			881	
1	17	2			1	1			1654	
1	19	6	3	2	3	3	1	+	2193	
1	13	10	14	2	4	4	1	1	1704	
1	5	5	1	2	2	3	1	1	1054	
3	1	2	2	+		+			428	
6	+	1	+	1					107	
									10	
3	66	27	25	6	11	11	2	2	25767	

-year total divided by 10).
 > make their sums exactly
 < less than 0.5.

**B PERCENTAGE FREQUENCIES
OF WIND DIRECTION AND SPEED:**

HOURLY OBSERVATIONS OF WIND SPEED (44 HOURS FOR RECORD)														DATE
DIRECTION	WIND SPEED													TOTAL
	0-3	4-7	8-12	13-16	16-20	21-24	25-30	31-36	37-46	47-54	55-63	64-72	73-81	
N	1	1	+	+	+	+	+							2
NNE	+		1	+	+	+	+							2
NE	1	2	1	+	+	+	+							4
ENE	1	3	1	+	+	+	+							5
E	2	3	1	+	+	+	+							6
ESE	1	2	1	+	+	+	+							4
SE	1	2	1	+	+	+	+							4
SSE	1	1	+	+	+	+	+	+						2
S	1	1	+	+	+	+	+							2
SSW	1	1	+	+	+	+	+							2
SW	1	2	3	1	+	+	+							6
WSW	1	5	10	4	+	+	+							20
W	1	5	7	4	+	+	+	+						17
WNW	1	2	1	+	+	+	+							3
HW	1	1	+	+	+	+	+	+						2
RNW	+	1	+	+	+	+	+	+						2
CALM	13													13
TOTAL	29	33	27	11	1	+	+	+						100

MOUNTS:

UR OF THE DAY										No. of Start Time
P.M. HOUR ENDING AT										
4	5	6	7	8	9	10	11	12	13	
7	6	8	8	8	7	7	7	8	27	
2	2	1	2	3	2	2	2	4	10	
3	3	3	4	3	4	5	5	4	10	
1	1	1	1	+	1	1	1	1	7	
+	+	+		+		+	+	+	6	
									1	
									1	
									1	
14	13	14	14	14	14	15	16	16	61	

OF

2000 0300	0412 0700	104
	4	1
4	4	1
4	1	2
4	6	13
4	17	26
1	37	48
4	5	6
4	2	2
7	68	100

PERCENTAGE FREQUENCIES OF
SKY COVER, WIND, AND
RELATIVE HUMIDITY:

E

HOURS OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M P H)					RELATIVE HUMIDITY (%)					
	0-3	4-7	8-10	0-3	4-12	13-24	25-34 OVER	0-29	30-49	50-69	70-79	80-89	90-100	
00	51	9	41	43	54	3	+	2	6	9	18	47	18	
01	49	7	44	46	51	3	+	2	6	8	16	47	21	
02	47	8	45	47	51	3	+	2	6	8	14	45	24	
03	45	8	48	46	51	3	+	2	6	8	14	43	26	
04	43	8	50	48	50	2	+	2	7	9	14	43	26	
05	40	8	52	48	50	2	+	2	7	9	15	42	25	
06	37	8	54	46	51	2	+	2	7	10	17	41	23	
07	35	9	56	43	54	3	+	3	8	15	26	33	16	
08	34	11	51	36	61	3	+	5	10	25	30	21	8	
09	44	12	44	27	69	4	+	6	12	40	25	11	4	
10	50	12	38	16	77	6	+	11	12	50	17	7	2	
11	55	12	33	10	76	13	+	13	13	56	13	4	2	
12	50	13	24	5	70	24	1	12	15	50	11	3	1	
13	61	12	27	3	61	36	1	10	14	61	11	3	1	
14	61	12	27	1	57	41	1	8	13	61	13	3	1	
15	61	13	26	1	57	41	1	7	12	58	17	5	2	
16	59	12	29	2	60	36	1	5	10	50	25	8	2	
17	57	13	30	5	69	26	+	3	7	35	35	17	3	
18	55	12	33	11	74	15	+	2	5	22	36	29	5	
19	56	11	33	16	75	0	+	3	5	17	31	37	8	
20	57	9	34	25	69	6	+	2	5	14	28	40	11	
21	56	9	35	32	63	5	+	2	6	12	25	42	13	
22	55	7	37	36	60	3	+	2	6	10	24	44	14	
23	52	9	39	40	57	3	+	2	6	9	21	46	15	
AVG	51	10	39	26	61	12	+	5	8	27	21	20	11	

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Int. Airport

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR	0-4 M.P.H.						5-14 M.P.H.					15-24 M.P.H.					25 M.P.H. AND OVER					TOTAL OBS				
	SE	NE	E	S	SW	NW	SE	NE	E	S	SW	NW	SE	NE	E	S	SW	NW	SE	NE	E		S	SW	NW	
4/100							+	+																		1
9/ 95	1						2	1																		6
4/ 90	1	1					10	8																		23
9/ 85	1	3					11	30																		54
4/ 80	2	9					14	69	14																	126
9/ 75	2	12	10				10	100	58																	211
4/ 70	1	19	45				6	98	164																	373
9/ 65	1	22	88	32	11		6	75	242	57	13															501
4/ 60	2	15	103	113	99	30	4	46	234	171	105	31														1001
9/ 55	1	13	81	139	191	113	3	34	173	174	204	85	2	13	35	17	26	11								11316
4/ 50	+	6	54	90	170	164	2	29	127	143	185	120	2	14	38	33	49	27								1274
9/ 45	+	6	46	65	135	167	3	18	93	140	216	139	3	19	49	50	78	30								1271
4/ 40	+	3	24	57	147	210	1	9	56	102	224	171	3	13	40	39	87	41								21238
9/ 35		2	10	23	87	205		3	22	42	112	138	+	6	33	22	35	28								1772
4/ 30			4	10	32	117	+	1	10	13	39	62	1	4	17	8	13	10								343
9/ 25		1	2	6	12	30	+	3	10	7	11	10	+	5	8	5	8	2								123
4/ 20		1	3	1	3	1		2	6	2	1	+		6	11	2	3									40
9/ 15			1	1	+	+		+	4	1	+	+		1	2											10
4/ 10			1	+	+	+		+	3	+	+	+		+												4
9/ 05			+						1	+	+	+														1
TOTAL	12	116	449	538	888	1036	73	526	1216	862	1108	758	33	138	286	185	307	150	1	5	15	11	23	68767		

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																							NO OF DAYS WITH	
	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	NOON	1	2	3	4	5	6	7	8	9	10	11		NOON
TRACE	38	36	36	38	45	46	47	49	43	42	46	47	45	48	47	43	42	39	40	36	34	32	38	36	45
01 IN	14	15	16	16	14	14	15	17	16	16	14	13	17	15	17	17	16	15	14	16	16	18	15	15	15
02 TO 09 IN	21	25	25	26	23	24	23	22	24	22	19	22	25	25	25	26	24	24	23	24	23	25	20	19	48
10 TO 24 IN	3	3	4	3	3	3	4	3	4	3	4	3	2	4	4	4	4	3	4	3	2	2	3	4	1
25 TO 49 IN	+	+	+	+				+	+	+		+	+	1	+	+	+	1		+	+				32
50 TO 99 IN																									17
100 TO 199 IN																									5
200 IN AND OVER																									+
TOTAL	76	78	81	84	84	87	89	91	87	83	83	85	89	92	93	89	85	82	81	78	76	77	75	73	201

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100-200	300-400	500-600	1000-1100	2000-2100	3000-4000	5000-7000	OVER	TOT
0 TO 1/8	1	+	+	+	+	+	+	+	+	1
3/16 TO 1/8	+	+	+	+	+	+	+	+	+	1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	1
1 TO 2 1/2		+	+	1	+	+	+	+	+	3
3 TO 6		+	+	1	2	1	2	1	4	11
7 TO 15	+	+	+	1	4	4	12	10	27	58
20 TO 30				+	+	1	4	4	8	16
35 OR MORE				+	+	+	+	1	7	9
TOTAL	1	1	1	2	7	7	18	16	48	100

ES:

4 AND OVER				TOTAL OBS
1	2	3	4	
1				1
6				6
23				23
54				54
126				126
211				211
373				373
581				581
1001				1001
11316				11316
21274				21274
21271				21271
21238				21238
772				772
343				343
123				123
40				40
10				10
4				4
1				1
5	11	23		65767

y 10).
ctly

NO OF DAYS WITH		
1	2	3
18	36	45
15	15	15
10	19	48
2	3	41
		32
		17
		5
		+
15	73201	

B PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED (IN MILES PER HOUR)																TOTAL	AV SPEED
	0	3	4	7	8	12	13	16	19	24	25	31	32	36	39	46		
	OVER																	
N	1																3	5.1
NNE	+	+															1	4.0
NE	1																1	4.1
ENE	+	+															1	7.4
E	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	4	10.1
ESE	1	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	13	10.8
SE	1	2	2	1	1	1	1	1	1	1	1	1	1	1	1	1	6	7.9
SSE	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	4	8.0
S	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	7	11.3
SSW	+	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	7	13.0
SW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	4	8.3
WSW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	7.4
W	1	2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	4	5.8
WNW	2	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	11	7.6
NW	3	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	14	7.3
NNW	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	6	7.3
CALM	11																11	
TOTAL	28	27	25	16	4	1	1	1	1	1	1	1	1	1	1	1	100	7.7

E PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M. P. H.)				RELATIVE HUMIDITY (%)							
	0-3	4-7	8-10	0-3	4-12	13-24	25-30	0-29	30-49	50-69	70-79	80-89	90-100		
	OVER			OVER											
00	37	9	54	36	50	13	1	+	1	12	22	36	29		
01	35	9	56	39	47	13	1	+	1	9	19	39	32		
02	33	9	59	41	45	13	+	+	1	7	17	39	36		
03	30	8	61	42	45	13	+	+	1	6	15	40	39		
04	27	9	64	44	42	13	1	+	1	5	13	36	43		
05	23	9	68	43	43	13	1	+	1	4	12	39	44		
06	20	9	72	42	44	14	1	+	1	5	14	39	42		
07	17	9	74	38	47	14	1	+	1	7	20	37	35		
08	17	9	75	32	51	16	1	+	1	14	26	31	27		
09	18	10	72	27	54	17	1	+	2	27	25	25	20		
10	20	10	70	23	56	20	1	1	5	37	22	22	14		
11	23	10	67	20	57	22	1	2	10	41	19	18	10		
12	25	10	65	16	58	24	1	2	17	41	16	16	8		
13	25	12	63	14	60	25	1	3	23	38	14	14	8		
14	26	12	62	13	60	26	1	4	27	36	13	13	8		
15	27	11	62	14	56	29	1	5	28	33	13	13	8		
16	27	11	62	15	55	29	1	5	28	32	13	14	9		
17	28	12	60	16	55	28	1	3	23	33	13	17	11		
18	30	12	58	18	54	27	1	2	18	33	15	18	13		
19	31	12	56	21	56	22	1	1	11	34	17	20	17		
20	34	11	55	23	58	19	1	1	6	31	21	23	19		
21	35	12	53	25	57	17	+	+	4	25	25	25	21		
22	36	10	53	20	55	16	1	+	3	20	26	28	23		
23	36	10	53	33	52	15	1	+	2	15	25	33	25		
AVG	20	10	62	28	52	19	1	1	9	23	18	27	22		

PORTLAND, OREG
Int. Airport

A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR. SPEED (KTS)	0-4 M.P.H.						5-14 M.P.H.						15-24 M.P.H.						25 M.P.H. AND OVER						TOTAL OBS.
	0-4	5-14	15-24	25-34	35-44	45-54	5-14	15-24	25-34	35-44	45-54	55-64	15-24	25-34	35-44	45-54	55-64	65-74	25-34	35-44	45-54	55-64	65-74	75-84	
99/ 95							1						1												2
94/ 90							2						2												6
89/ 85							12						3												24
84/ 80	1	2					34	2					14	1											62
79/ 75		9	2				66	15					23	4											123
74/ 70	1	9	12				85	86	1				34	23											258
69/ 65	1	7	28				73	199	26				29	57											448
64/ 60		3	42	31	23		43	236	124	67	19		22	72	32	13									750
59/ 55		5	31	36	61	66	33	173	169	222	201		20	73	54	57	47								1272
54/ 50		5	26	28	51	117	34	127	136	245	327		18	65	64	89	54								1462
49/ 45		3	27	29	60	107	19	104	131	237	292		14	68	74	117	99								1445
44/ 40		1	17	28	64	132	1	15	74	107	224	335	1	11	38	62	145	97							1408
39/ 35			8	15	40	123	1	11	40	61	142	256		8	17	16	63	85							914
34/ 30			4	9	16	92	1	11	21	21	49	135		5	12	8	12	27							427
29/ 25			2	3	6	16		6	14	7	10	17		4	6	4	4	5							104
24/ 20				1	1	2		3	7	4	4	2		2	5	2	2	1							39
19/ 15			1					2	6	3	1			1	2										20
14/ 10									1	1	1														3
TOTAL	4	43	100	188	324	666	37	449	1098	792	1205	1583	25	207	442	325	505	450	1	8	38	42	61	57	6767

In Table A, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

DATA NOT AVAILABLE

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)										TOT.
	0	100-200	200-400	400-700	700-1000	1000-2000	2000-4000	4000-6000	OVER 6000		
0 TO 1/8	1	1	+	+	+	+	+	+	+		2
3/8 TO 1/2	+	+	+	+	+	+	+	+	+		1
1/2 TO 3/4	+	+	+	+	+	+	+	+	+		1
1 TO 1 1/2	+	+	1	1	1	+	+	+	1		4
3 TO 6		+	+	1	2	1	1	1	3		9
7 TO 15			+	2	7	6	9	8	26		58
20 TO 30				+	1	1	2	3	10		17
35 OR MORE				+	+	+	+	1	6		8
TOTAL	1	2	2	4	10	9	13	13	47		100

SEATTLE, WASHINGTON
Seattle-Tacoma Airp

UMIDITY OCCURRENCES:

15-24 M.P.H.				25 M.P.H. AND OVER					TOTAL OBS.
2-4%	5-7%	8-9%	10-14%	15-24%	25-34%	35-44%	45-54%	55-64%	
									2
									6
									24
									62
1				+	+				123
4									258
25	+			+	1	+			448
57	7	1		+	1	2	+	+	750
72	32	15	6	+	4	2	1	+	1272
73	54	57	47		1	6	5	5	1462
65	64	89	64		2	9	8	12	1445
68	74	117	99		1	11	13	25	1408
58	62	145	97	+	3	12	27	13	914
17	18	63	85	+	+	2	10	12	427
12	8	12	27		1	1	1	2	104
6	4	4	5		+	1	+	+	39
5	2	2	1		1	1	+	+	20
2	1				1	+			3
4									
442	325	505	450	1	8	38	42	81	578767

(10-year total divided by 10).
 id to make their sums exactly
) but less than 0.5.

I AMOUNTS:

ES OF

25-34%	35-44%	OVER 44%	TOT.
+	+	+	2
+	+	+	1
+	+	+	1
+	+	1	4
1	1	3	9
9	8	26	58
2	3	10	17
4	1	6	8
13	13	47	100

SEATTLE, WASHINGTON
 Seattle-Tacoma Airport

B-16

B PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

DIRECTION	HOURLY OBSERVATIONS OF WIND SPEED IN MILES PER HOUR									
	0 - 3	4 - 7	8 - 12	13 - 18	19 - 24	25 - 31	32 - 38	39 - 46	47 OVER	
N	+	1	3	3	+	+	+			
NNE	+	1	3	3	+	+	+			
NE	+	1	3	2	+	+				
ENE	+	1	1	+	+	+				
E	+	1	1	1	+	+				
ESE	+	1	2	1	+	+	+			
SE	+	2	3	1	+	+				
SSE	+	1	2	1	+	+				
S	+	2	4	3	1	+	+	+		
SSW	+	1	3	4	2	1	+	+		
SW	+	1	4	5	2	1	+	+		
WSW	+	1	2	1	+	+	+	+	+	
W	+	1	1	1	+	+	+			
WNW	+	1	1	+	+	+				
NW	+	1	1	+	+	+	+	+		
NNW	+	+	1	1	+	+	+			
CALM	10									
TOTAL	13	16	35	26	8	2	+	+	+	

E PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

HOUR OF DAY	CLOUDS SCALE 0-10			WIND SPEED (M. P. H.)				RELATIVE HUMIDITY				
	0-3	4-7	8-10	0-3	4-12	13-24	25- OVER	0-29	30-49	50-69	70-79	80-89
00	33	10	57	14	53	31	2	+	2	9	16	33
01	32	9	59	16	54	29	2	+	2	7	13	33
02	29	9	61	17	55	27	2	+	1	6	11	31
03	27	10	63	17	55	26	2	+	1	5	10	30
04	24	10	66	19	55	24	2	+	1	4	9	28
05	20	10	70	20	54	24	2	+	1	3	8	28
06	18	11	71	19	55	25	1	+	1	4	10	30
07	16	10	74	18	55	26	2	+	1	7	14	33
08	16	9	74	17	53	28	2	+	2	12	20	36
09	17	10	73	15	52	30	3	+	3	20	22	26
10	19	11	70	13	50	33	3	+	5	29	22	22
11	20	13	67	11	48	37	4	1	9	36	20	18
12	21	15	64	10	48	38	4	1	13	40	17	14
13	22	14	64	9	46	41	4	2	15	39	15	11
14	23	14	63	8	45	42	4	2	23	37	13	10
15	24	14	62	9	46	42	3	3	24	34	13	10
16	25	13	62	10	46	41	3	3	23	32	14	10
17	26	14	60	11	47	40	2	2	20	30	14	10
18	27	14	60	11	49	37	3	1	17	29	15	11
19	28	14	58	12	50	36	2	1	11	29	16	12
20	31	14	56	13	49	36	2	+	6	25	19	20
21	32	13	55	12	51	36	2	+	4	21	20	20
22	33	11	55	12	50	36	2	+	3	16	20	30
23	33	11	56	12	52	33	2	+	3	12	19	30
AVG	25	12	63	13	51	33	3	1	8	20	15	20

TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

WIND DIR. ALAND TEMP (°F)	0-4 M.P.H.					5-14 M.P.H.					15-24 M.P.H.					25 M.P.H. AND OVER					TOTAL OBS.			
	UNDER 20	20-49	50-69	70-79	80-89	UNDER 20	20-49	50-69	70-79	80-89	90-100%	UNDER 20	20-49	50-69	70-79	80-89	90-100%	UNDER 20	20-49	50-69		70-79	80-89	90-100%
77/105						+																		+
77/100						1																		2
77/95	+					3	12		1			2	4							+				21
77/90						2	40	12				1	16											79
77/85	+	4				5	69	63	2			4	24	16										200
77/80	1	14	22	7	1	7	96	129	33	5	+	7	30	21	7	+		1	1	+	+			383
77/75	1	13	30	27	23	12	9	106	147	79	58	23	8	35	24	8	6	4	1	1	1	+	+	615
77/70	1	12	34	31	51	53	12	86	169	88	103	65	9	26	26	10	9	8	1	1	1	+	1	819
77/65	1	9	36	36	51	44	12	78	152	92	109	83	9	34	32	10	11	12	1	2	1	+	1	814
77/60	1	11	30	35	45	44	12	80	133	79	87	82	9	36	32	8	12	14	1	2	1	1	+	755
77/55	1	10	29	28	37	34	10	83	124	67	66	80	8	33	37	11	12	19	1	3	1	1	1	697
77/50	1	9	31	24	37	30	6	81	136	61	73	83	3	36	32	12	13	19	+	3	1	+	1	692
77/45	1	9	33	28	30	29	5	70	133	69	68	72	3	47	47	12	13	21	1	3	4	1	1	701
77/40	+	9	35	28	30	32	2	81	171	77	57	74	2	52	65	19	18	21	1	5	3	+	1	784
77/35	+	8	42	33	31	25	1	62	209	82	70	82	2	49	69	17	16	35	+	6	4	1	1	846
77/30	+	7	38	22	19	19	1	57	172	52	41	45	1	52	60	10	9	22	+	5	3	+	+	637
77/25		2	17	11	8	5	1	38	113	31	16	12	2	36	51	6	2	4	+	3	3	+	+	360
77/20	+	3	11	5	2	+	1	27	70	12	6	1	1	21	29	3	4	3	+	2	1	+	+	202
77/15		2	8	3	1	1		12	32	6	2	+	+	15	19	2	3	+		3	1	+	+	109
77/10		1	4	+	+	+		4	11	1	1	+		4	9	+	1	+		+	+	+	+	38
77/05			+					1	5	1				2	2		+							11
77/00									1	+				+										2
TAL	8	131	406	320	366	327	88	1082	1984	832	763	723	69	552	575	132	129	181	7	39	27	6	8153767	

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

INTENSITIES	FREQUENCY OF OCCURRENCE FOR EACH HOUR OF THE DAY																								NO OF DAYS WITH
	AM HOUR ENDING AT												PM HOUR ENDING AT												
	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11		
TRACE	28	27	28	26	31	26	29	32	33	29	30	30	29	32	30	28	27	26	27	28	27	27	29	29	60
01 IN	7	8	11	9	6	7	9	8	8	8	7	8	6	6	6	8	7	7	9	6	8	9	8	8	12
02 TO 09 IN	17	16	17	16	15	15	14	15	14	14	14	13	14	14	15	14	14	14	15	15	15	15	16	15	33
10 TO 24 IN	4	5	5	5	5	5	5	4	4	5	4	4	5	3	2	4	4	3	3	5	3	4	5	5	27
25 TO 49 IN	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	21
50 TO 99 IN	+	+	+	+	1	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	20
100 TO 199 IN																									9
200 IN AND OVER																									1
TOTAL	57	56	58	57	58	56	58	60	60	58	56	56	55	57	57	55	52	51	55	55	55	57	59	59	182

D PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

VISIBILITY (MILES)	CEILING (FEET)									
	0	100- 200	200- 400	400- 600	600- 800	800- 1000	1000- 1200	1200- 1400	OVER 1400	TOT
0 TO 1/8	+	+	+	+			+		+	+
3/16 TO 1/4	+	+	+	+	+		+	+	+	+
1/2 TO 3/4	+	+	+	+	+	+	+	+	+	2
1 TO 2 1/2			+	1	3	1	+	+	1	3
3 TO 6			+	+	2	3	1	2	2	23
7 TO 15	+			+	+	2	2	6	7	66
20 TO 30										
35 OR MORE										
TOTAL	+	1	1	6	6	4	8	10	65	100

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PERCENTAGE FREQUENCIES OF
SKY COVER, WIND, AND
RELATIVE HUMIDITY:

NEWARK, N
Newark Ai

Mobile, Alabama

STATION NO.		OCCURRENCES OF PRECIPITATION AMOUNTS:																								NO. YEARS	
01-5478 ANN		FREQUENCY OF OCCURRENCES FOR EACH HOUR OF THE DAY																								5	
INTENSITIES		A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												DAYS WITH	
		1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12		
.01 IN.		3	5	4	4	4	2	2	2	4	4	5	3	3	4	6	5	6	5	5	5	5	4	4	4	6	
.02 TO .09 IN.		8	6	7	7	8	7	7	7	8	9	8	8	10	14	13	13	11	11	13	10	9	7	8	7	34	
.10 TO .24 IN.		3	4	2	3	2	3	4	4	4	7	3	4	4	3	4	6	4	4	5	4	3	3	2	3	22	
.25 TO .49 IN.		1	1	1	1	1	1	1	2	2	*	1	2	3	3	4	2	2	3	2	2	1	1	1	1	18	
.50 TO .99 IN.		1	*	*	*	1	1	1	*	*	*	1	1	2	2	2	1	2	1	2	1	1	*	1	*	20	
1.00 TO 1.99 IN.		*	*	*	*	*	*	*	*	*	*	*	*	*	1	*	*	1	*	1	*	*	*	*	*	15	
2.00 IN. AND OVER		*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	3	
TOTAL		17	16	15	15	16	14	16	16	18	20	18	19	23	29	29	27	26	24	26	21	20	15	16	15	121	

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Seattle, Washington

STATION NO.

OCCURRENCES OF PRECIPITATION AMOUNTS:

NO. YEARS

45-7433 ANN

FREQUENCY OF OCCURRENCES FOR EACH HOUR OF THE DAY

5

INTENSITIES

	A.M. HOUR ENDING AT												P.M. HOUR ENDING AT												DAYS WITH	
	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12		
.01 IN.	19	25	28	31	20	15	11	9	7	10	9	9	14	14	18	15	21	23	24	15	12	14	13	19	10	
.01 TO .04 IN.	19	21	27	28	27	21	21	27	25	17	19	22	20	21	20	24	24	26	23	22	20	18	20	35	35	
.10 TO .24 IN.	2	3	2	2	3	4	4	4	2	3	2	3	3	3	3	2	3	3	4	3	2	4	3	5	43	
.25 TO .49 IN.	*		*		*					*		*			*		*		*		*	*			26	
.50 TO .99 IN.		*																							18	
1.00 TO 1.99 IN.												*													4	
2.00 IN. AND OVER																									*	
TOTAL	41	49	58	62	50	39	36	40	34	30	31	34	36	38	41	41	48	52	52	41	34	36	36	39	136	

B-19

APPENDIX B, EXHIBIT B

FREQUENCY OF ANNUAL WEATHER OCCURRENCES BY WORK SHIFT

Location Portland, ME

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.016	.074	.118	.171	.579	.039	.003	.0
Afternoon	.013	.069	.118	.192	.586	.022	.001	.0
Night	.008	.057	.108	.207	.611	.009	.0	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.069	.165	.160	.156	.408	.039	.003	.0
Afternoon	.057	.161	.175	.168	.416	.022	.001	.0
Night	.044	.147	.181	.183	.436	.009	.0	.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day	.5813	.3975	.0213	Day	.4200	
Afternoon	.8438	.2212	.0125	Afternoon	.1837	
Night	.8375	.2571	.01			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day	.916	.022	.046	.016	Average .013	
Afternoon	.913	.027	.048	.012		
Night	.898	.031	.053	.018		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day	.835	.165	.069	.141	.050	.013
Afternoon	.700	.300	.057	.138	.081	.018
Night	.510	.490	.044	.123	.086	.022

Location Boston

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.002	0.036	0.089	0.168	0.641	0.055	0.009	0.0
Afternoon	0.001	0.030	0.080	0.174	0.664	0.046	0.005	0.0
Night	0.0	0.019	0.064	0.179	0.706	0.028	0.003	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.063	0.163	0.153	0.150	0.407	0.055	0.009	0.0
Afternoon	0.052	0.146	0.156	0.163	0.433	0.046	0.005	0.0
Night	0.037	0.131	0.165	0.173	0.463	0.028	0.003	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day	0.3925	0.5413	0.0688	Day	0.4150	
Afternoon	0.4838	0.4750	0.0450	Afternoon	0.1812	
Night	0.5838	0.3800	0.0325			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day	0.912	0.027	0.043	0.018	Average	.01
Afternoon	0.912	0.027	0.045	0.016		
Night	0.903	0.031	0.046	0.020		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day	0.8900	0.1100	0.063	0.101	0.040	0.003
Afternoon	0.8500	0.1500	0.052	0.091	0.041	0.003
Night	0.7800	0.2200	0.037	0.076	0.041	0.005

Location New York

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.0	0.007	0.072	0.168	0.694	0.053	0.006	0.0
Afternoon	0.0	0.005	0.061	0.170	0.719	0.042	0.004	0.0
Night	0.0	0.003	0.047	0.169	0.750	0.029	0.002	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.028	0.121	0.154	0.161	0.476	0.053	0.006	0.0
Afternoon	0.023	0.108	0.162	0.165	0.497	0.042	0.003	0.0
Night	0.016	0.095	0.156	0.172	0.530	0.029	0.002	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day	0.4763	0.4800	0.0450	Day		
Afternoon	0.5713	0.4000	0.0313	Afternoon	0.5612	
Night	0.7050	0.2738	0.0200		0.1912	

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day	0.926	0.020	0.039	0.015	Average	0.01
Afternoon	0.925	0.021	0.040	0.014		
Night	0.920	0.021	0.042	0.017		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day	0.8862	0.1138	0.028	0.078	0.040	0.006
Afternoon	0.8362	0.1638	0.023	0.067	0.040	0.006
Night	0.7325	0.2675	0.016	0.055	0.038	0.006

Location Philadelphia

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.0	0.021	0.070	0.167	0.629	0.097	0.017	0.000
Night	0.0	0.017	0.064	0.172	0.659	0.077	0.011	0.0
	0.0	0.013	0.048	0.171	0.719	0.046	0.004	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.019	0.105	0.144	0.150	0.473	0.093	0.016	0.000
Night	0.016	0.096	0.150	0.158	0.493	0.077	0.011	0.0
	0.011	0.071	0.145	0.168	0.555	0.046	0.004	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	0.6188	0.3613	0.0175	Afternoon	0.4275	
Night	0.7425	0.2475	0.0100		0.1925	
	0.8188	0.1788	0.0063			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	
Afternoon	0.935	0.018	0.036	0.011	0.01	
Night	0.929	0.020	0.037	0.014		
	0.923	0.020	0.039	0.018		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	0.9062	0.0938	0.019	0.079	0.052	0.012
Night	0.8800	0.1200	0.016	0.073	0.055	0.015
	0.7137	0.2863	0.011	0.050	0.053	0.019

Location Baltimore

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.0	.017	.065	.163	.622	.107	.025	.0
Afternoon	.0	.016	.061	.160	.660	.087	.017	.0
Night	.0	.015	.055	.166	.714	.048	.004	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.023	.110	.157	.163	.415	.107	.025	0
Afternoon	.016	.093	.151	.162	.475	.087	.017	0
Night	.012	.078	.144	.167	.547	.048	.004	0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day	.5900	.3813	.0300	Day		
Afternoon	.7136	.2688	.0138	Afternoon	.4688	
Night	.8025	.1888	.01		.2062	

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day	.933	.020	.035	.012	Average .01	
Afternoon	.927	.020	.037	.016		
Night	.929	.019	.038	.014		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day	.8912	.1088	.023	.074	.051	.009
Afternoon	.8575	.1425	.016	.068	.056	.011
Night	.6837	.3163	.012	.061	.058	.015

Location Norfolk, VA.

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.0	.003	.033	.111	.704	.121	.028	.0
Night	.0	.001	.026	.106	.752	.097	.018	.0
	.0	0	.019	.100	.811	.063	.008	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.007	.060	.112	.158	.514	.121	.028	.0
Night	.004	.049	.104	.155	.573	.097	.018	.0
	.002	.036	.092	.155	.645	.063	.008	.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	.5550	.4263	.0175	Afternoon	.4700	
Night	.7250	.2625	.0125		.1987	
	.7313	.2588	.0100			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day						
Afternoon	.935	.017	.033	.015		
Night	.927	.020	.035	.018		
	.932	.018	.037	.013		
					Average	.04

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	.9375	.0825	.007	.039	.028	.007
Night	.8375	.1625	.004	.030	.027	.008
	.6612	.3388	.002	.019	.024	.011

Location Mobile

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.0	0.000	0.008	0.043	0.689	0.210	0.049	0.000
Night	0.0	0.0	0.006	0.037	0.789	0.145	0.023	0.0
	0.0	0.0	0.004	0.028	0.874	0.086	0.008	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.001	0.022	0.059	0.117	0.541	0.210	0.049	0.000
Night	0.0	0.015	0.048	0.101	0.667	0.145	0.023	0.0
	0.0	0.009	0.036	0.082	0.779	0.086	0.008	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	0.5763	0.4088	0.0175	Afternoon	0.4862	
Night	0.7775	0.2163	0.0050		0.2087	
	0.8275	0.1638	0.0063			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	0.01
Afternoon	0.941	0.011	0.026	0.022		
Night	0.938	0.013	0.028	0.021		
	0.957	0.010	0.020	0.013		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	0.9087	0.0913	0.001	0.012	0.011	0.001
Night	0.7187	0.2813	0.0	0.007	0.010	0.001
	0.4650	0.5350	0.0	0.004	0.006	0.001

Location New Orleans

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.0	.0	.001	.023	.682	.245	.048	.0
Night	.0	.0	.0	.020	.758	.197	.026	.0
	.0	.0	.0	.015	.870	.106	.008	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.0	.012	.043	.090	.560	.246	.048	.0
Night	.0	.009	.031	.077	.662	.197	.026	.0
	.0	.005	.019	.058	.804	.106	.008	.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	.6025	.3825	.015	Afternoon	.6150	
Night	.8038	.1888	.0001		.2075	
	.8425	.1475	.0001			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	.01
Afternoon	.938	.012	.028	.022		
Night	.946	.013	.025	.016		
	.960	.010	.017	.013		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	.9125	.0875	.0	.002	.002	.001
Night	.8087	.1913	.0	.001	.002	.002
	.4800	.5200	.0	.001	.001	.003

Location Houston

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.0	0.0	0.002	0.024	0.652	0.248	0.073	0.0
Night	0.0	0.0	0.001	0.024	0.728	0.202	0.045	0.0
	0.0	0.0	0.002	0.022	0.855	0.108	0.013	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.001	0.014	0.048	0.106	0.510	0.248	0.073	0.0
Night	0.0	0.012	0.044	0.094	0.602	0.203	0.045	0.0
	0.0	0.011	0.033	0.081	0.754	0.108	0.013	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	0.4713	0.4838	0.0463	Afternoon	0.4400	
Night	0.5600	0.4188	0.0188		0.2000	
	0.7463	0.2425	0.0100			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	
Afternoon	0.953	0.013	0.026	0.018	0.01	
Night	0.955	0.013	0.020	0.012		
	0.960	0.012	0.017	0.011		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	0.9000	0.1000	0.001	0.005	0.004	0.0
Night	0.8000	0.2000	0.0	0.004	0.004	0.0
	0.4637	0.5363	0.0	0.004	0.003	0.0

Location Galveston

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.0	0.0	0.0	0.013	0.653	0.324	0.010	0.0
Night	0.0	0.0	0.0	0.012	0.681	0.301	0.007	0.0
	0.0	0.0	0.0	0.009	0.717	0.270	0.004	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.001	0.015	0.041	0.089	0.519	0.324	0.010	0.0
Night	0.0	0.015	0.036	0.080	0.561	0.301	0.007	0.0
	0.0	0.012	0.028	0.066	0.619	0.270	0.003	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	0.4550	0.5163	0.0300	Afternoon	0.4987	
Night	0.5763	0.3975	0.0263		0.2112	
	0.6275	0.3438	0.0300			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average .005	
Afternoon	0.955	0.011	0.021	0.013		
Night	0.968	0.010	0.014	0.008		
	0.963	0.010	0.016	0.011		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	0.8850	0.1150	0.001	0.002	0.001	0.0
Night	0.7987	0.2013	0.0	0.002	0.001	0.0
	0.69	0.31	0.0	0.001	0.0	0.0

Location San Diego, CA

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.0	.0	.0	.001	.963	.033	.003	.0
Night	.0	.0	.0	.0	.986	.013	.0	.0
	.0	.0	.0	.0	.991	.008	.0	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	.0	.0	.0	.018	.946	.033	.003	.0
Night	.0	.0	.0	.016	.971	.013	.0	.0
	.0	.0	.001	.018	.973	.008	.0	.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	.8638	.1350	.0025	Afternoon	.6265	
Night	.9638	.0350	.0013		.2750	
	.9800	.0200	.0013			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	.01
Afternoon	.983	.006	.007	.004		
Night	.981	.006	.010	.003		
	.975	.009	.013	.003		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	.9862	.0138	.0	.0	.0	.0
Night	.9512	.0488	.0	.0	.0	.0
	.8275	.1725	.0	.0	.0	.0

Location Los Angeles

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.0	0.0	0.0	0.001	0.966	0.030	0.002	0.000
Afternoon	0.0	0.0	0.0	0.000	0.988	0.011	0.0	0.0
Night	0.0	0.0	0.0	0.002	0.989	0.009	0.0	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	0.0	0.000	0.006	0.049	0.912	0.030	0.002	0.000
Afternoon	0.0	0.0	0.002	0.040	0.946	0.011	0.0	0.0
Night	0.0	0.0	0.004	0.041	0.946	0.009	0.0	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day	0.7838	0.2100	0.0063	Day		
Afternoon	0.8675	0.1275	0.0038	Afternoon	0.3950	
Night	0.9738	0.0263	0.0013		0.2600	

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day	0.974	0.006	0.008	0.012	Average 0.01	
Afternoon	0.978	0.005	0.014	0.003		
Night	0.977	0.007	0.011	0.005		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day	0.9737	0.0263	0.0	0.0	0.0	0.0
Afternoon	0.9112	0.0888	0.0	0.0	0.0	0.0
Night	0.7762	0.2238	0.0	0.0	0.0	0.0

Location Portland, OR

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.0	.002	.019	.097	.842	.033	.006	.0
Afternoon	.0	.001	.018	.111	.834	.032	.004	.0
Night	.0	.0	.019	.176	.803	.002	.0	.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day	.006	.034	.096	.184	.641	.033	.006	.0
Afternoon	.004	.034	.102	.200	.624	.032	.004	.0
Night	.001	.032	.135	.275	.554	.002	.0	.0

Shift	Wind Speed		
	<13	13-24	25+
Day	.7638	.2238	.0100
Afternoon	.7763	.2163	.0088
Night	.8600	.1325	.0075

Shift	Cloud Cover
	Sunny
Day	
Afternoon	.2987
Night	.1500

Shift	Precipitation			
	None or Trace	.01	.02-.09	.1+
Day	.880	.043	.067	.010
Afternoon	.884	.043	.063	.010
Night	.885	.041	.065	.009

Fog (Visibility <1/16 Mile)	
Average	.01

Shift	Relative Humidity	
	90	90-100
Day	.8712	.1288
Afternoon	.8275	.1725
Night	.6250	.3750

Correction of Effective Temperature for Painters Only			
<5	5-19	20-29	30-39
.006	.018	.016	.012
.004	.034	.019	.015
.001	.014	.029	.028

Location Seattle

FREQUENCY OF ANNUAL OCCURRENCES

Shift	Drybulb Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.0	0.003	0.018	0.123	0.838	0.016	0.002	0.0
Night	0.0	0.002	0.017	0.138	0.830	0.013	0.001	0.0
	0.0	0.001	0.015	0.199	0.783	0.002	0	0.0

Shift	Effective Temperature							
	<5	5-19	20-29	30-39	40-79	80-89	90-99	100+
Day								
Afternoon	0.005	0.056	0.158	0.247	0.517	0.016	0.002	0.0
Night	0.002	0.056	0.169	0.263	0.496	0.013	0.001	0.0
	0.001	0.064	0.211	0.320	0.402	0.002	0	0.0

Shift	Wind Speed			Shift	Cloud Cover	
	<13	13-24	25+		Sunny	
Day				Day		
Afternoon	0.6000	0.3638	0.0338	Afternoon	0.2962	
Night	0.6088	0.3688	0.0225		0.1475	
	0.7200	0.2638	0.0188			

Shift	Precipitation				Fog	
	None or Trace	.01	.02-.09	.1+	(Visibility <1/16 Mile)	
Day					Average	0.02
Afternoon	0.902	0.031	0.059	0.008		
Night	0.883	0.047	0.061	0.009		
	0.864	0.058	0.068	0.010		

Shift	Relative Humidity		Correction of Effective Temperature for Painters Only			
	90	90-100	<5	5-19	20-29	30-39
Day						
Afternoon	0.8050	0.7950	0.005	0.022	0.025	0.009
Night	0.7600	0.2400	0.002	0.027	0.027	0.011
	0.4925	0.5075	0.001	0.018	0.040	0.020

APPENDIX C

WEATHER EFFECTS ON OUTDOOR WORK EFFICIENCY

A review of the literature was undertaken to establish, to the extent possible, quantitative efficiency coefficients for outdoor workers engaged in "shipyard-like" activities, as influenced by climatic conditions. Unfortunately, the published literature in this area provides little useful information in a form that can be directly applied. Where data are available, generally they are in the form of physiological factors which are not directly related to either weather factors or laborer efficiency.

From the limited literature which is applicable (see Bibliography at end of the Appendix), the following summary of weather effects can be established.

The important climatic conditions affecting outdoor workers are:

- Temperature: high, low, diurnal and annual range
- Precipitation: rain, snow, sleet and ice
- Humidity: also presences of salt
- Wind: also presence of sand or dust
- Miscellaneous: sunlight, fog.

Temperature

Figure 1 summarizes data from eight sources. Variations reflect measurements of work activities requiring different skills. Furthermore, some efficiency loss data were compiled from studies where only the tempo of the actual work was measured. Time to warm the hands or feet in winter, or time to cool off in summer, was not included. These higher estimates of efficiency are, therefore, probably conservative, since total loss in work time was not

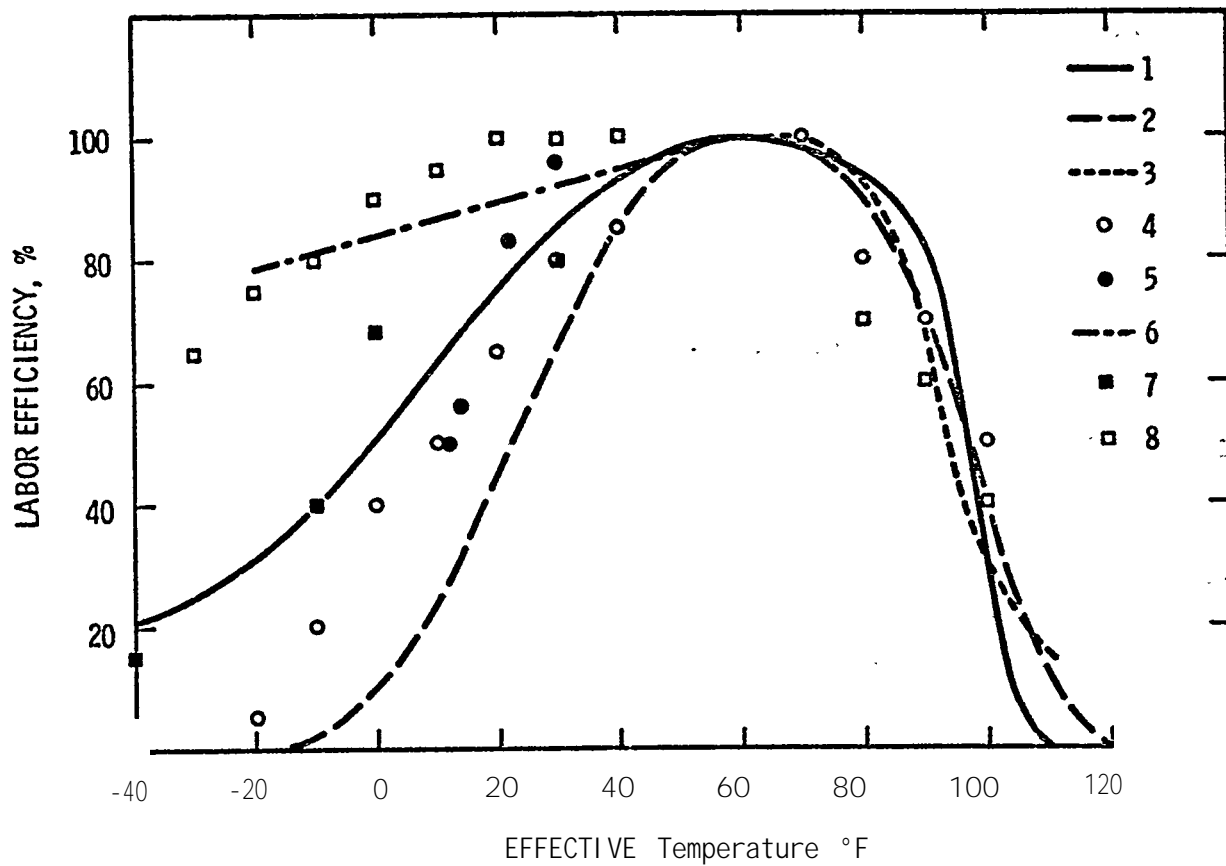


FIGURE C-1. Outdoor Worker Efficiency

LEGEND

1. Doyle, "Controlling Climate Effects", Tool Engr., 1955 (efficiency curve prepared under condition of little or no wind).
2. General Dynamics, Quincy (DX Study).
3. ASHVE Guide and Data Book (men at work 90,000 ft-lb of work per hour).
4. Constructor, May 1972 (welders, pipefitters, carpenters, electricians).
5. Unidentified shipyard estimate (converted from equivalent temperature to effective temperature).
6. Bechtel construction project in Canada (winter) - (Converted from wind chill temperature and corrected to 100% efficiency at 60°F).
7. ASHVE Guide and Data Book (Armstrong's data for line-maintenance job).
8. Constructor, May 1972 (laborers, ironworkers, operating engineers).

really considered. Another factor that would decrease efficiency even further is bad "ground" conditions resulting from ice, water or mud. When such conditions prevail, the estimates are quite conservative.

Wind

Human efficiency is significantly affected by cooling, which is a function of both temperature and of wind speed. Studies by the U.S. Army Quartermaster Corps resulted in the computation of a "wind chill factor" by which the effect of temperature and wind can be objectively evaluated (see Figures C-2 and C-3). Most outdoor operations cease when the chill factor reaches 1200, "bitter cold".

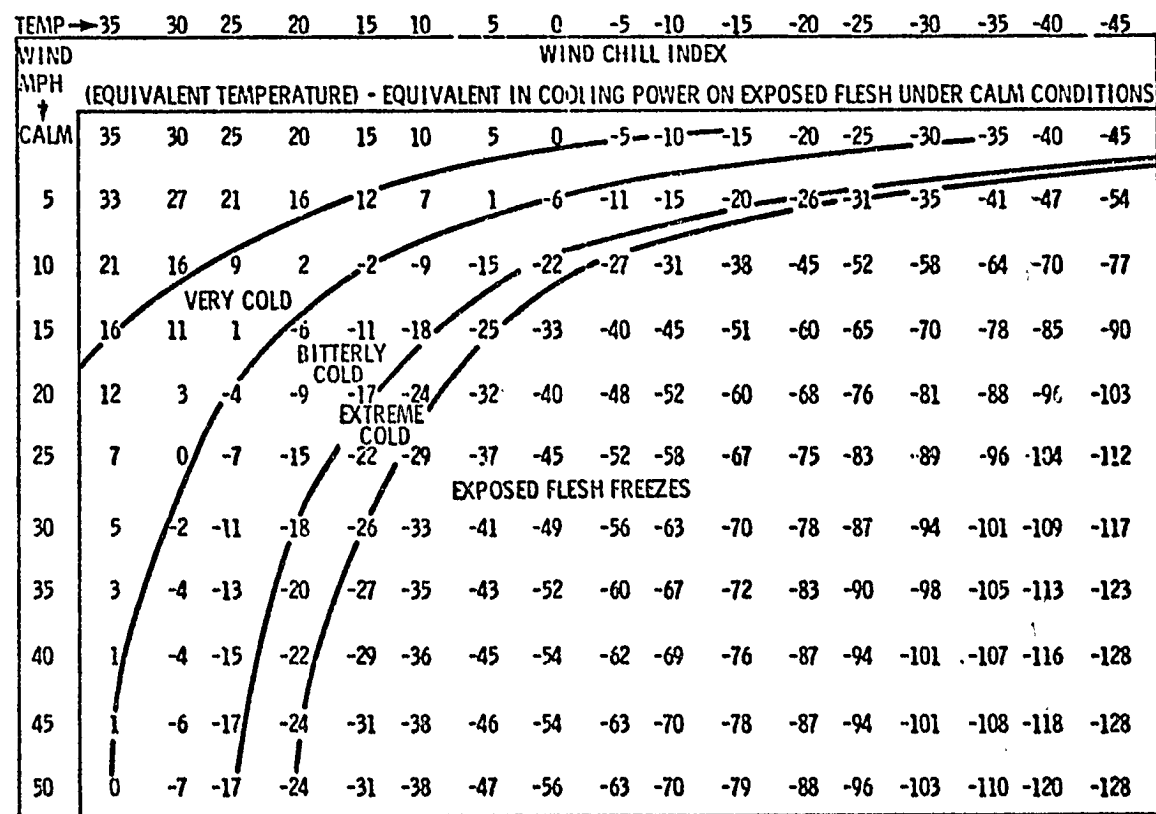
Wind also hinders the movement and positioning of large pieces and increases paint losses. Wind "noise" reduces effective communication between workers. Wind-blown dust and salt sprays increase maintenance problems with equipment.

Another method used to measure the effective of temperature and wind is effective temperature (ET). The ET is determined from dry- and wet-bulb temperatures and air motion by reference to standard ET charts. When a wind is blowing, the ET can be estimated by lowering the measured temperature one degree for each one mile per hour of wind, using a practice adopted by environmental engineers.

The curves in Figure 1 are plotted against ET although the difference between ET and wind chill temperature (equivalent temperature) is seldom great. The ET index is most applicable to warm atmospheres when radiation effects are not significant. An ET of 78 represents the threshold of sweating, while an ET of 90 is the upper limit for continuous exposure of heat-acclimatized men engaged in light activities. The upper permissible limit for moderately hard work is an ET of 85, and for heavy work, 80 ET. In hot spaces of Naval ships (underway), 91 ET is well tolerated during the usual 4-hr watches.⁽¹⁾

At moderate temperatures, depending upon the work being done, labor efficiency gradually declines with increasing wind speeds over 15 mph and

C-4



WIND SPEEDS GREATER THAN 40 MPH HAVE LITTLE ADDITIONAL CHILLING EFFECT

Figure C-2 - The U.S. Army Wind Chill Index

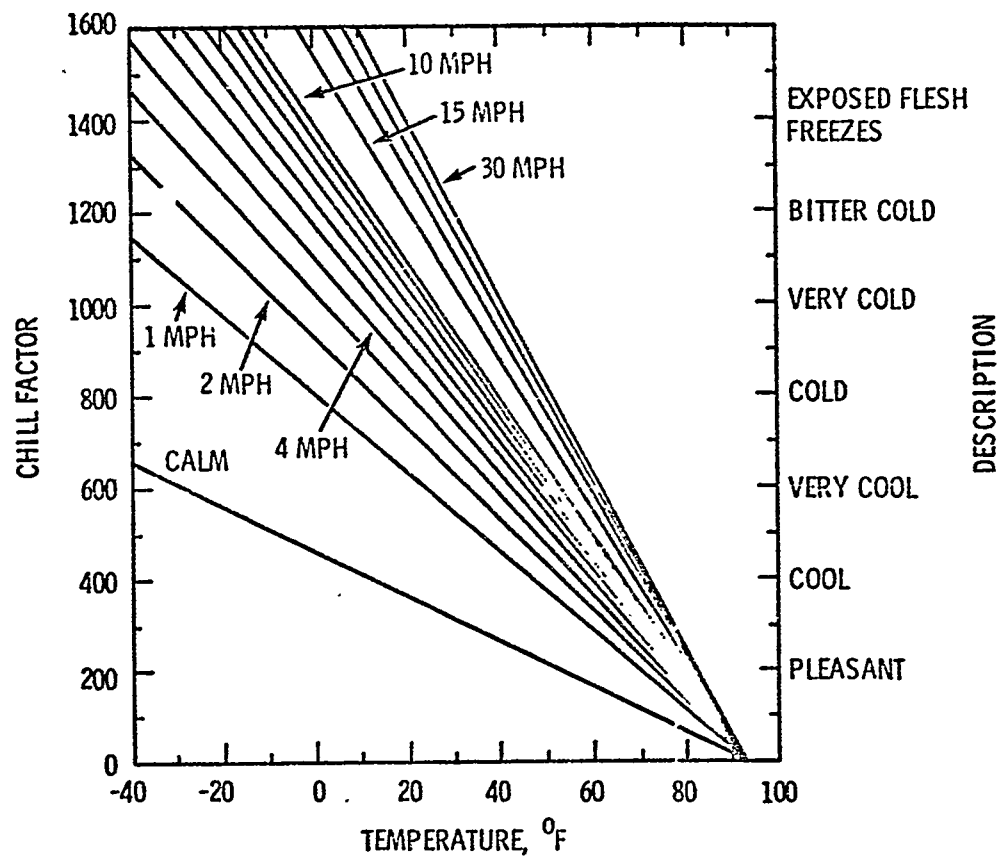


Figure C-3 - Chill Factor for Selected Wind Speeds

rapidly approaches zero between 40 and 60 mph. Winds of 40 mph are likely to stop work on exposed staging.⁽¹⁾

Precipitation

Rain decreases efficiency. Under rainy conditions at 50°F and without wind, workers well clothed in rain trousers, jackets, hats and boots lose only about 10% in efficiency. When exposed to rain and strong winds, men cannot remain dry for much more than one hour regardless of how well they are clothed.

At low temperatures, labor efficiency and safety are still further impaired by precipitation. Sleet or ice are considered more limiting to outside work than rain or snow. Workers will generally not continue working during a sleet storm. Precipitation has been found more serious than freezing temperatures in reducing efficiency of an outside railroad car building line in a mild climate. In 23 days of rain, 97 cars or about 35% were lost out of a scheduled 278. During 5 days of ice, snow, sleet and rain, 28 cars or 50% were lost out of a scheduled 56. Only 4 cars out of 14 were reported lost because of cold weather alone.

Besides discomfort, precipitation decreases efficiency by decreasing visibility; making parts, tools, and equipment slippery and hard to handle; and making working conditions more hazardous.

Humidity

Several comfort indexes have been devised to express the effect of temperature and humidity. There is general agreement that the comfort zone for normally efficient work extends to about 80°F with 50% relative humidity and to the mid-70's with 75% relative humidity. Discussions with construction personnel indicate that operations are not significantly affected until the temperature rises above 80°F. It is estimated that a reasonable threshold of temperature-humidity would be 85°F and 50%. This corresponds to a U.S. Weather Bureau Temperature-Humidity Index value of 77, and Table 1 gives several combinations of temperature and relative humidity that are equivalent.⁽²⁾

TABLE 1. U.S. Weather Bureau Temperature-Humidity Index

<u>Temperature</u>	<u>Relative Humidity</u>	<u>Index</u>
86	79	77
85	50	77
90	24	77
95	8	77

Reduced efficiency appears to occur at the following limits of temperature and humidity:⁽⁸⁾

<u>Maximum Temperature</u>		<u>Humidity</u>
85-89°	and	<u>>50%</u>
90-94°	and	<u>>30%</u>
95-99°	and	<u>>20%</u>
100°	and	Any

Night Lighting

Shipyard estimates for improper lighting (outdoor areas) range from 10 to 25% productivity loss. Survey results by others show increases in work output of 3 to 20% are possible for heavy work activities similar to shipbuilding. These increases were brought about by illumination changes. Atypical example: original-4.6 fc, new-12.7 fc.

FOG

The, effect of fog is to reduce visibility. In shipbuilding this affects primarily riggers and crane operators who must be able to see the boom, the load being lifted and hand signals. Reduction of visibility to less than the boom length or the distance to a signaler stops crane work.

The 100% humidity accompanying fog also affects painting operations. It usually prevents painting outdoors.

Sunlight

The effect of sunlight, e.g. hot summer sun, is to reduce worker efficiency not only by raising the effective temperature but by heating steel plates to uncomfortably high temperatures. Personnel working on sun-heated surfaces are often forced to retire to a shaded area, provide shade or find work in a cooler location.

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APPENDIX D

TYPICAL HEATHER PROTECTION STRUCTURES IN U.S. SHIPYARDS

In the course of the study, nine U.S. Shipyards were visited. Photographs of some of the weather protective devices and structures were obtained and are shown on the following pages.

In addition to those devices pictured, numerous shelters of a temporary nature--plywood, tarpaulin or plastic on wood or scaffold framework--are used for rain and wind protection. Several shipyards use portable weather protective devices to keep welding electrodes dry. Each welder has a heated container which holds 10 pounds of electrodes and can be carried from place to place and plugged in to an outlet nearby. Used containership containers have also been utilized for storage, shops and office space in a U.S. shipyard.

An all-weather painting facility at the General Dynamics yard in Quincy, Massachusetts, has been in operation since 1968. It is able to handle subassemblies up to 50 ft square and 30 ft high. The facility includes climate control for painting and drying, telescoping doors for access, and a heating-ventilating system rated at 75,000 cfm.

The Ingalls Shipyard at Pascagoula, Mississippi, has installed a weather-protected shotblasting facility. It is able to handle 56 ft by 56 ft sections up to-100 tons.

Other examples of weather protection are shown in the following photographs.

D-2

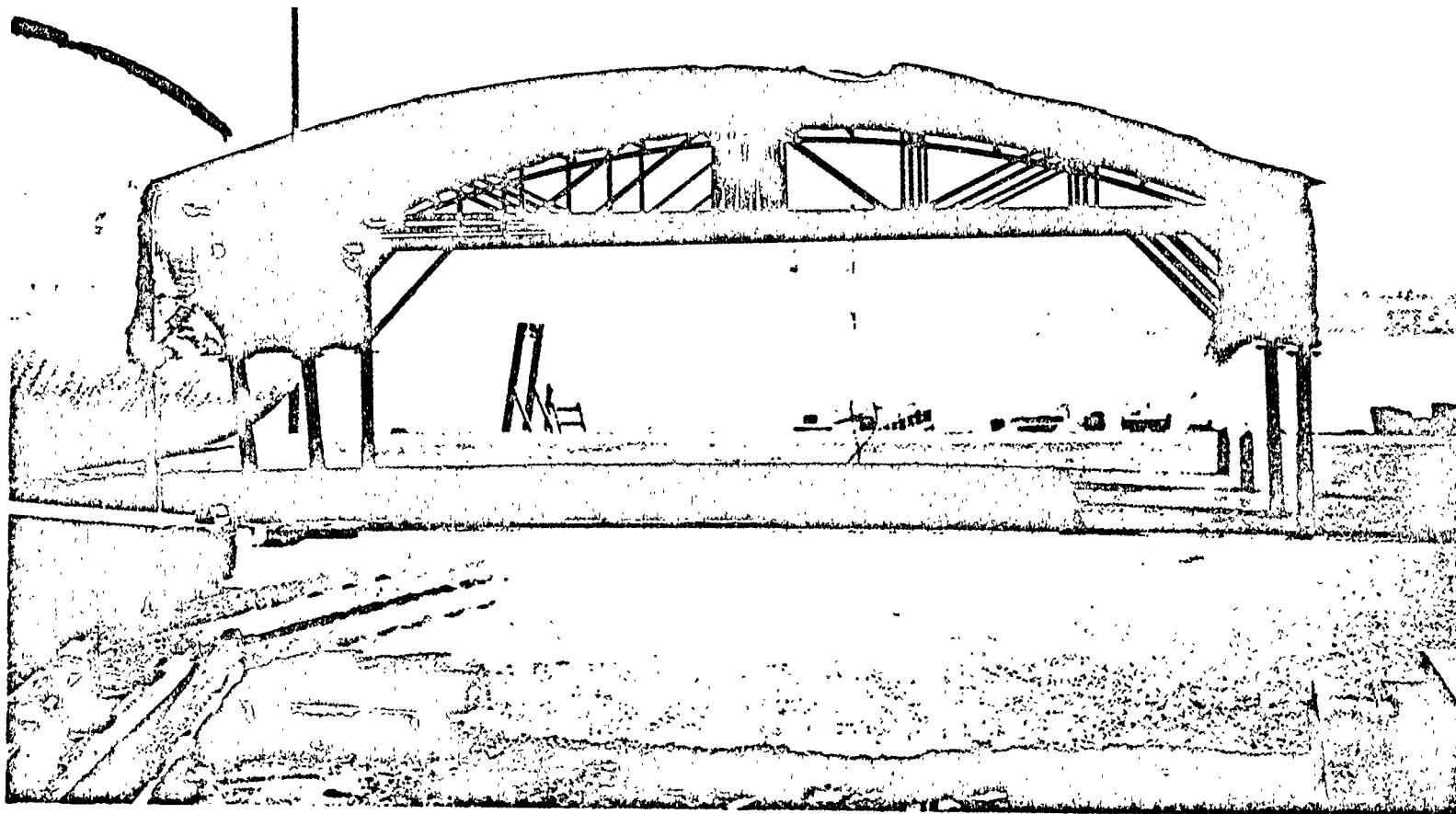


Figure D-1 - A portable steel shelter used to provide rain protection and shade for shipyard work either on the ground or on the deck of a ship or barge. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.

D-3

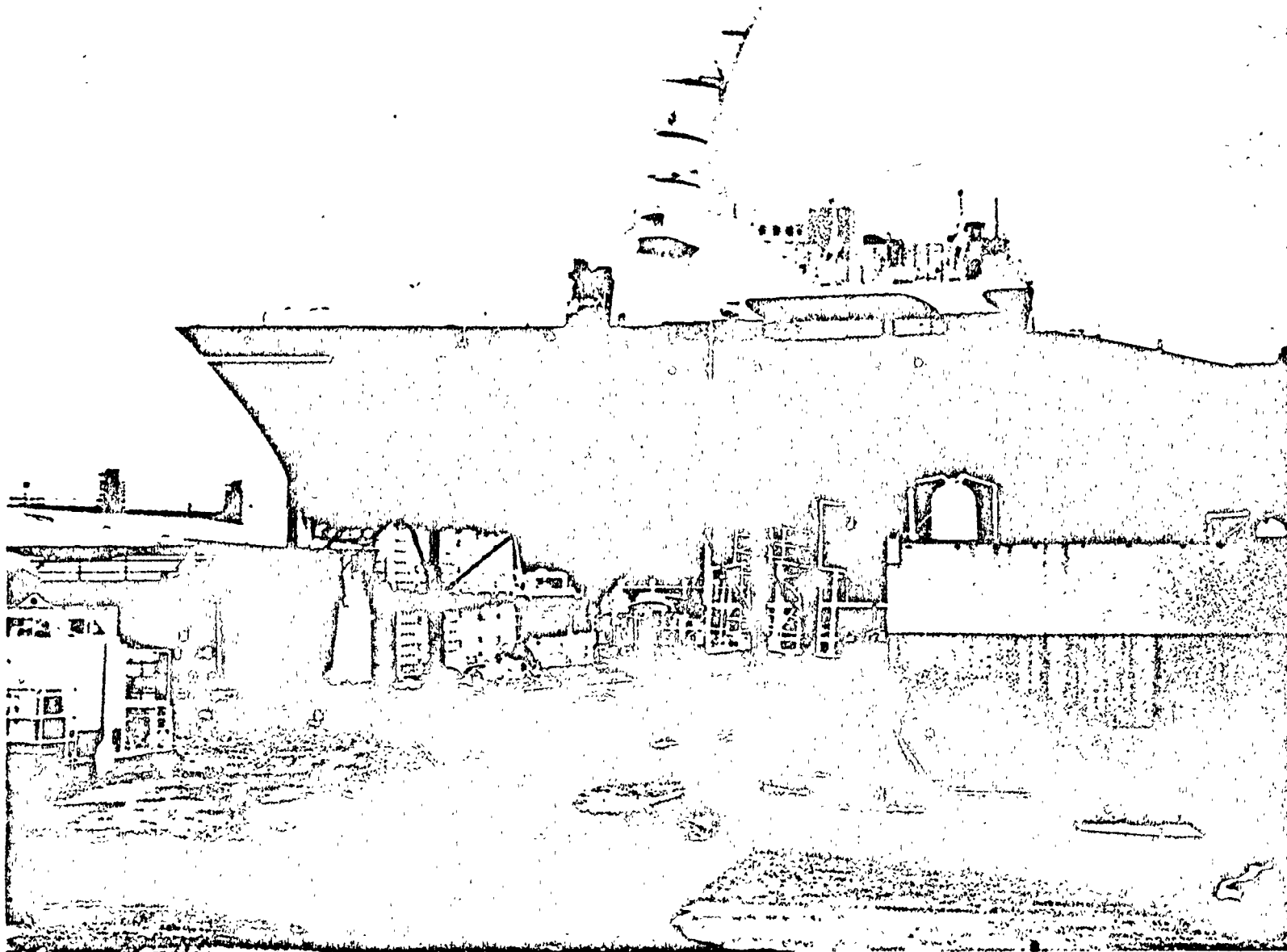


Figure D-2 - A portable steel shelter used to provide rain protection and shade for shipyard work either on the ground or on the deck of a ship or barge. Courtesy of Avondale Shipyards, Inc., New Orleans, Louisiana.

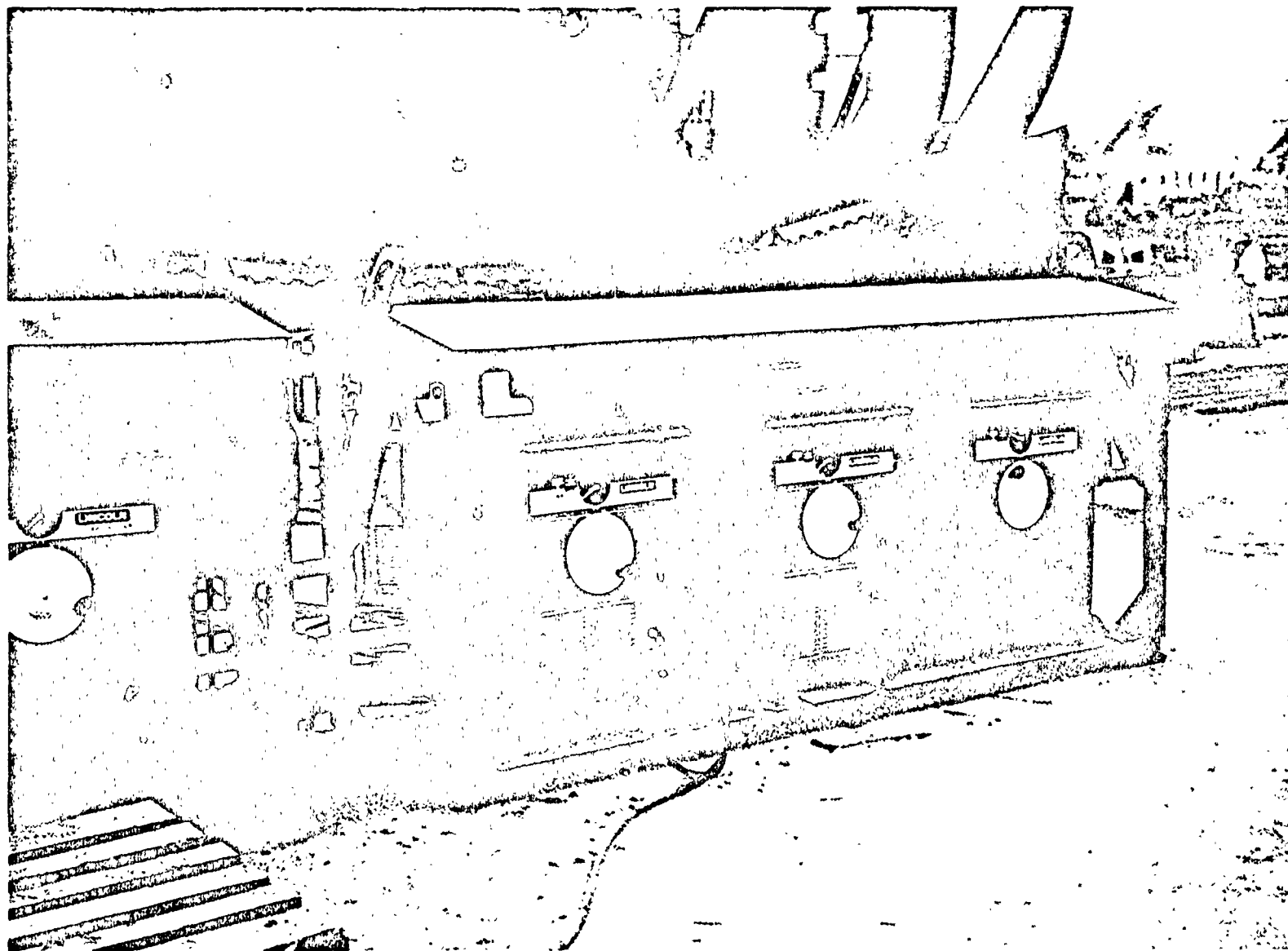


Figure D-3 - A close-up of a weather protective device for welding machines. The roof provides protection from the rain and hot sun both of which tend to shorten machine life. Fastening the machines to the frames gives an added bonus of rapid portability. Courtesy of Todd Shipyards Corporation, Houston, Texas.

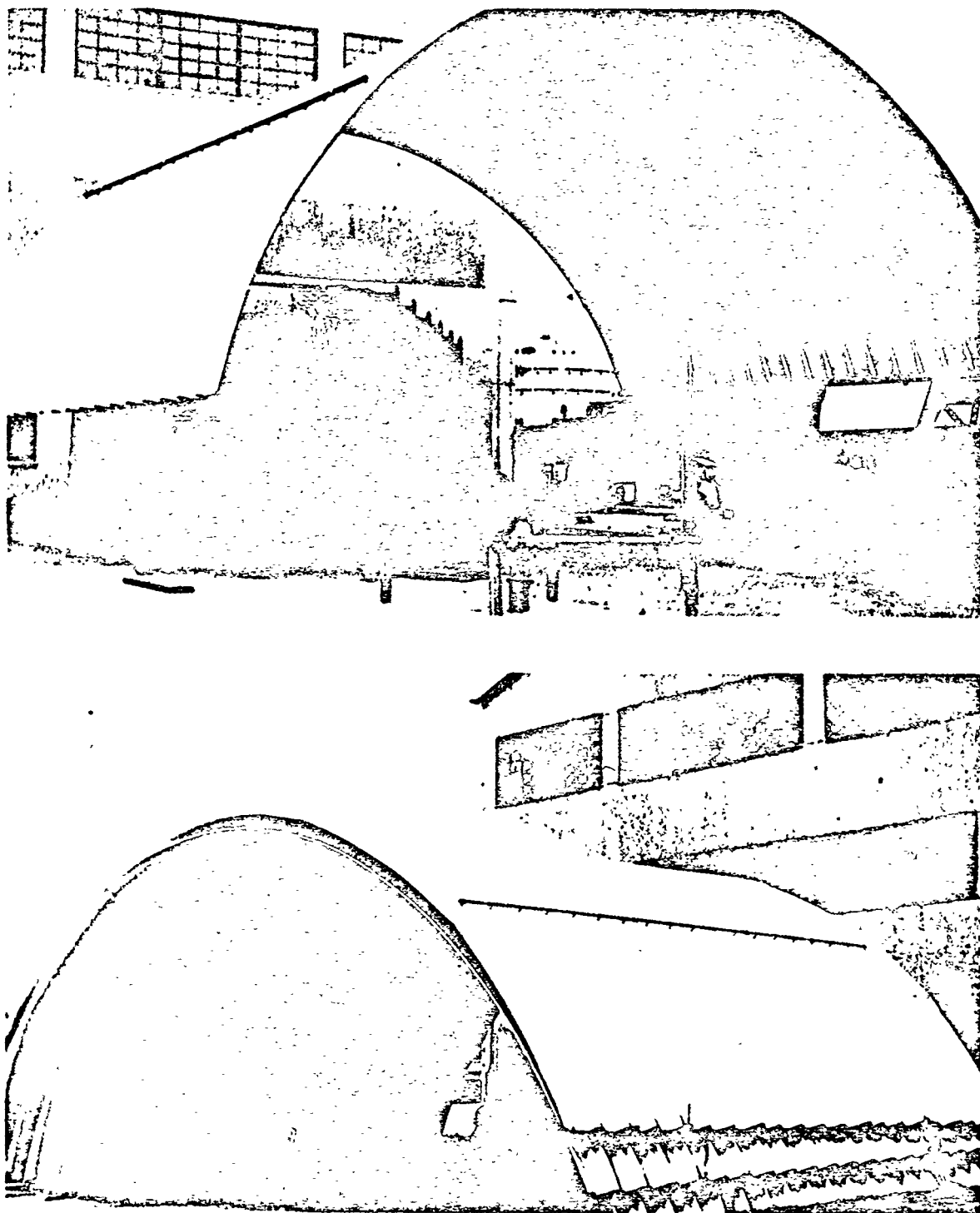


Figure D-4 - Heavy corrugated sheet metal roofs ("Wonderbuilding" arches) used for rain and shade protection for various operations. Units can be nested for storage as shown in lower photo.

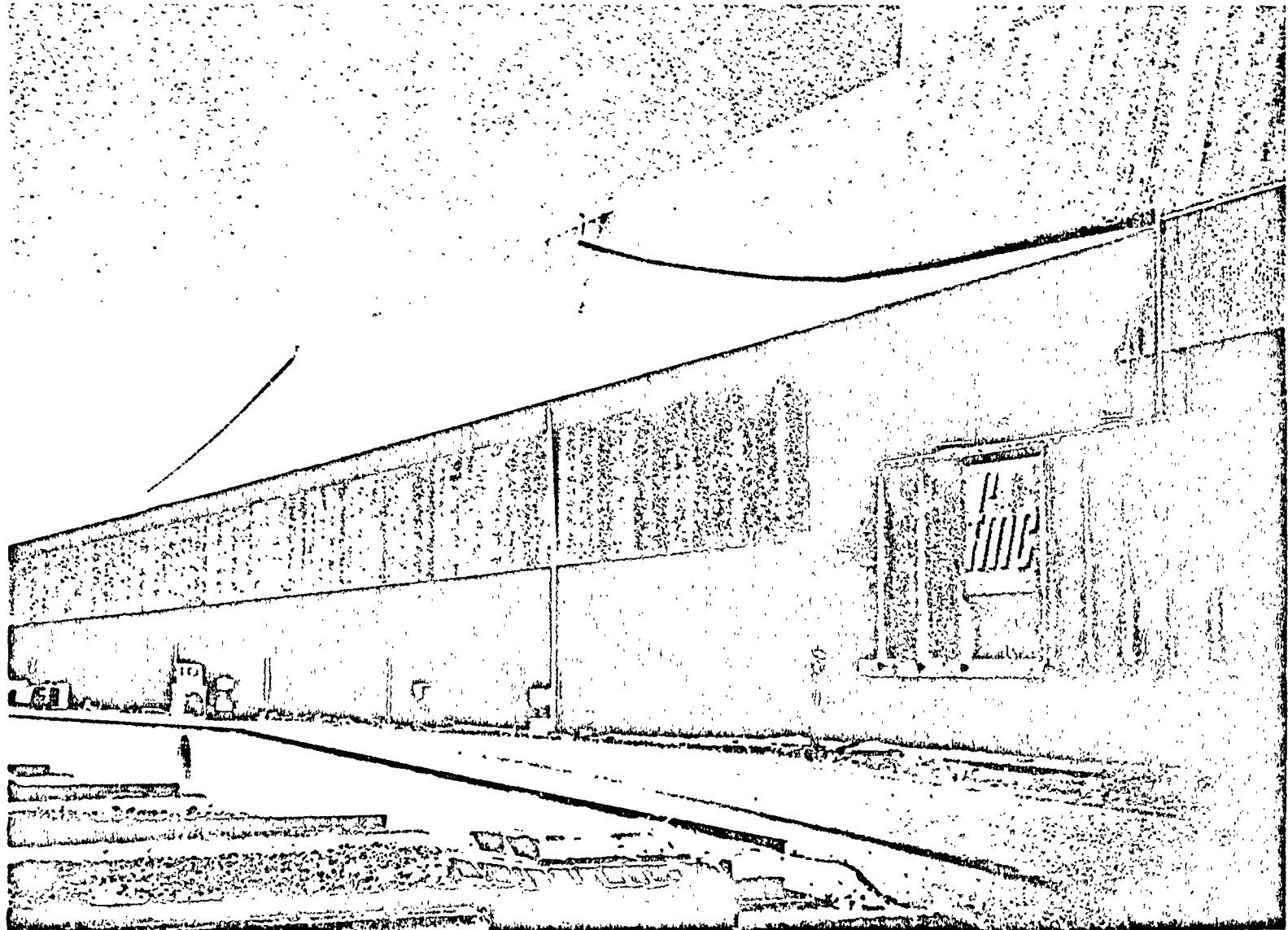


Figure D-5 - A lean-to addition used for rain and sun protection in heavy manufacturing (rail car). The shelter allows work to proceed in bad weather when it might otherwise be forced to shut down. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.

D-7

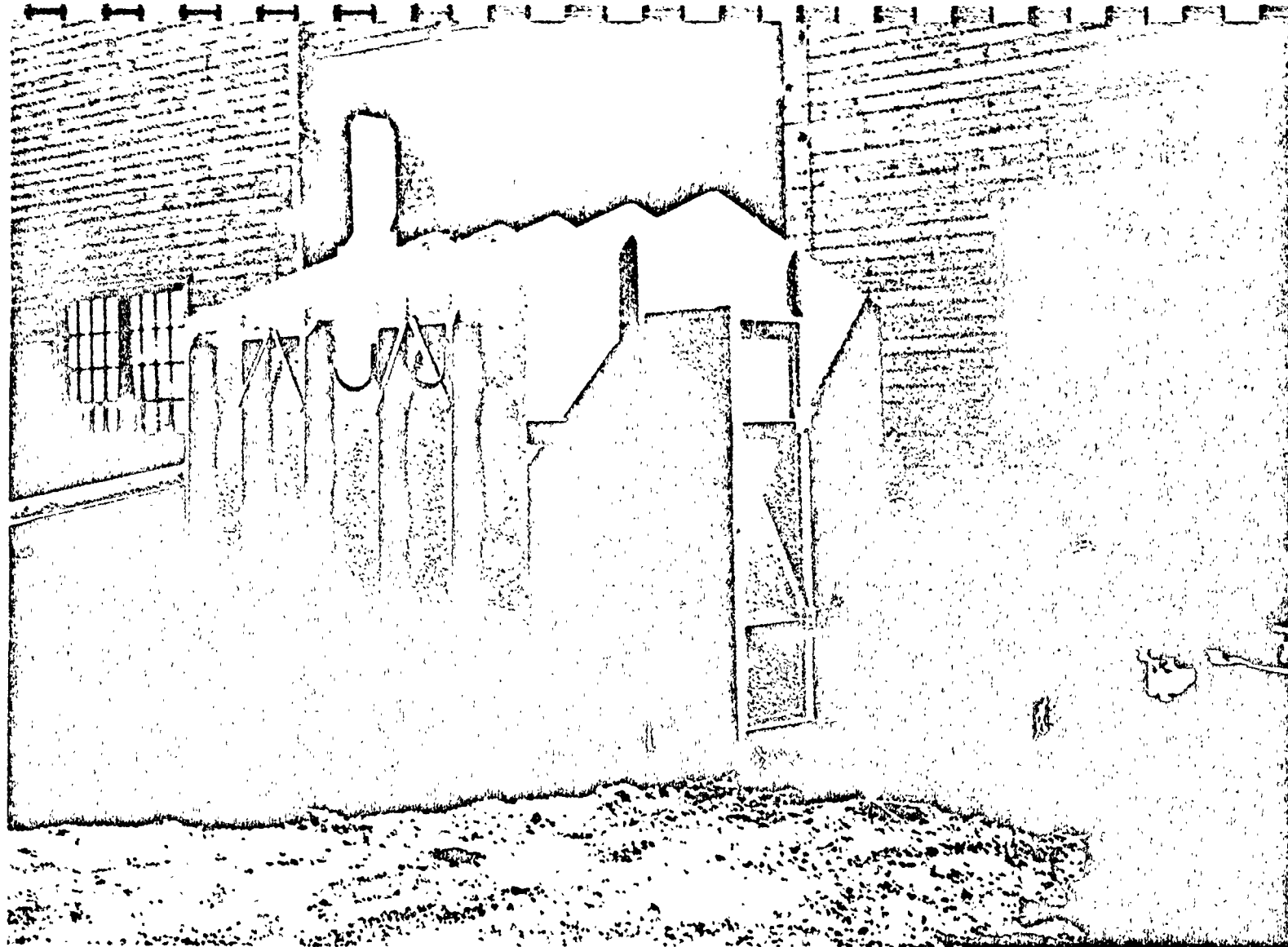


Figure D-6 - An all-weather protective shed for storage of paint and paint pumps. Electrically heated, it is a complete, portable paint station which prevents freezing of stored paint and the paint pumps and pots themselves. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.

D-8

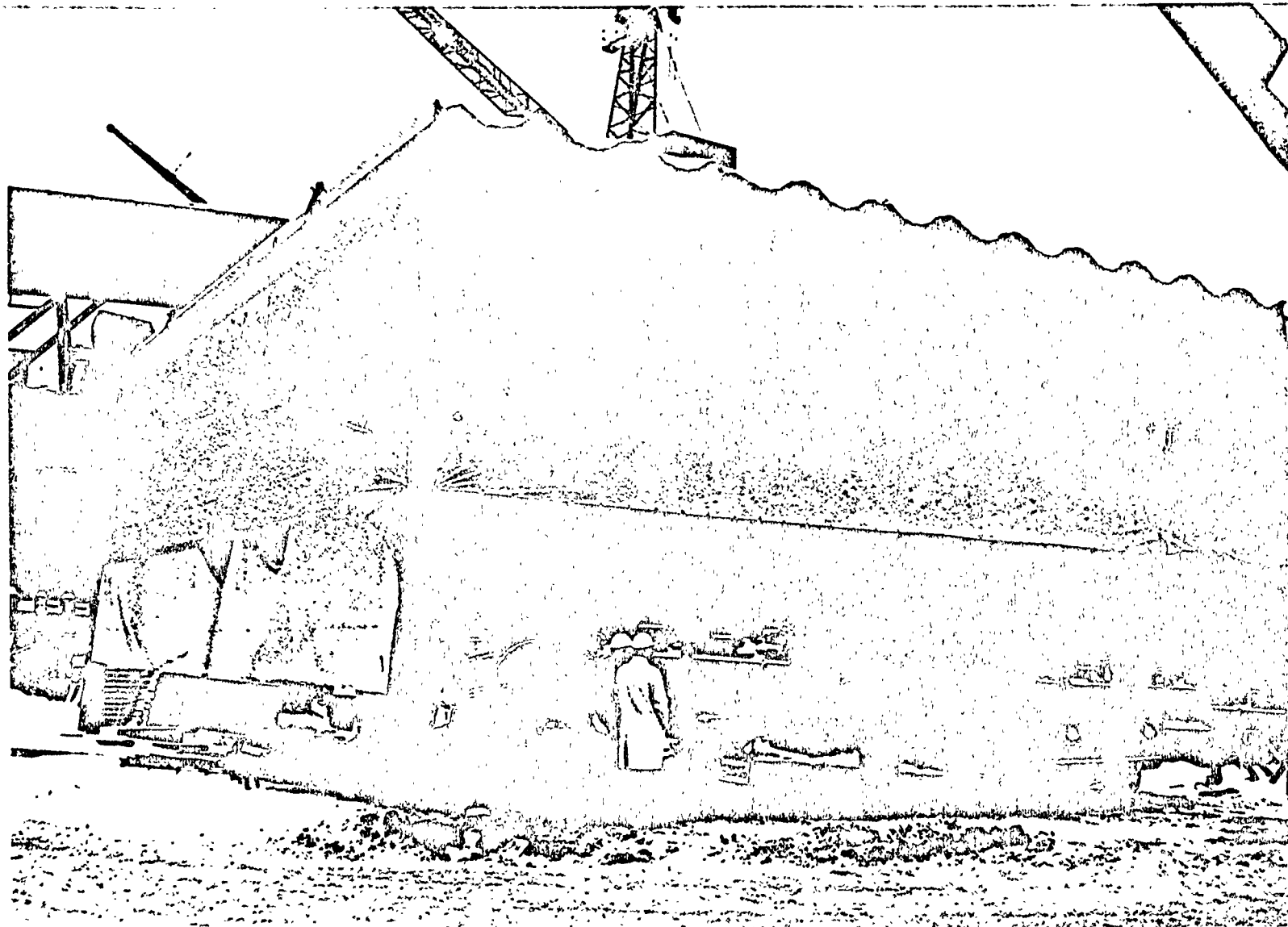


Figure D-7 - Temporary weather protective shelter. These portable structures measure 40 ft x 50 ft in plan with roof heights varying from 12-30 ft. The roof grid is assembled from cold rolled beams and supported on pipe columns. The roof cover is large corrugation metal sheeting. Removable rubberized canvas sidewalls provide additional protection. The shelter encloses sufficient volume to protect a variety of welding, blasting, painting and storage activities. Courtesy of Bath Iron Works Corporation, Bath, Maine.

1. RAIN REMOVAL SYSTEM TO HANDLE 4" OF WATER PER HOUR WHEN ROOF IS INSTALLED ON SLOPES UP TO 5/8" PER FOOT AND NOT ALLOW WATER TO PUDDLE CAUSING FREEZE DAMAGE.
2. SAFETY POLES AROUND HATCH OPENING TO FOLD DOWN OR OTHERWISE BE STOWED ON ROOF. CABLES MAY BE CONNECTED TOGETHER WITH SAFETY HOOKS OR EQUIV.
3. ROOF AND HATCH TO HAVE INDEPENDENT LIFTING PROVISIONS.
4. WALKWAYS TO BE EXPANDED METAL TYPE OR EQUIV. NON SKID MATERIAL.
5. ROOF TO BE STABLE ON SLOPES UP TO 5/8" PER FT.
6. ROOF TO HAVE ABILITY TO BE STACKED 4 HIGH AND WITHSTAND '2G' IMPACT LOADS.

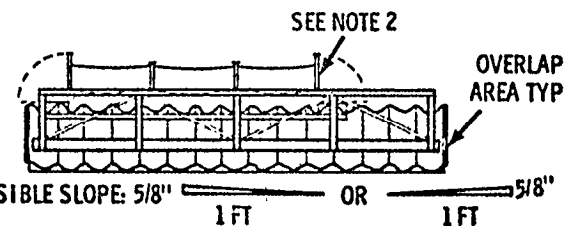


Figure D-8 - Design for a Portable, Trussless Cover with Hatch for Hull Construction - Newport News Shipbuilding and Dry Dock Company.

APPENDIX E

MODULAR WEATHER PROTECTION PANELS

HOARDING PANELS

Typical Design Criteria

1. Diffusion of Light

Hoarding panels should be such that no auxiliary light is required during the normal daylight.

2. Resistance to Wind

Closure system should be such that it could stand the high winds during the winter months (up to 70 mph).

3. Strength of Panels

Enclosures should be such that they could support the load of the different panel sections when installed one on top of the other. When used as the roof, they should also be able to support the snow load.

4. Loss of Heat

The closure should be such that the heat loss is at a minimum.

5. Versatility

Closures should be such that they could be adapted to numerous configurations, re: stand alone structures, structural steel requirements, etc.

Design Specifications

To meet the above criteria, one contractor assembled hoarding panels in an 8'-0" x 16'-0" size, which were constructed of 2 x 4 spruce frame with 2 x 4 studs at 2'-8" on center. Reinforced woven polyethylene was applied on the frame and was held in place by 1 x 2 lumber strips all over the frame and studs. Design of the hoarding panel is shown in Figure E-1.

E-2

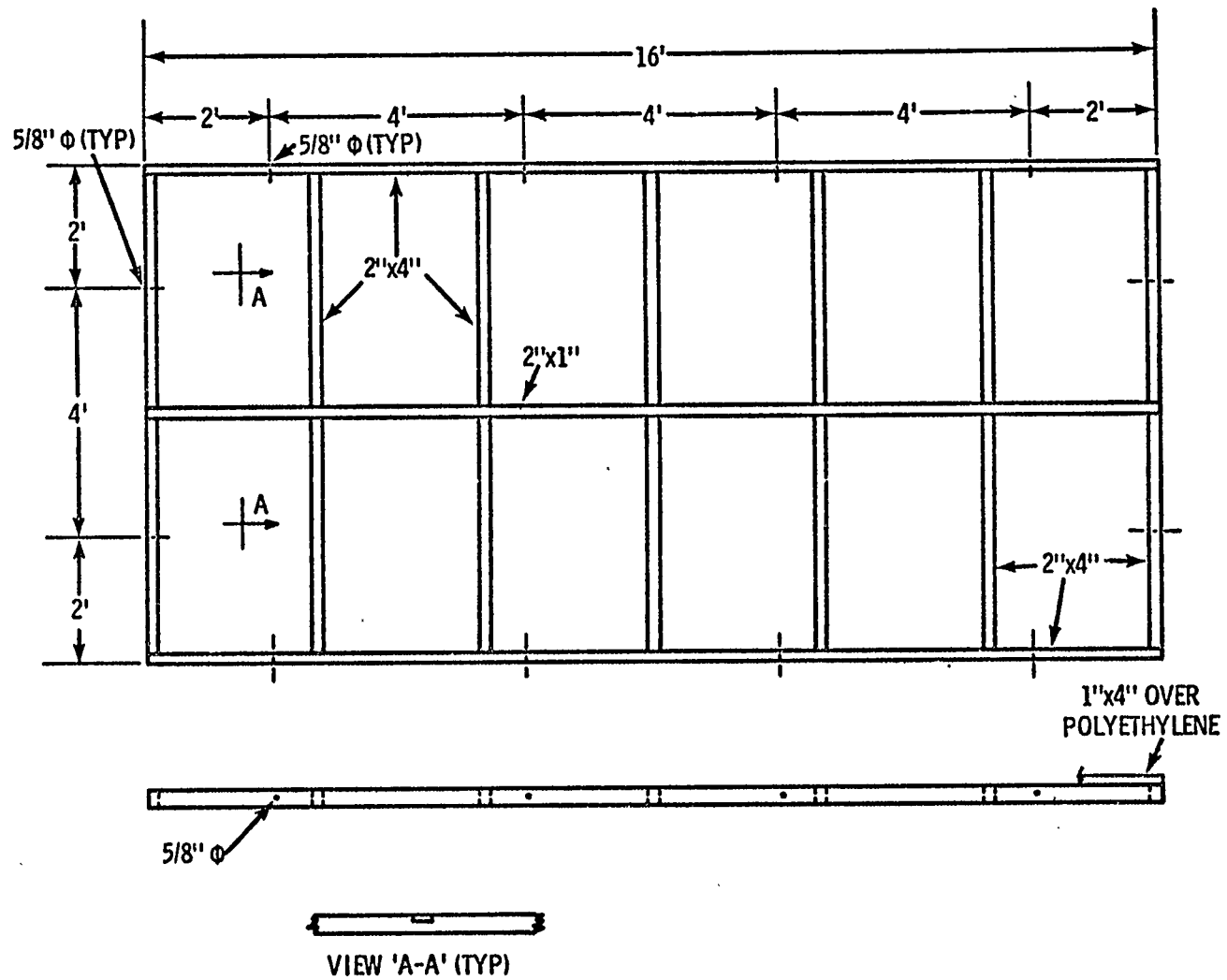


Figure E-1 - Design of Hoarding Panels

For the fabrication of the hoarding panels, a jig was made which permitted panels to be made in different sizes: 8' x 16', 6'x 16', 4' X 16', 2' X 16'.

To minimize heat loss, two layers of polyethylene can be used, if necessary, with air gap up to a maximum of one inch between the two layers.

Erection

Hoarding panels are secured together by a tie and wedge system. Panels are then nailed to small wooden frames built around the steel building frame as shown in Figure E-2.

For the construction of structures inside a main building, hoarding panels are attached to one another to forma closure.

Cost of Hoarding Panels

A cost studies indicated that it is more economical to fabricate panels on the job site rather than purchase or rent them from others. Total cost of the hoarding panels is about \$0.40/sq ft with a cost breakdown as follows:

Material	\$0.09 Sq ft
Manufacture Labor	0.44 "
Erection Labor	0.19 "
Dismantle Labor	<u>0.08 "</u>
Total	\$0.40 Sq ft

Average cost of one panel, 8x 16 ft= \$48.00.

Figure E-3 illustrates portable welder's shelter used in civil construction works.

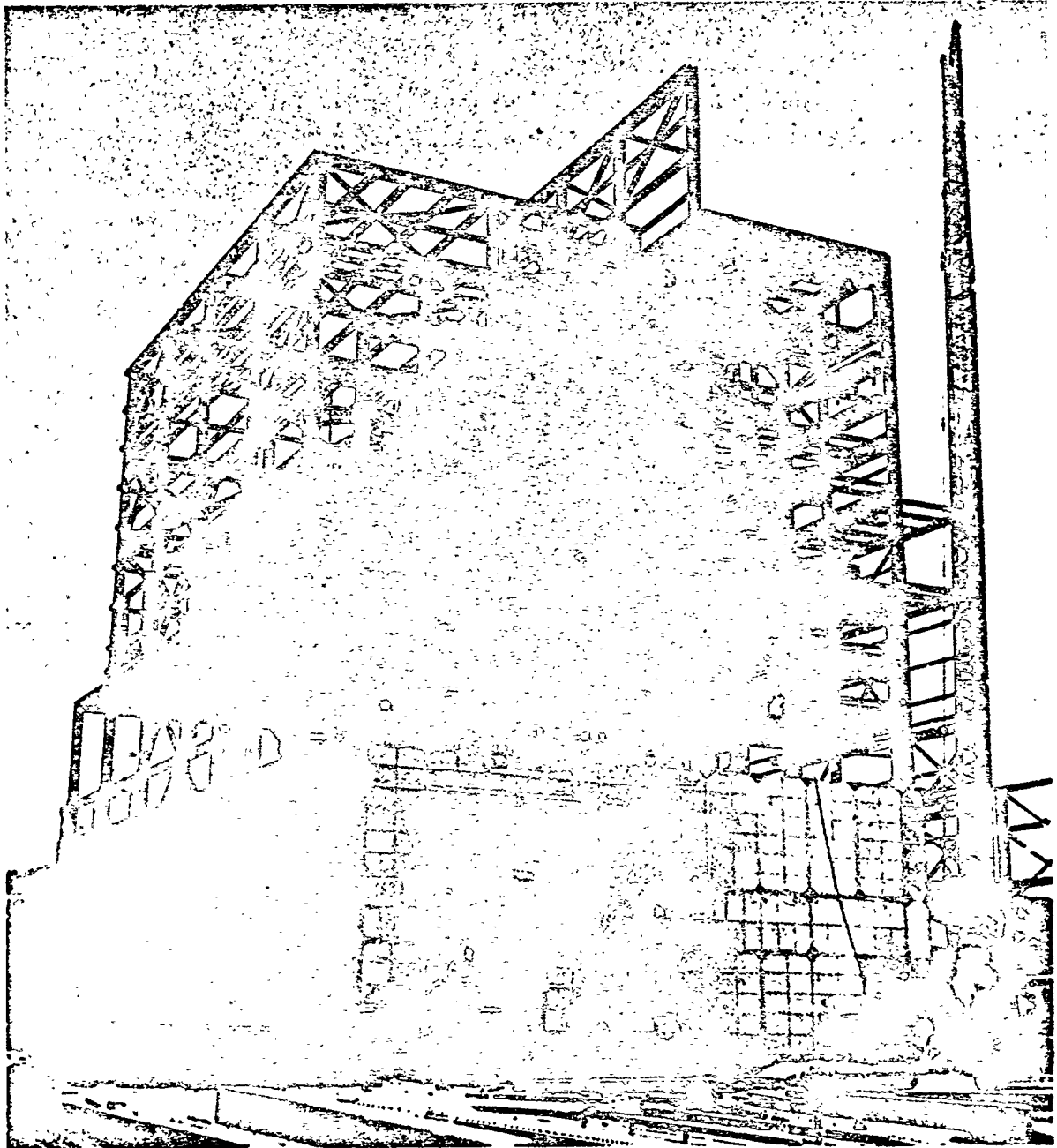


FIGURE E-2 - Hoarding Panels Attached to Building Frame to Form Weather Enclosure.

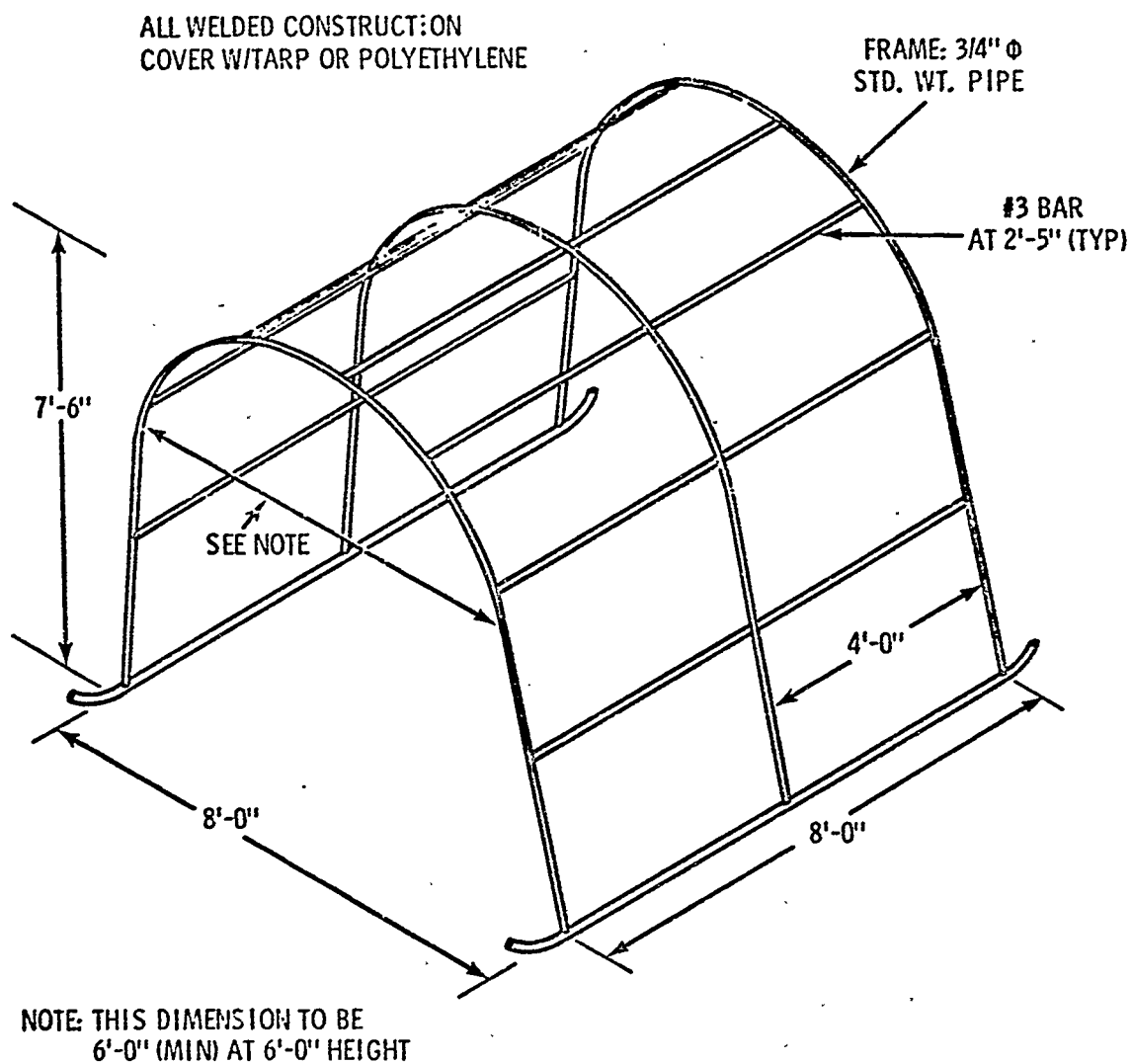


Figure E-3 - Portable Welder's Shelter

APPENDIX F

DESCRIPTION OF AIR-SUPPORTED SHELTER

A large, most unique shelter used on a civil works project in Canada was an "air shelter" or, as it is commonly called, a "bubble". It is an air supported structure, a strong, flexible, balloon-like envelope, supported and stabilized by maintaining a small pressure differential within the envelope. The air supported shelter is a dynamic structure, as contrasted with a static pile of bricks, mortar or timbers, and is the ultimate in structural efficiency. There is no redundancy of structural material in the pretensioned shell and the apparent simplicity of the shelter belies the actual complexity of the design of all its components. The shell must tolerate and resist all the normal loadings experienced by any other type of structure. It does so with a shell measuring only a few hundredths of an inch thick.

Physical characteristics of the shell material, seam design, loading around the doorways, and the pressurization system must be carefully chosen and controlled to ensure satisfactory life and usefulness.

The structure was 100' wide, 200' long, and 50' high, with ends that were almost 'square". It covered an area of almost 20,000 sq.ft., the surface area of the shell was 35,000 sq.ft. The fabric was guaranteed for eight years.

The bubble used a vinyl-coated nylon with a 2x 2 basket weave, having a tensile strength of 400 x 400 lb/in. The material was described as off-white which admitted sufficient light during the daytime for all types of work. Inside, the shell appeared to be an unusual orange-yellow color.

The joints were heat sealed to develop the full-strength of the fabric. The envelope was supplied in three sections which were joined by a single interlocking peg system which was readily assembled or disassembled without special tools. The sectionalizing permitted the individual packages to be kept to a reasonable size to handle and, also gave flexibility to the ultimate size of the shelter by adding or subtracting additional center sections when required.

Sandbags were installed in the ballast skirt, approximately six cubic feet of sand per foot of periphery, to hold the shell down and solid anchors were provided for the attachment of cables to isolate and redistribute the load around the doorways.

Two Buffalo-Forge, Model 600A, 3 H.P. centrifugal blowers, each having a free delivery of 14,000 cfm provided sufficient pressure for normal operation and the other was used for unusual conditions as well as being a standby unit. The inflation pressure was just less than one inch of water, which resulted in a pressure of approximately 5 lb/sq.ft.

Automatic pressure controls operated the second blower when the internal pressure dropped because of excessive leakage through open doors or damage to the shelter or because of failure of the primary blower.

A plywood airlock, twenty feet wide, twenty feet high and thirty feet long with full opening access doors was used to permit the passage of all materials, trucks, and cranes. Small doors were installed in the airlock for personnel ingress or egress to avoid using the main doors and two additional emergency exits were also provided in the sides of the shelter.

The inlet air to the blowers was heated by six Herman-Nelson oil-fired heaters which were enclosed in a temporary shelter. The maximum output of the heaters was 1-1/2 million BTU/hr. The thin shell does not provide very good insulation qualities and the overall heat transfer coefficient is approximately 1.2 BTU/hr/°F/sq.ft. which is similar to single glazing.

The introduction of the heat through the blowers gives good distribution, and as the mass of the structure is low, the internal temperature can be increased rapidly.

The delivered cost of the shelter was just over \$50,000 \$2.50/sq.ft.

The weight of the suplliment was 8706 pounds and occupied a volume of 720 cu. ft.

The shelter was first erected in early February over the excavation for the foundation of the Final Extraction Plant. The temperature ranged from 20° above zero to 22° below zero. The erection was completed within two working days by a crew of sixteen men. No real problems arose despite the complication of raising the shelter over the large excavation. The structure was completely dismantled, at the end of its useful period, in four hours.

The shelter possesses several advantages over the more conventional types of hoarding, such as:

- 1) The interior is completely free of posts, trusses, cables, or other supporting members, this allows for more flexibility of operation and construction.
- 2) The blowers provide a natural circulating media for heat, which is provided by any type of heater located outside the working area. This saves space and also reduces the fire hazards.
- 3) The skin is translucent and little additional illumination is required during daylight hours. This factor can be a major item for more conventional types of shelter.
- 4) The structure can be reused, as required, with no loss of material, as many times as necessary. While the original cost is higher than other types of hoarding, even only a second reuse would be economical.

The disadvantages of the structure must also be considered:

- 1) Limited working area and height inside the shelter. This is not too serious for small, low buildings, but the work must proceed slower than outside. The handling of material and equipment through the airlock has to be planned and coordinated.
- 2) The loss of air pressure, for any reason, could be disastrous. All sharp projections on rebar, forms, etc., were covered with a plywood cap to avoid damage to the skin, should the shelter collapse. In good weather, little damage should result, however in a storm (which also

increases the possibility of power failure) the structure could be completely destroyed.

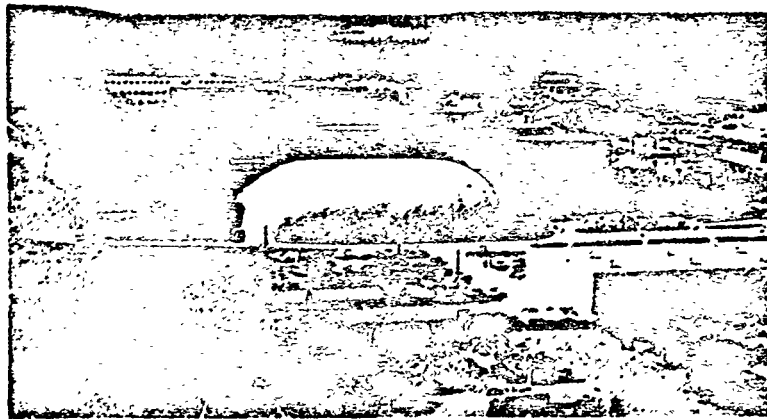


Figure F-1 - View of the 100' x 200' 50' high air shelter. A large vehicle access air lock is at the left end of the structure.



Figure F-2 - Concrete form work in progress inside the air shelter. Note the height of the columns, the wooden caps on top of the reinforcing steel to protect the skin in case of a loss in pressure. Also note the excellent natural light.

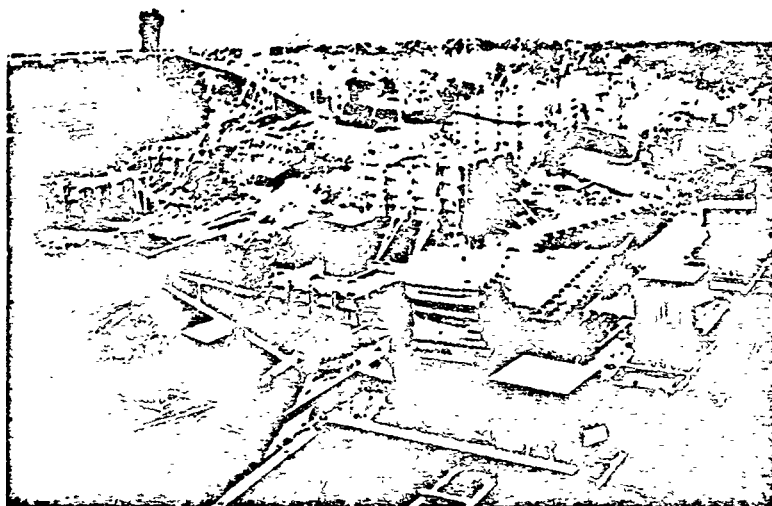


Figure F-3 - An earlier view in the air shelter. Note the trestle supporting the base of the "bubble" over the excavation. The workers in the upper left are standing in front of a small man-made access way.

APPENDIX G
INFORMATION SOURCES

Information on the effects of weather on outdoor worker productivity and methods to provide weather protection was sought through letter contacts with the following:

Trade Associations

1. Associated Builders and Contractors
2. Associated General Contractors of America
3. Building Research Advisory Board
4. Building Research Institute
5. American Concrete Institute
6. American Society of Concrete Constructors

Construction Firms

1. American Dredging Company
2. The Austin Company
3. Bow Valley Industries, Ltd.
4. Bovis Corp., Ltd.
5. Dravo Corp.
6. Dravo of Canada, Ltd.
7. Fluor Corporation
8. General Construction Company
9. J. A. Jones Construction Company
10. Kaiser Industries Corp.
11. M. W. Kellogg (Div. of Pullman, Inc.)
12. Michigan Wisconsin Pipe Line Company
13. Morrison-Knudsen Company, Inc.
14. Guy F. Atkinson Company
15. Blaw-Knox Company
16. C. F. Braun and Company
17. Chemical Construction Corp.-
18. Hoffman Construction Company

19. Whitehead Kales Company
20. Genstar, Ltd.
21. Bechtel Corp.
22. ITT Levitt and Sons, Inc.
23. Pullman, Inc.
24. Ocean Drilling and Exploration Company
25. Ocean Service and Engineering, Inc..
26. The Ralph M. Parsons Company
27. Pacific Car and Foundry Co.

Research Organizations

1. Cold Regions Research and Engineering Laboratory
2. Environmental Protection Systems Division
3. Fordham University
4. National Bureau of Economic Research
5. Naval Arctic Research Laboratory
6. Rand Corporation
7. Stevens Institute of Technology
8. U.S. Department of Commerce
9. University of Illinois
10. University of Michigan
11. Department of the Army, Construction Engineering Research Laboratory

REPORT OF THE STUDY FOR
DETERMINING THE STATE-OF-ART OF
THE USE OF WEATHER PROTECTION IN
THE JAPANESE SHIPBUILDING AND
HEAVY EQUIPMENT INDUSTRIES.

to
Battelle Pacific Northwest
Laboratories

May, 1973

Mitsubishi Research Institute
1-1, Yurakucho, Chiyodaku
Tokyo, Japan

Preface

This is the Final Report on the Study for Determining the State-of-the-Art of the Use of Weather Protection in the Japanese Shipbuilding and Heavy Equipment Industries, based on the Special Agreement B-654, signed on 31st, October 1972, between the Battelle Pacific Northwest Laboratories and Mitsubishi Research Institute.

The study has been carried out according to the principles and definitions stated in the Research Proposal dated 15th November 1972, made by The MRI on the subject above stated. The Draft Report of MRI, dated 27th March 1973, was reviewed by BNW and succeeding comments were met and incorporated into the Final Report.

Japanese experience on the weather protection for outdoor works are unique and has a history of nearly two decades in many shipyards. Weather Protection facilities in these shipyards are one of the cause of productivity improvement in Japanese shipbuilding industries, competing in the world market with foreign shipbuilders.

It would be the first time to describe the state-of-the-art of the use of and the cost-effectiveness of the weather protection devices in Japan in a comprehensive way for foreign people who have the interest on it.

We hope this Report will be good for the use for the sponsors in U.S.

May 1973

S.Ikeda, General Manager
T. Miyakawa, Senior Transportation
Economist
Research and Development Department
Mitsubishi Research Institute,
Tokyo, Japan.

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1. The method of study and other explanations

First we have surveyed the usage of weather protection facilities among 25 major Japanese shipyards to get overall picture. Then, we have selected four shipyards, located at places with a wide weather variation and represent different type of workshop layouts, i.e. one from northern region, one from central region and two from western region of Japan. We have asked for these four shipyards necessary data for weather protection devices used and carried out enquete survey to engineers at workshops to get data for productivity gains. Photographs were taken on the protection facilities studied during these enquete surveys on the spot.

As for the heavy construction industry we have selected one large steel construction site located central region of Japan. We add brief survey of crane and wharf protection during extreme climatic conditions, the data for which were obtained simultaneously during the survey on the spot.

This study was carried out by us with close cooperations of engineers in the Shipbuilding Division of Mitsubishi Heavy Industries Ltd.

2 Selection of Shipards and a Large-scale Construction site to be Investigated

Pattelle Northwest are requesting to obtain the informations on shipyards, having a range of typical climatic conditions. We set two criteria for the selection of shipyards. The first is the criteria by the climatic conditions and the second is the one concerning the layout of the shipyards.

2.1. The Criteria by the climatic conditions.

The climatic conditions concerning out-door heavy construction works in Japan can be devided into following three types (for detailed explanation on each climate see comments p.9 seq.)

- 1) Eastern Japan-Pacific Coast
- 2) Western Japan-Pacific Coast
- 3) Northern Japan

Whereas the difference in climate between Eastern Pacific Cost and Western Pacific Coast are not so clear except the duration of rainy months during summer, this difference on rainy weather would be significant in considering the out-door working conditions. The climate in Northern Japan differs clearly from the other parts of the country. Despite the relatively low latitude (for example Sapporo, the capital of Hokkaido is at 35°N), the climate there has the same characteristics like Northern Europe, in higher latitude. Thus we need, at least, three types of shipyard that are locating in each of one climatic conditions mentioned aboved.

2.2. The criteria concerning the layout of shipyard.

In Japan there are 45 major shipyards that have at least one shipbuilding berth over 5,000 gross tonnage. Among these, 23 shipyards have been building the major part of new ships. These 23 large shipyards that have at least one building berth over 30,000 gross tonnage, can be divided into 3 groups in terms of the date of their establishment.

First group of shipyards are old ones that were established before or during the World War II and some of them even dated from one hundred years ago. The layout and the construction flow of these old shipyards have been modernized and renewed as possible within the limited land use after the War, especially during the Suez Crisis shipbuilding boom, (1956-58), and the second boom after 1963.

The second group of shipyards are completely new giant shipyards that are established upon the reclaimed land, and its layout were designed to achieve the most effective construction. These shipyards were erected mainly after 1965. Whole of them have building docks that can build super tankers over 100,000 gross tonnage.

The third group is the most newly established and the largest shipyards. They have large building decks in which tankers up to one million dwt can be built. They began their operation around 1970.

The types of weather protection devices used among these shipyards depend on the differences of the duration of operations since shipyard's establishment and subsequent modernization and their final layouts.

2.3 The differences of the use of weather protection devices among the type of shipyards.

In Japanese shipbuilding industry, the means to prevent the fluctuation of productivity in the outdoor welding and assembling works due to the variation of weather, have been improved significantly during these decade.

In the most old conventional type of shipyards, the outdoor works in hull construction yard were changed and arranged to fit into the large welding and black assembling factory during the later half of 1950's. In the case of Nagasaki shipyard (Mitsubishi Heavy Industries), these improvements were carried out through following process.

- (1) change of the flow of sheets
- (2) modernization of sheet bending and cutting process
- (3) enlargement of welding spaces
- (4) increase of crane capacities
- (5) construction of huge roof overwelding and small block assembling yard
- (6) integration of welding work and small-block assembling work

At the end of covered assembling factory, hull blocks, usually 50 to 80 metric tons in average, were lifted up and down directly onto the adjacent building berths by the giant gantry cranes. Thus the most parts of hull construction stages were covered by the roofs except final assembling processes that were carried out on the building berths. These improvement, which included the change of factory layout partly, was completed by the end of 1957, when the ratio of outdoor works was reduced to only 14 percent to the whole hull construction works. The layout of building berths were changed again substantially during 1965-68 to enlarge building capacity at Nagasaki. These improvement consisted of the integration and increase of width of old berths, replacement of old gantry cranes to giant goliath cranes and construction of new building docks. The crane capacities were increased from 50 tons to 120 tons and thus the maximum size of blocks to be supplied from the assembling factory reached up to 120 tons. However major flow of hull blocks remained, in principle, the same as before.

These "indoorization" of outdoor welding and assembling works were carried out, in general, through similar processes in other major shipyards on the Pacific Coast during 1955-1965.

The plannings and constructions of the new shipyards in the second group began around 1960 among the largest shipbuilding companies. In this case, some of the Swedish examples of advanced shipbuilding technology and novel ideas incorporated into the layout of ships within shipyards, e.g. those at the Arendal Shipyard of Gotaverken A/B, had a considerable influence upon the planning of new larger shipyards in Japan. In these new generation of shipyards, the most part of outdoor works were "indoorized" from the beginning, having large welding and block-assembling shops. For example, in Yokohama Shipyard of Ishikawajima-Harima Heavy Industries Co., Ltd., there are five indoor welding and block-assembling shops, each 853 feet long and 115 ft. wide. Hull block over 100 tons can be assembled in these shops. The outdoor works remain only at the final assembling stage on the uncovered building dock.

This New Yokohama shipyard of IHI began its operation 1968.

In the third group of new shipyard, even the large building dock is covered partly by the roof. For example, in Koyagi Shipyard of Mitsubishi Heavy Industries, the maximum size of a hull block which can be assembled within assemble shops are 600 tons. Over the buildingdock, that is 3182 ft. long and 328 ft. wide, there are two sets of travelling roofs each 164 ft-long and 328 ft. wide. Thus, the works in the final stage of ship-construction are partly "indoorized". This newest shipyard has just begun its operation in this year.

2.4. The Selection of shipyard

We select three large shipyards each located in different climatic conditions from layout type 1, that is Shipyard W from Eastern Japan, Shipyard X from Western Japan and Shipyard V at Northern Japan. For the method used in the indoor welding assembling works in the type 2 shipyards are the same to those are used in the type 2, we do select no shipyard from the layout type 2, However we add Shipyard Y from layout type 3. (cf. Table 1),

Although we will survey the use of weather protection facilities in these four shipyards in depth, we supplement the result with further informations on other shipyards, if we find significant exceptional examples to the fact surveyed.

Table 2-1 Classification of Shipyards. (1) (2)

Type of Layout Climatic Condition	Type I.	Newly Built large Shipyard	
	Old but modernised	Type II.	Type III.
Eastern Japan	IHI-Tokyo, IHI-Nagoya, MHI-Yokohama NKK-Tsurumi Sumitomo	Mitsui-Chiba IHI-Yokohama	NKK-Tsu
Western Japan	IHI-Kure IHI-Aioi MHI-Nagasaki MHI-Kobe MHI-Hiroshima Kawasaki-Kobe Mitsui-Tamano Hitachi-Innoshima Osaka Sasebo	Kawasaki-Sakaide Hitachi-Sakai	MHI/Koyagi
Northern Japan	Hakodote Hitachi-Maizuru		

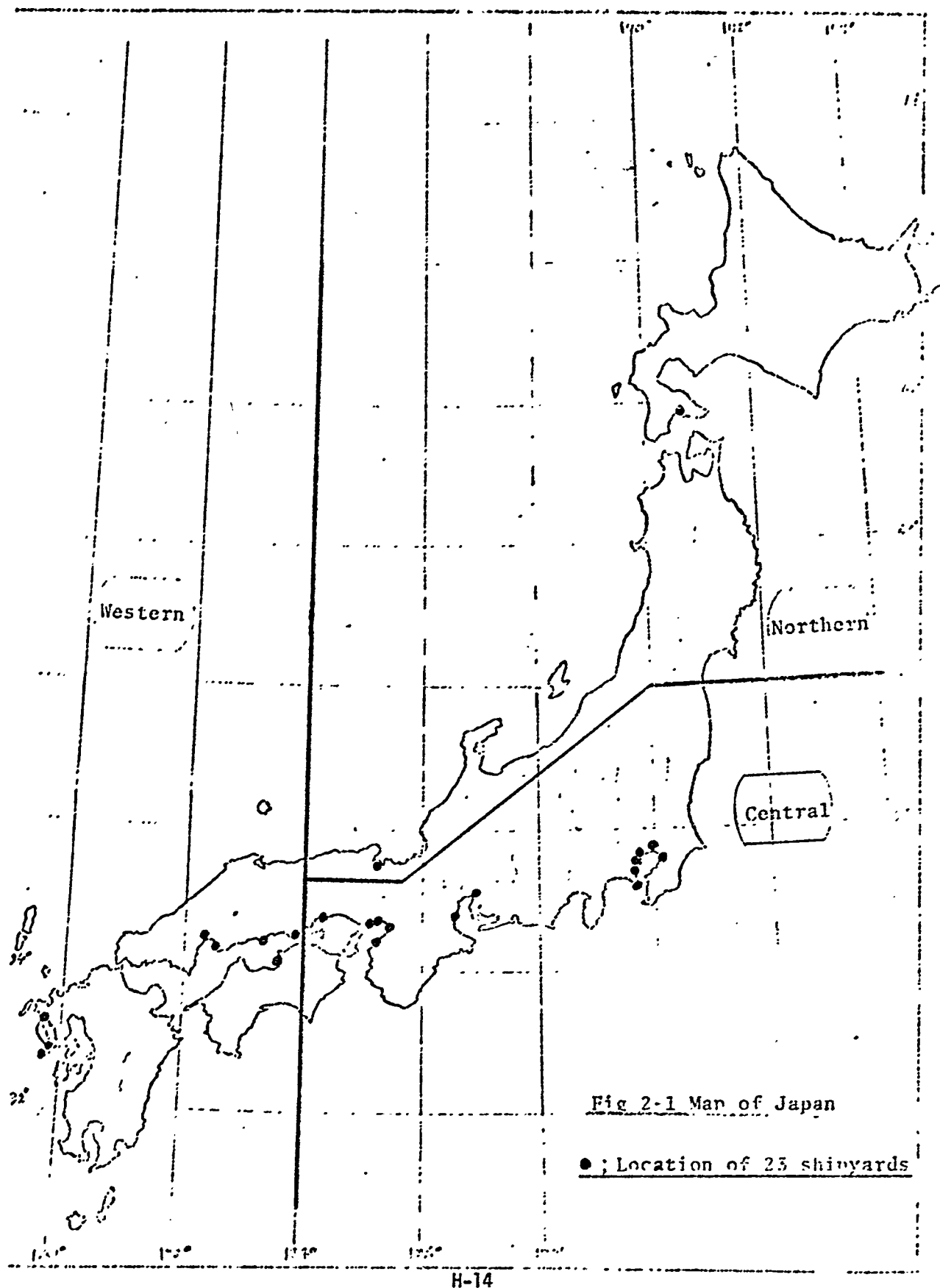
Note (1) Major 23 shipyards are listed first by the name of company and then of shipyard, i.e. IHI-Tokyo means Ishikawajima-Harima Heavy Industries, Tokyo Shipyards.

(2) Abbreviation of the names of companies,
MHI: Mitsubishi-Heavy-Industries
NKK: Nippon Kokan Company

Table 2-2. Shipyard to be studied in Depth.

region	name	shipbuilding capacity
northern	shipyard V	43.700 G.T.
central	shipyard W	106.000 G.T.
Western	shipyard X	170.000 G.T.
	shipyard Y	250.000 G.T.
Large-scale construction shop	workshop Z	_____

A rough distribution of shipyards under study is shown in the figure 1.



3.1. Two Patterns in Climate

Japan consists of islands, facing eastwards to the Pacific Ocean and westwards to the Sea of Japan. Japan also has a latitudinal span of 21, from 24°N to 45°N. Hence, there are two different climatic conditions in Japan. The first, which we call "climatic pattern of omote Nippon", forward side of Japan, i.e. Pacific Coast, except northern Tohoku, North eastern region of Honshu, and Hokkaido, has a similar character of weather. It is hot and moist in summer and relatively warm and dry in winter. In June and first half of July we have usually the rainy season due to the monsoon from the Asian Continent. But in winter, we have relatively stable weather. It is fine and rarely rains or snow.

The second pattern that we call "climatic pattern of Ura Nippon", back side of Japan, i.e. regions along Sea of Japan and Hokkaido. The weather in summer is not so different from "Omote Nippon", but in winter there are many snowy days. It is cold and dark from November to March. From December through February the temperature is below freezing point in Hokkaido. In this region, "the rainy season in June and July" is not so distinct. We explain these differences in details constructing with the number of the days of rain and snow and temperature and precipitation at four cities.

3.2. Temperature

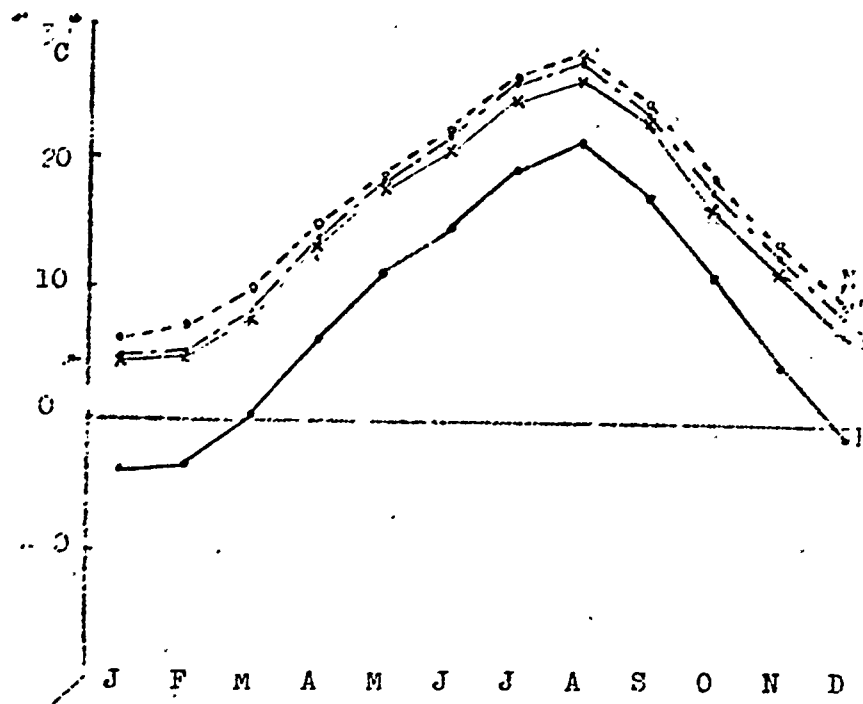
In temperature significant difference can be observed between Hakodate (Hokkaido) and other three cities in Honshu. In Hakodate average temperature through year is under 10°C and during winter, monthly average are below freezing point.

month	Hakodate	Yokohama	Kobe	Nagasaki
1	-3.9	4.4	4.5	6.2
2	-3.5	4.8	4.8	7.1
12	-1.1	7.0	7.4	8.9
average	-2.1	6.0	6.2	8.1
7	19.3	24.6	25.8	26.4
8	21.5	26.1	27.3	27.6
9	17.2	22.6	23.6	24.3
average	17.5	24.4	25.6	26.1

(Observation data: 1941-70)

Fig 3-1

temperature (average, 1941-1970)



H: Hakodate
Y: Yokohama
K: Kobe
N: Nagasaki

3.3 Precipitation and Wind

Monthly change in precipitations at four cities are shown in Fig 2. The peak due to the monsoon is in June except in Hakodate. The second peak in September are usually due to the typhoons. The largest precipitation is observed at Nagasaki. (cf. Table 1)

Table 3-1 Precipitations

	average precipitation per month		precipitation per per year	
	millimeters	(inches)	millimeters	(inches)
Hakodate	95.3	(3.75)	1143	(45.0)
Yokohama	136.0	(5.35)	1632	(64.3)
Kobe	113.9	(4.48)	1367	(53.8)
Nagasaki	164.7	(6.48)	1976	(77.8)

Table 3-2 Days of Rain and Snow

Month Place	J	F	M	A	M	J	J	A	S	O	N	D
Hakodate	11 (9)	11 (10)	9 (7)	3	4	4	4	3	4	6	6	11
Yokohama	3 (1)	4 (1)	4	5	4	6	3	3	4	6	4	2
Kobe	3 (1)	4 (2)	4	3	4	6	4	2	5	5	3	3
Nagasaki	5 (3)	5 (1)	5 (1)	4	5	7	5	2	4	3	2	5 (1)

(Observation Data: 1945-52)

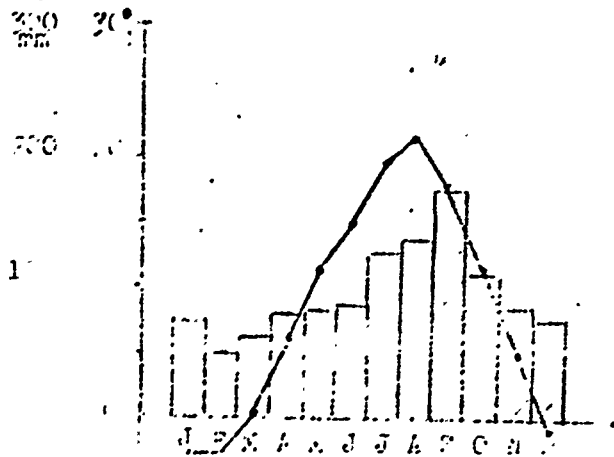
Note: Figures in brackets show the days of snowfall.

Fig. 3-2

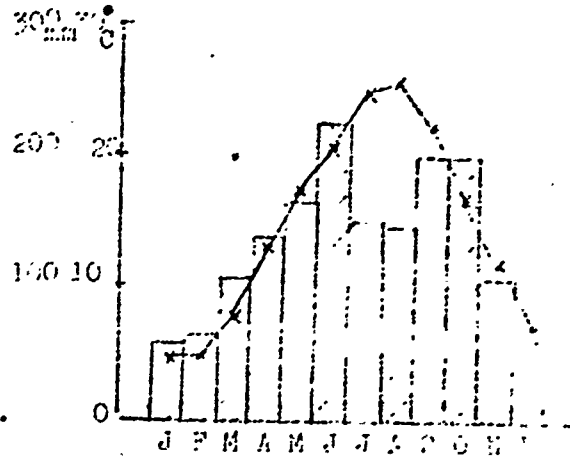
Precipitation and Temperature

▨ precipitation
— temperature

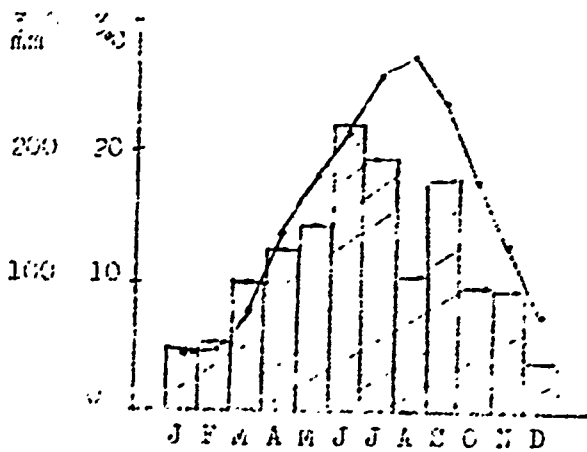
Hakodate



Yokohama



Kobe



Nagasaki

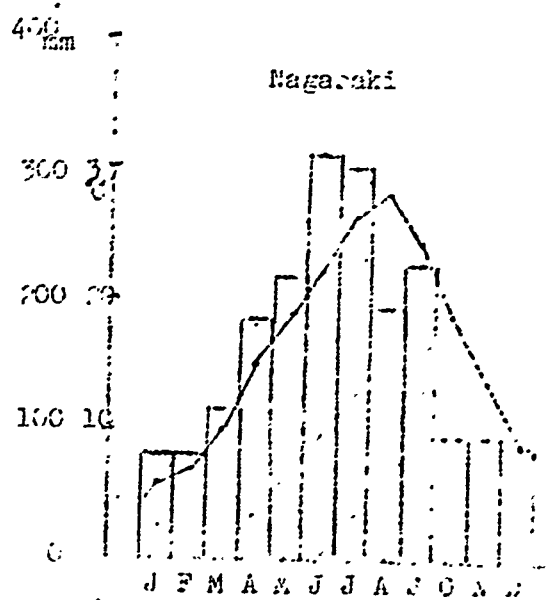


Table 3-3

The amount of snowfall (Depth of snowfall of each month is designated by number of days in each category)

month region	Categories of depth of snow (inch)	11	12	1	2	3	4	total
Western	under 3.94	0	0	2	1	0	0	4
	over 3.94	0	0	0	0	0	0	0
	over 7.87	0	0	0	0	0	0	0
	over 19.69	0	0	0	0	0	0	0
Central	under 3.94	0	0	1	3	1	0	5
	over 3.94	0	0	0	1	0	0	1
	over 7.87	0	0	0	1	0	0	1
	over 19.69	0	0	0	0	0	0	0
Northern	under 3.94	6	14	7	5	10	2	45
	over 3.94	1	9	24	22	11	0	67
	over 7.87	0	4	14	16	7	0	41
	over 19.69	0	0	0	0	1	0	1

(Values above are averages between 1941 and 1960)

Table 3-4

Temperature (in centigrade) (during the work hours)

month region	1	2	3	4	5	6	7	8	9	10	11	12
Western	6.2	7.1	10.2	14.7	18.5	21.9	26.4	27.6	24.3	18.6	13.8	8.9
Central	4.4	4.8	7.5	12.7	17.1	20.5	24.6	26.1	22.6	16.5	11.5	7.0
Northern	-3.9	-3.5	0	6.1	11.0	14.8	10.3	21.5	17.2	11.3	4.6	-1.1

(Above values are averages between 1941 and 1970.)

Table 3-5
Wind Velocity (during the work hours)

month region		1	2	3	4	5	6	7	8	9	10	11	12
West- ern	22.4												
	-33.6	8	7	9	7	6	7	7	3	4	3	3	5
	33.6	1	1	2	2	1	2	2	1	1	1	0	1
Cent- ral	22.4	15	15	16	16	14	9	8	7	8	12	11	12
	-33.6												
	33.6	3	4	4	4	2	1	1	1	2	2	2	3
North ern	22.4	15	14	16	16	14	7	4	3	7	10	11	13
	-33.6												
	33.6	3	3	2	2	2	0	1	0	1	1	1	2

(Above values are averages between 1949 and 1960)

Table 3-6
The number of days of high discomfort index (during
the work hours)

month region	June			July			August			September		
Discomfort index	75	80	85	75	80	85	75	80	85	75	80	85
Western	9.0	0	0	30.0	14.4	0.4	30.8	18.2	1.2	19.4	4.8	0
Central	8.4	1.2	0	24.4	8.4	0	27.2	17.2	0	13.8	4.4	0.2
Northern	0	0	0	1.6	0	0	6.0	0	0	0.4	0	0

(Above values are averages between 1956 and 1960)

note:

$$\text{discomfort index} = 0.72 \times (\text{temperatures} + \text{wet-bulb temperatures}) + 40.6$$

We feel rather discomfort when the index shows over 70 and very discomfort when it shows over 80.

Table 3-7

The number of days with outdoor temperatures below zero at the shipyard V.

The time of measurement: 9.00A.M., 12.00A.M., 3.00P.M.
Measurement was made at above three time points and the average was taken of the three values.

month	The number of days with temperatures below zero					total
	28.4°F	24.8°F	21.2°F	17.6°F	14°F	
Nov. 1969	3	0	1	0	0	4
Dec. 1969	9	5	3	0	0	17
Jan. 1970	8	3	2	2	1	16
Feb. 1970	10	6	3	1	0	20
Mar. 1970	4	7	1	1	0	14
Nov. 1970	2	0	0	1	0	3
Dec. 1970	5	2	1	0	0	8
Jan. 1971	5	5	3	1	0	14
Feb. 1971	7	2	3	0	2	14
Mar. 1971	5	0	0	0	0	5
Nov. 1971	1	0	0	0	0	1
Dec. 1971	3	2	0	0	0	5
Jan. 1972	10	4	2	0	0	16
Feb. 1972	7	2	1	1	0	11
Mar. 1972	4	1	0	0	0	5

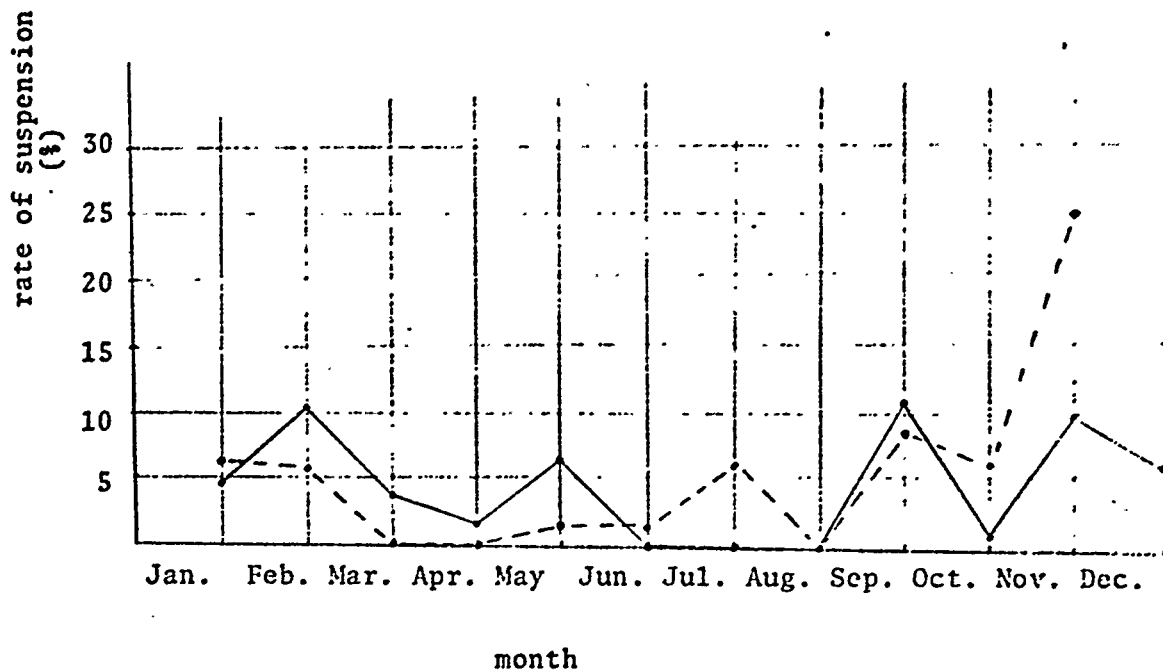
Table 3- 8

The record of wind velocity in recent times at the shipyard V

month	the number of days of operation	the number of days crane operations were stopped	the number of days warning index issued against crane operation	remarks
Jan. 1971	22	1.0	3.0	Warning is issued against crane operation when wind velocity reaches 33.6 to 40.3 miles per hour. Crane operation is stopped when wind velocity is more than 40.3 miles per hour.
Feb. 1971	23	2.5	1.0	
Mar. 1971	27	1.0	3.0	
Apr. 1971	23	0.5	5.0	
May 1971	21	1.5	3.0	
Jun. 1971	26	0	0	
July 1971	26	0	0.5	
Aug. 1971	25	0	2.5	
Sep. 1971	22	2.5	4.0	
Oct. 1971	26	0.5	4.5	
Nov. 1971	25	2.5	4.5	
Dec. 1971	25	1.5	2.5	
Jan. 1972	23	1.5	4.0	
Feb. 1972	25	1.5	3.5	
Mar. 1972	25	0	1.5	
Apr. 1972	21	0	2.5	
May 1972	22	0.5	2.5	
Jun. 1972	25	0.5	4.0	
Jul. 1972	25	1.5	2.0	
Aug. 1972	26	0	2.0	
Sep. 1972	24	2.0	2.0	
Oct. 1972	24	1.5	4.5	
Nov. 1972	24	6.0	2.0	
Dec. 1972	-	-	-	

Fig. 3-3.

The monthly rate of suspension of crane operation



note: 1) The solid line designates the curve for 1971, while the dotted line designates the curve for 1972.

note: 2) The average rate for 1971.....5.7%
The average rate for 1972.....4.6%

note: 3) Monthly rate of suspension of crane operation is defined here as the ratio of number of days when crane operations were stopped to the number of days of operation (cf. Table 3-8 in the previous page),

4. Actual Condition. of Protection Facilities in Japan

There are four type of weather protection facilities, adopted for outdoorworks in shipyards and heavy construction industries, i.e. (1) roofs, (2) other facilities in workshops, (3) special devices for cranes and (4) those for wharfs.

4.1. Roofs

Covering with roofs is one method to provide protection from wind, rain, snow and heat. There are four types of roofing and their specifications are described roughly in the Table 4-1.

Table 4-1. Type of Roofing

Type	Specification
Permanent building, fully closed	Steel frame roof covered with galvanized iron sheet
	Steel frame roof covered with long precoated iron sheet
Permanent building with traveling roof	Steel frame roof covered with galvanized iron sheet or long precoated iron sheet
	Steel frame roof covered with slate
Permanent building with roof, not fully closed	Steel frame roof covered with galvanized iron sheet
Simple traveling roof	Light gage steel frame roof covered with galvanized iron sheet
	Lightweight steel tube roof covered with eslon sheet

Table 4-2.

Covered rate of assembling yard in major shipyards in Japan mainly as of 1970.

Region	Shipyard	Covered rate(%)			Remarks
		total	type 1	type2	
North-ern	V	56	42	14	
	A	51	51	0	type 1 100%, as of April 1972
	B	52	17	35	
	W	47	29	18	{ type 1, 37% type 2, 33% total 70%, as of April '72
	C	84	76	8	
	D	100	100	0	
	E	59	42	17	
Central Japan	F	34	0	34	
	G	56	25	31	{ type 1, 49% type 2, 21% total 70%, as of April '72
	H	68	36	32	
	I	96	96	0	
	J	34	34	0	
	K	27	16	11	
	L	49	7	42	
	M	61	61	0	
Western Japan	N	62	0	62	
	O	90	90	0	
	P	60	49	11	
	Q	100	100	0	
	R	87	87	0	
	S	72	61	11	
	T	55	20	35	
	X	67	64	3	
	Y	100	100	0	as of April '72

Note:
(1)

covered rate (%) of assembling yard

$$= \frac{\text{Square meter of indoorized assembling surface}}{\text{Total square meter of assembling surface}} \times 100$$

(2) Type 1: covered by fixed roof, type 2: covered by travelling roof.

Among four production stages in new construction work, Steel Fabrication stages are wholly indoorized. The vital parts of Block Assembly stage are covered by roofs in the most shipyards. The covered rate of workshop is outlined below.

Block Assembly Shop: Covered ratios by roofs range from 51 to 100% in shipyards.

Pre-Erection Shop, Dock and Bulking Berth: Almost all shipyards have no protection facilities, except for several new shipyards provided with roofs of a covered ratio of about 10%. This may also apply to constructional steel works. Painting and Coating Shop: Traveling and fixed roofs are used in roofed shipyards and constructional steel works, with covered ratios ranging from 60 to 100%.

The data of the roofs actually installed at four shipyards surveyed in depth, are shown in the Table 1-5 in the Appendix 1 and their photograph as No. 1-12 in the Appendix 2.

The fiscal 1970 survey on covered ratios in block assembly shops Of Japan's principal shipyards (Table 4-2 on previous page.) gives the following covered ratios: (1) 27 - 87% for shipyards built prior to 1960; (2) 51 - 99% for those built from 1961 to 1970 ; and (3) 100% for those built from 1971 up to now. According to the survey made this time in 1972, covered ratios of block assembly shops in shipyards in (2) have increased to 70 - 100%. This means that introduction of flow production systems like coveyor lines to promote automation and labor saving in block assembling has necessitated roofing. Particularly, all of newly constructed, sophisticated shipyards In the central and western parts are fully roofed regardless of their siting and weather conditions.

4.2. Other Protection Tools

4.2.1. Needs for personal protection tools

Conditions for which needs for personal protection arise in winter and summer are as follows:

Winter: In the northern part, leather windbreakers and trousers are supplied to all outdoor welders for protection from cold while in the central and western parts outfits for protection from cold are lent to several thousand outdoor workers. Each workshop has heating devices installed as required to allow workers to warm themselves. However, no measures for protection from cold are taken in workshop which are not covered completely.

Summer: Since the maximum temperature in the year (monthly average) is 70.7°F, most comfortable to the human body, in the northern part, no protection from heat is provided there. In the central and western parts indirect methods such as fans and coolers and direct methods like cool suits are taken.

4.2.2. Specifications of protection tool for personal use.

There are five main items in protection tool, i.e. ventilating fan, cooler/heater, water cooler, clothing and material to make shadow.

Applications of such protection tools and equipment are listed below.

Table 4-3 Protection Tools and Equipment

Item	Location	Specification
Ventilating fan	Block assembly shop Pre-erection shop Building berth and dock Painting and coating shop	Commercially available motoroperated ventilating fans 5 - 30 KW
Cooler and eater	do.	Inboard cooler with the same performance as commercially available type 33 KW
		Gas and kerosine stoves are used as heaters
		Coke stove are used as heater
Water cooler	do.	Commercially available types are used
Outfit for protection against cold	Outdoor block assembly shop, building berth and dock in welding	Coat and vest for protection against cold
		Leather windbreaker and trousers and pocket warmer

-cont'd-

-cont'd-

Net for protection against heat	Building berth and dock Pre-erection shop	Made of nylon and sized 269 to 1076 sq. ft.
Cool suit	Pre-erection shop Building berth end dock	Compressed air is fed into bag in vest to cool

4.2.3. Use of protection tools among shipyards

We surveyed the state of the arts of the use of protection tools for personal use among 25 major shipyards in Japan, using the data made by Nihon Zosen Kogyokai (Ship-builders Association of Japan). The data were revised by us through direct interview or questionning to get up-to date picture in Jan. 1972. Percentages in the following Tables denote the share of the number of shipyards in which particular tools adopted to the total number of shipyard surveyed, otherwise mentioned.

Diffusion of use of Protection devices for variation of temperature in the major Shipyards, in Japan as of January 1972 is as follows.

A. Heating

Table 4-4. Adopted Types by shipyard (25 shipyards)

Shops Types	Steel Fabrication	Assembly	Dock and Build- ing Berth
Steam heating	0	0	0
Warm air blower	0	0	0
Gas Stoves	8	5	3
Electric heater	1	0	0
Coal stoves	0	6	1
Oil heater etc	15	10	11
nothing	1	4	10

Table 4-5. Wearings

	percentage of adoption among 24 shipyards
Winter cloths	83%
Portable body warmer	42%
Winter waistcoat	12%
Anorak	4%
Muffler	4%
Ear-cover	4%

Table 4-6. Standard and system of Supply

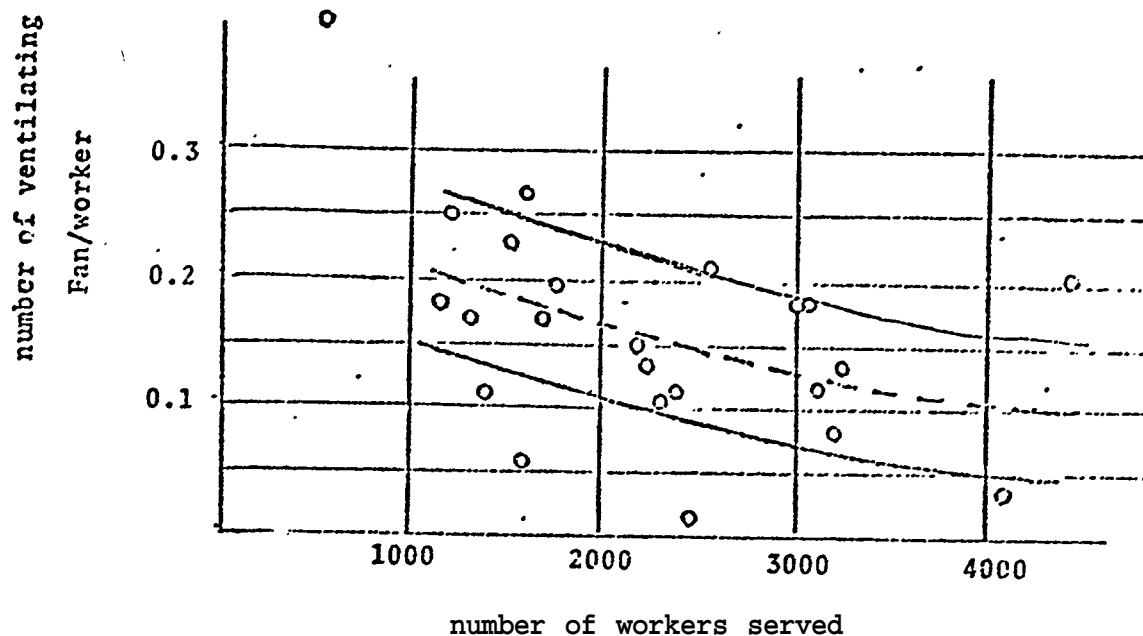
For those who work outdoor wholeday	37%
For workers at building berth and dock during over-time work at night	25%
For outdoor crane operators at night	4%
For all outdoor workers	46%
Lending system	71%
Supply as personal effects	17%

B Cooling (for 23 shipyards)

Ventilation Fan

Ventilation Fans are used widely among shipyards, of which two standard types are shown as photographs 13 and 14 in the Appendix 2. The correlation of number of ventilating fans installed and the number of workers served are shown in Figure 4-1.

Figure 4-1. Number of ventilation Fan installed

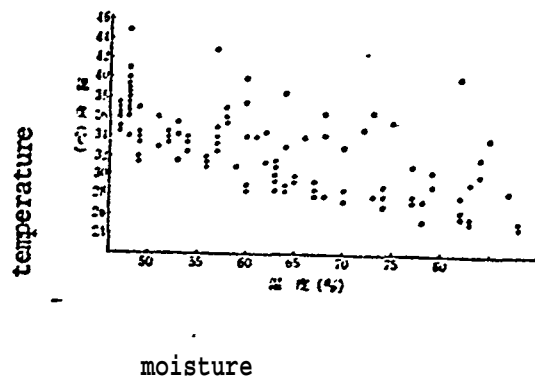


Spot Cooler Unit

In some shipyard, Spot Cooler Unit, which is shown as photograph 16 in the Appendix 2, are used to blow cool air through ducts into the shop or into the tank block of ships on the dock. The complete enclosure of ways do arise other kinds of extreme environments. These are high temperature, moisture, noise and dust. For example, in welding and fitting works in large hull blocks on the docks in summer, people sometimes have to work in as high temperature as 104°F and in high moisture

over 80 percent. These hot and moist environment are caused by the radiation heats both from the equipments themselves people using, i.e. gas cutters, welding tools etc., and steel sheets hot up by direct sunshine. We show an example of high temperature and moisture observed in the hull construction works in Japan.

Figure 4-2. Temperature and moisture in the holds and tanks on the dock.



source: Shipbuilding Association of Japan
Working Environment Committee.

These temperatures and moistures are usually extremely high in the holds and tanks directly under the deckplates and inside of side shells in summer. To protect welders and strain removers who are working under such an extreme conditions, Spot Cooler Unit are available in several shipyards. (cf. Figure 4-3). The effects of this device at the shipyard W in the Central Japan and the shipyard X in the Western Japan in the summer 1972 are shown in the Table 4-5. Temperature decrease was 37.4°F in average, moisture decrease 3-5% and discomfort index was lowered to 80.

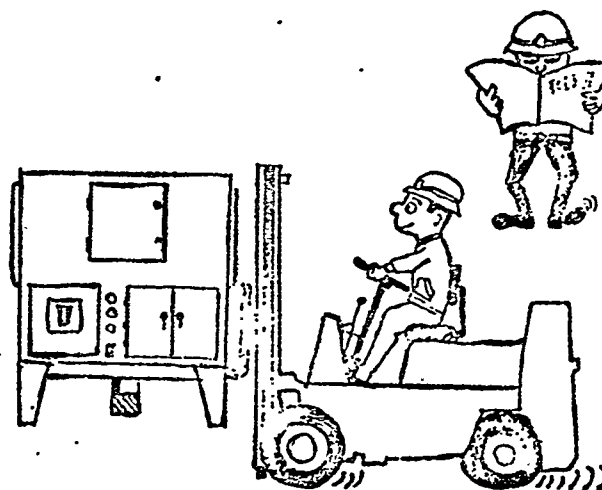
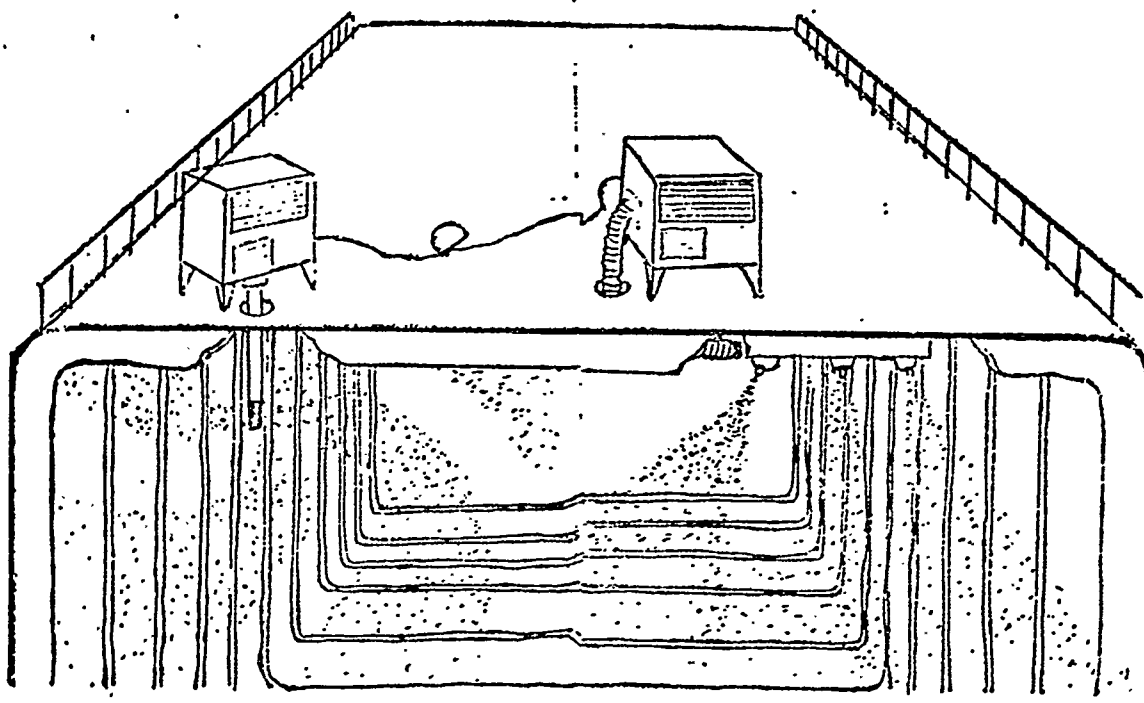
Table 4-7. The effects of Spot Cooler Unit in the Tanks and Holds.

Observed: middle of June—middle of September 1972.
(Shipyard W in Central Japan)

middle of June—middle of October, 1972.
(Shipyard X in Western Japan)

item region	temperature °F				humidity %				discomfort index			
	air on the deck	(1)no air cooler	(2)air cooler	(1)-(2)	air on the deck	(3)no air cooler	(4) air cooler	(3)-(4)	air on the deck	(5)no air cooler	(6)air cooler	(5)-(6)
Central	93.2	95.0	89.6	5.4	47	47	44	3	84	85	80	5
Western	89.6	100.4	91.4	9.0	66	47	42	5	82.5	88	81.5	6.5

Figure 4-3. Spot Cooler Unit on the deck plate



Other devices

In all 23 shipyards surveyed, sunnet are used to make shadow to protect workers under direct sunshine on the outdoor working shops (cf. photograph 26 in the Appendix 2.)

In some shipyards dry ice is supplied to the outdoor workers to prevent the heat, especially to cool their heads.

They put the packed dry ice in the bag of felt and set it in the helmet. They change it. twice a day, that is, in the morning and in the afternoon. However the use of dry ice has been suspended recently in many shipyards.

The cool suits is shown as photograph 19 in the Appendix 2.

Table 4-8. Other devices

	Percentage of adoption among 23 shipyards surveyed
Sunnet	100%
Supplying dry-ice for personal use	31%
Vortextube and cool-suits	52%

4.3. Cranes

To prevent cranes from speeding and overturning due to wind force, all outdoor cranes are equipped with clamping devices regardless of their size. (Installation of this device is required by regulations of the Japanese Government.) There are four types of crane protection method, of which photographs attached in the Appendix 2, as follows.

- Type 1. Rail clamping (photos. No. 20)
- Type 2. Hooking (photos. No. 21.22.)
- Type 3. Pin drop (photos. No. 23.24.)
- Type 4. Guy wire (photos. No.25)

Though different depending on type of crane, these devices may be roughly divided as listed below.

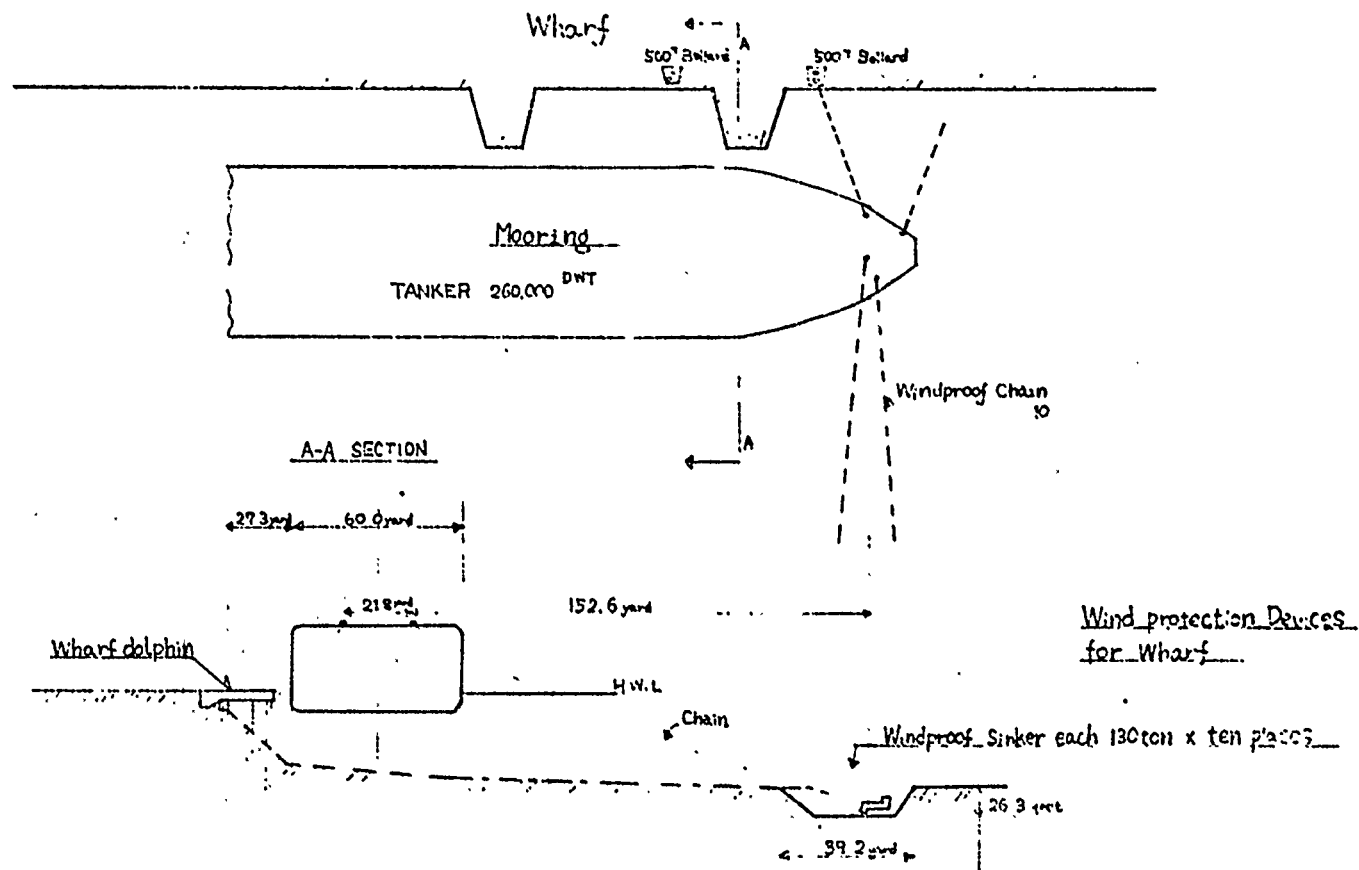
Table 4-9 Crane protection methods

Description	Specification
Rail clamping System	Crane rail is clamped with steel clamp near crane saddle
Hooking system	Steel hook provided on underside of crane saddle is fitted into eye provided outside or inside of crane rail to clamp crane
Pin (Drop-in) system	Steel bar or strip pin equipped on outside of crane saddle is put in hole provided in foundation outside of crane rail to fix crane
Guy wire system	Steel wire a steel turnbuckle is used to fix crane to foundation from outside of crane saddle

4.4 Wharf

Almost all shipyards have no particular provisions against strong wind, except for some newly built shipyards in which windproof sinkers are equipped, provided there are ample open sea in front of wharf. An example of the windproof sinker at Shipyard Y is shown as Figure 4-1. Ten chains fixed at the bottom of open sea can hold a mooring ship with other ten chains on wharf side in the case of strong winds.

Figure 4-4. Windproof sinker at Shipyard Y.



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5. Relationship of Weather Variation to Productivity in Japan

5.1 Background of the survey

We defined, here, productivity as man-hour efficiency, i.e., man-hours consumed per unit volume of construction. This productivity measure is generally used, as basic index for daily and monthly production control in Japanese shipyards. The productivity is influenced by equipment, personnel composition, management organization and construction method; of which latter two factors are based on the former two. Weather conditions have also influences on the productivity as a whole. This makes it difficult to single out precise relationship of weather variation to productivity change.

We have tried to find statistical correlations between man-hours consumed in particular workshops and weather variations during certain time span. Here, productivity measured mainly by man-hours, is a function of weather variations, method of production and management and two factors for production, i.e. equipments and labour. However, man-hours consumed per unit volume constructed differ ship by ship due to their type and size. If we took the man-hour data on the same type and size of ships in longer periods, say four and five years, the production methods were improved gradually during these years. Thus we could not find any precise correlation statistically between weather variation and man-hours consumed.

When we have carried out surveys in depth at four shipyards selected, we have asked for over fifty supervisory personnel at various managerial levels who have long experiences in production work, on their opinions on the effect of weather variations on productivity. Replying to this question, some one relies on man-hours data and others on different data they are using according to their types of workshop. We asked for them to express their empirical observations on the effect of weather variations in terms of percentages.

5. 2 Degree of Effect of Weather Change

The degree of effects of weather change on productivity, based on the empirical observation thus collected, is shown in Table S-1 . In this table, the monthly degree of effects on productivity are shown as percentages of monthly production in each region compared with the best production efficiency observed from the past experience. This best efficiency is for the production activity of shipyard as a whole, not for the outside work only. Although the effects of weather variation are naturally the largest on outside works, the production efficiency in roofed Block Assembly Shop has to be reduced, if there occur slow down due to weather variation in succeeding working stage, i. e. Pre-Erection

The most shipyards in Japan are usually located at relatively narrow site along old ports, for example Nagasaki port is older than United States itself, i.e. it had been receiving foreign traders since 17th century. When Commodore Perry asked for Tokugawa Shogunate Government to open several Japanese ports for U. S. merchant marines 120 years ago, Yokohama, Kobe and Hakodate were in his list of ports to open doors to him. In old shipyards located at such historically old ports, there are scarcely ample spaces between workshops for storing stock and members to adjust the difference of production efficiencies if any, among workshops. The slow down of production at

Pre-Erection and Dock/Building Berth inevitably affects the production pace of Block Assembly Shop. The effect of weather variation should not be considered separately for outside work only. Thus the figures shown in the Table 4-9 denote the effects of weather change observed as a whole for each shipyard, based on the experiences and opinions of fifty managers and supervisor interviewed.

At the shipyard in northern region, monthly productivities are reduced to 85% to those in best conditions during winter, from November to March. These reduction are mainly caused by low temperatures and snows. The work does not stop in the cold days below 0°C, however it is impossible to estimate the reduction of efficiency due to cold temperature. Further, snow removal on uncovered surface needs another costs. Based on the data of the past few years, the costs of snow removing works are as follows.

For total surface	\$ 362/100yd ²
of which for- assembly	\$ 162/100yd ²
of which for- welding work	\$ 200/100yd ²

Table 5-1

Degree of Effect of Weather Change on Productivity by Region
in Percent

Month														annual
Region	1	2	3	4	5	6	7	8	9	10	11	12		average
Northern	85	85	85	90	90	95	100	100	95	90	85	85		90
Central	95	95	95	100	100	100	85	85	85	100	100	95		95
Western	95-97	95-97	100	100	100	90	85	85	85	100	100	95-97		95

Note : 100% denotes the best conditions in each region

Table 5-2:

Seasonal Division by region

Month	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.
Region												
Northern	Winter →					← Summer				← Winter		
Central	Winter →					← Summer				Winter		
Western	Winter →					← Summer				Winter		

In the Shipyard W in Central region, the effect of weather variation, are usually the largest in summer, especially due to the high temperature and moisture (of. Table 3-5) and partly due to rain. Monthly productivities during summer arc reduced to 85% to the best efficiencies.

In the shipyard X in Western region weather conditions and its effects on productivity arc almost the same as the Central region, except precipitations during summer months.

The effect of weather variations to the best production efficiencies, considered in annual average percentage, are 10% at shipyard in Northern region and 5% at shipyard W and X in the Central and Western regions.

5-3 The Secondary Cost Effect

There is no direct correlation between accidents rate and extreme environment in Japanese shipyards. Here accident rate is defined as the frequency of accident, for which worker has to absent himself from work, to one million working hours. The frequency observed at shipyard W and X in Central and Western regions in shown as Table 5-3 . Accident rates are rather high in a fine and comfortable day like spring afternoon. People usually seem to be more cautious to protect themselves in the extreme working conditions.

Table 5-3 Accident frequency at Shipyard W and X
1972.

Month	J	F	M	A	M	J	J	A	S	O	N	D
Accident Frequency	6.35	5.01	10.87 5.20	2.35	0	0	0	0	0	0	0	2.80
Rainy days	3	4	4	5	4	6	3	3	4	6	4	2

Note; Accident Frequency = $\frac{\text{Accident}}{\text{Total working hours}} \times 10^6$

6. Improvement in Productivity after Adoption of Protection Facilities.

6.1. Roofs .

As described above, block assembly shops are only workshops that allow measurement of effect through the adoption of roofs. The results of survey on block assembly shops are given in the Appendix I-Collection of Data, "The results of surveys on roof installment, Table-1-4," and in Table-5, "Effects through Indoorization in major shipyards as of 1970".

Roofing a block assembly shop promises an effect of about **20 to 30%** thanks to: (1) Ability **to** continue work despite rain; (2) shortening of time required for arranging assembly blocks due to improved facilities; and (3) improvement in working environment due to uniformly maintained temperature.

Effect of covering is great in the northern part in winter because it can prevent reduction in efficiency arising from stopping of cranes due to strong winds, snow removing work due to low temperatures.

Covering of pre-erection shops and building docks and berths have been rarely practiced in Japan despite its great effect expected, except newly built giant shipyard like shipyard Y in western region. However, we can not obtain any stable data there at present, because the operation has just begun there in 1972.

6.2. Protection Tools and Facilities

As a direct method protection tools are supplied to cope with bad working environment. According to the results of the questionnaire, this, coupled with improvement in moral of workers, has an effect of about 5% for equipment standards in Table 6 to 9 in Collection of Data. The estimation of 58 increase in efficiency is based upon

the opinions of experts questioned, for it is further difficult to single out the effect of the adoption of particular protection tool, say cool suits or portable body warmer on the productivity. These tools, it seems, have a more direct effect upon the motivation to work as whole.

6.3. Crane Clamping Devices

A Japanese crane construction standard provides that devices to prevent a crane from speeding and overturning be installed to the crane. It is impossible to calculate the effect on protection units.

6.4 Additional Works Arising from Unfavorable Working Environment and Resultant Reduction in Efficiency

Additional works required in Japan are the following direct and indirect types:

- (1) Wind : e.g., crane clamping
- (2) Rain : e.g., rain protection (temporary awning installation), drying, draining
- (3) Snow : e.g., snow removing
- (4) Heat : e.g., net and cooler installation
- (5) Cold : e.g., heating

Among these works, heating is measurable. This heating work attendant on welding involves the heating of portions of high tension steel plate and sheet to be welded with a gas burner, etc. to compensate poor welding conditions at low temperature. According to Table "Results of Survey on Additional Works" in Collection of Data compiling the results of the survey, these heating works reduce efficiency by about 20 % with ordinary welding speed taken as 100 %. The term "heating work" used here does not mean removal of moisture or nor drying a portion to be welded but raising low steel plate temperature to that optimum for welding, that is 300°-400°F.

Water removal cost in the case of heavy rain can not be estimated separately.

Table 6-1.. Additional Work for welding in low temperature

	Heating Method	Investment	Decrease of productivity measured by man-hours (%)
Shipyards X	In welding works on docks and building berths, worker heat welding points at first through gas-burner heater & then weld immediately.	\$ 380 / 5 heaters	20% reduction compared to normal welding work
Workshop Z	Gas-burner method	\$ 38 / heater	20%
Shipyards V	During winter (from November to March) no welding-work in the night (6.00p.m.-8.00p.m.). In the winter day time, stop welding works, if temperature is getting low under 23°F Using gas-burner heater	n.a.	approximately 20%

7. Examples of Productivity Increase through Adoption of Roofs.

7.1 On the Job Compositions in the Workshop affected by Weather Protection Devices

The organization of production in the Japanese shipyards has been changed drastically, in recent years, due to the adoption of flow production system. In previous days, workers were allocated and organized by their trades to each workshop. However it became difficult to control workers on production flow and keep good efficiency by such a production organization based on trades. Today, in the most large shipyard in Japan, the production arc reorganized on the stage unit through construction processes and workers who belong to different trades arc mixed up in to a working unit. In the case of Shipyard W in Central region, the composition of trades (jobs) in each production stage is shown in Table 7-1.

Table 7-1 The Composition of Jobs
at Shipyard W.
(1)

stage Trades	Fabrication	Block Assembly	pre- Erection (4)	Erection (on Dock and Building Berth)
Marking	X	x	x	
Fabrication (2)	X	x	x	x
Crane Operation and Rigging	X	X	X	X
Welding	X	X	X	X
Assembling(3)	X	X	X	X
Bending and Caulking				X
Fitting (3)				X
Scaffolding				X
Launching and Testing				X

- notes:
- (1) X denotes major trades in each stage and x denotes minor trades in it.
 - (2) Fabrication includes gas-cutting, bending and scale removing.
 - (3) including gas cutting, scale removing.
 - (4) Pre-Erection. In this stage, which is between Block Assembly and Erection in some shipyard, a larger Block is assembled by uniting two or more small blocks into one. The aim of Pre-Erection stage is to complement the limit of indoorized Block Assembly workshop where larger Blocks can not be assembled due to relatively narrow working surface.

In the Shipyard X there are three major section in the Hull Construction Department, i. e. Hull Fabrication, Block Assembly and Erection (including Pre-Erection stage), and three in the Outfitting Department (Table 7-2). Necessary jobs for Hull Construction Dept. are fifteen, of which welding and maintenance jobs appears in every section, hull assembly, crane operation and rigging, pneumatic service and power jobs appears in two sections. Further the workers who belong to the same job do not make one group in the Section but scattered among working groups. Hull Fabrication Section consists of about 450 workers, which are divided into three Sub-Section (Kakari). One Sub-Section, then, consists of ten Group (Han). Each Group, the smallest working unit, has a forman and fifteen **to** twenty workers. These working unit themselves, consist of several crafts, i. e. welders, gas cutters, platers, riggers and pneumatic serviceman etc.

Such a mixed composition of multiple jobs in the working organization, will be one of the remarkable characteristics of Japanese shipyard. All necessary informations to control production processes are based on these mixed working organizations and not on jobs.

Table 7-2 Composition of major job by working section at Shipyard X as of 1972

Job	Department Section	Hull Construc- -tion			Out fitting		
		1	2	3	4	5	6
Hull Fabrication		x					
Hull Assembly		x	x				
Plater				x			
Welding		x	x	x		x	
Crane Operating & Rigging			x	x	x		
Pneumatic Service			x	x			
Power		x		x			
Maintenance		x	x	x	x	x	
Slipway Service				x			
Inner Fitting					x		
Interior Fitting for Living- -Quarter						x	
Outer Fitting							x
Painting							x

Note: Section 1: Hull Fabrication

- " 2: Block Assembly
- " 3: Erection
- " 4: Inner Fitting
- " 5: Super Structure
- " 6: Hold

Further, there is a trend to multiple workmanship in the smallest working unit.

Every worker has been trained in and has, at least, one qualified skill necessary for shipbuilding works. However, in recent years, there is a remarkable trend to have multiple skills or qualifications among worker. For example, welders in Hull Construction Department usually have other related skill, i. e. qualification as plater. Platers, in turn, can have gas cutters skill.

7.2 Available Measures on Efficiency for This Study

The measures on efficiency that are used as production management indexes, daily or monthly, in each Department, depend naturally on the type of working organizations.

In the shipyard surveyed, man-hours per ton of constructed ship and/or volume of steels fabricated per month are used as measure on efficiency.

Data that show differences of efficiencies by trades do not exist, because of multi-trades working unit already mentioned.

Any physical measure like welding lengths per man per shift can not be obtained unless one carry out special observation beside the production line. It is impossible for us to do such special observations within limited term and thus we have to relied upon available existing informations on efficiencies.

7.3 Example A.

We have obtained during our survey man-hours statistics at particular workshop, i.e. Block Assembly Shop at Shipyard X. In this shop the surface was uncovered in 1968, where roofs were installed in 1970. We calculated the productivity increase using these man-hours data as a clue.

Table 7-3..Areas covered under roof (1970)

Block Assembly shop	(1) Total Area sq. ft.	(2) Covered sq. ft.	(3) Covered ratio. (2)/(1)x100
A	41,980	26,910	64%
B	11,840	7,104	60%
C	16,146	10,226	63%
Total	69,966	44,240	63%

Table 7-4 Productivity measures recorded, in 1968, in the term of man-hours per square meters of Block Assembly shops listed below.

Block Assembly shop	man-hours consumed on the area (H/Y)	of which --- welding man-hours		number of workers in average (man)
			%	
A	136,800	84,820	62	50
B	86,400	47,520	55	30
C	172,800	96,770	56	70
Total	396,000	229,110	58	150

note: These man-hours were consumed on the uncovered area in 1968 where roofs were installed in 1970. Therefore, 396,000 hours are corresponding to the covered 44,240 ft² in 1970 in Block Assembly Shops A.B.C.

Table 7-5 . . Working hours affected by rains, in 1968,
before the installation of roofs.

	days or hours affected per worker	total loss time (hours)	remarks
1) Fully idle days	22 days	42,420	The days, precipitation is over ^{0.004} _{inch} /H at 08:30 a.m. and all workers are ordered to back home.
2) Interruption of welding works only	86 hours	12,242	The days, precipitation became over ^{0.004} _{inch} /H after beginning of operation.
3) Interruption of all works	88 hours	12,242	The days, precipitation became over ^{0.004} _{inch} /H after beginning of operation.
4) Reduction of efficiencies due to the drizzling rains and interruption listed above in related works	50 hours	9,356	In drizzling rains, that are under ^{0.004} _{inch} /H, all works can be continued. However there occur efficiency reduction in some degree.
Total	—	64,018	—

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In 1970, the uncovered area above mentioned in this Block Assembly Shop was covered by roofs and thus they could eliminate the loss times due **to the** rain that amounted to 64,018 hours in 1968. The loss rate of working hours in 1968 can be obtained by a ratio of total loss times to total man-hours at that year on the particular area in Block Assembly Shop. This was 16% annually, i.e.

$$\text{loss time ratio} = \frac{\text{Total loss times}}{\text{Total man-hours}} \times 100\%$$

$$\frac{64,018}{396,000} \times 100\% = 16.2\%$$

We can read approximately this loss time ratio as productivity increase ratio by the adoption of roofs over **these** particular area of Block Assembly Shop. It is because that when roofs were installed over the area, the production methods there were changed drastically. The most significant change must be taken place in the type of cranes, i.e. from jib type to overhead travelling one and consequently in their handling and lifting capacities. This leads to other changes in supplying and handling procedures of sheets and pieces on the production lines, in distribution and location of tools, e.g. those for cutting and welding and total number of workers on the area. Therefore even if we obtain the productivity figures for 1970 at the same workshop, we should not compare this figure with those of 1968 to estimate the effects due to the installation of roofs. The above estimated gains of 16.2% can be considered as the most conservatively calculated figure based on the conditions that there is no change except roofs in the production methods.

7- 4. Example B.

As we already described in Section 2.3, the "indoorization" process had begun in some Japanese Shipyard as early as on later half of 1950's. At that time, the engineers in Shipyard iv estimated the productivity gains if they installed roofs over Block Assembly Shop. The basis of estimation and the result are as follows. The estimation had been made on the data of seven months from April to October 1957. The estimation was based on the production volume per hours and production reduction due to rain was calculated 23.6% ($W_r/W_f \times 100$).

In this case the differences of man-hours consumed due to the different size and type of ships were assumed to have no significant effect upon production volume. It was assumed, too, the necessary man-powers were always supplied to the workshop to keep the marginal production capacities.

The introduction of roof over this workshop eliminated the reduction of production due to rain. However we have to add further gains, i.e. reduction of piece stock for rain and changes in crane capacity and production methods.

This old estimation can be used as standard and classical calculation on the effect of rains.

Basis of estimation

(A) Reduction of Prodction due to rain

$$W_r = K \times R$$

$$\text{here } K = \frac{W}{H - (R + E)}$$

W_r = Reduction of Production due to rain

R = Loss time due to rain

W = Production Volume

K = Production Volume per hour in net working hours

H = Total working hours

E = Loss time due to labour dispute

H is defined as

$$H = H_w - H_h + H'h$$

here H_w = Total working days x normal working hour per day

H_h = Total holidays x normal working hour per day

$H'h$ = Total working days in holiday x normal working hour per day

n = Operation ratio in holiday

$$= \frac{m}{H''} \cdot \frac{1}{M}$$

here m = Total workers who work in holiday

M = Average of workers in weekday

H'' = Total working days in holiday

R is defined as

$$R = R_w - R_h + \eta R'h$$

here R_w = Total rainy hours in normal working hours

R_h = Total rainy hours in holiday

$R'h$ = Total rainy hours in working hours in holiday

E is defined as

$$E = E_d + E_i$$

here E_d = Direct loss time due to labour dispute

E_i = Indirect loss time due to labour dispute

(B) Reduction of Production due to labour dispute (W_e)

$$W_e = K \times E$$

(C) Operation capacity of Block Assembly Shop (W_f)

$$W_f = W + W_r + W_e$$

here w_f is defined as normal production volume on Block Assembly Shop if there occur no rainy days and labour disputes

(D) Normal working hours was nine hours per day,
i.e. 8.00am-noon, 1.00pm-6.00pm.

Table 7-6

Effects of rains to Block Assembly Shop

Observed at Shipyard W during 7 months
(April to October) 1957.

Item month	Total working hours (h)	loss time due to rains (h) (R)	loss time due to labor dis- pute (h) (E)	Volume of production		Losses due to rains (t) (Nr)	Losses due to labor dispute (t)	Full capacity/ when Nr=0 Mo=0(t) (W)
				per month (tons) (N)	per hour (t)			
April	243.0	53.5	0	5641	29.7	1590	0	7231
May	248.4	69.0	0	5427	30.2	2080	0	7507
June	235.8	62.2	0	5056	29.1	1805	0	6361
July	239.0	73.9	38.5	3662	28.9	2140	1115.0	6917
August	243.4	21.0	0	6042	27.2	572	0	6614
September	241.6	96.5	0	4074	28.2	2720	0	6794
October	249.9	25.3	14	6118	29.2	740	406.0	6853
Average	243.0	57.3	7.5	5145.7	28.9	1655.0	217.0	7017.7

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8. Weather Protection Devices ,in the Heavy Equipment Industries.

8-1. Description of Workshop Z

As we have already described in our Research Proposal, we restrict the scope of heavy-equipment and construction industries to be studied to the works which are carried out within the same enterprises with shipyards as a field of their diversified operation.

We have selected a large scale construction shop, workshop Z, that is located beside shipyard W in central region of Japan. Weather variations in Workshop Z is the same with that of shipyard W. (cf. 3. seq.) The products in this workshop Z are steel bridge, highway structure, water sluice gate, hydraulic pipe, parking facilities and steel frame for building etc.

8-2. Weather protection devices adopted.

The surface of this workshop Z is not covered by roofs, exports a part of paint shop, that has a floor space of 30,030 ft² of which 3,305 ft², i.e. 11% of space is now covered by roof (the data of which are given in Table 4, Collection of Data.) Protection devices adopted other than roof are 1) heater,

2) Sunnet, 3) Water cooler and 4) Winter Cloth. heating devices that were introduced since 1968, were small portable gas-stoves to heat workers in the closed section of steel structure on the ground (cf. Table-7, Collection of Data and photograph No. 15). Sunnet were used since 1957 to shade workers from direct sunshine during summer. At present nets are made of nylon and have different size according to the places to be used. Water cooler that is shown in photograph No.17, commercially available ordinary one to serve workers on work surface in summer. Winter cloth (photograph 18) are supplied for rent, without fee, for every workers

during winter. The cranes on this work surface have same clamping devices as those of shipyards and the types and costs are shown in the Table-11 and 12, Collection of Data.

8.3. Their effects on productivity..

The use of protection devices are limited to rather simple ones like portable stoves, water-coolers and winter cloth. Thus, their effects on productivity can not be singled out and, it seems, have good effect on the moral of workers in some degree.

In this workshop, preheating of welding points are usually done by gas-burner method in low temperature. These additional works for welding usually reduce the productivity measured by man-hours by about 20%.
(cf. Table. 6-1. in the Report).

9 The distribution of shipbuilding costs in Japan

9-1 The method of estimation

The shipbuilding cost usually differ from the type and size of ship and from the conditions on which shipyard operates. Although tankers are the largest single type of ships that are constructed in Japan, there are wide variety of ships constructed among 25 major shipyards here, and it is impossible to get average figures on the shipbuilding costs. Another difficulty arises from the fact that the field of business of the most shipbuilding enterprises have been diversified significantly in recent years, and ^{it} distort cost figures appeared in company's annual financial statements.

Consequently, we select two shipbuilding companies whose manufacturing activities concentrate on shipbuilding and especially on single type of ship, so as to get relatively stable and reliable cost pictures. The figures base on the financial statement of these companies.

9-2. The distribution of shipbuilding costs

The shipbuilding company A has only a large shipyard in western region, according to climate classification used in this report, and the sales of shipbuilding department accounts for 82% of the annual company sales in 1971. The three fourth of shipbuilding sales comes from new construction and one fourth comes from reparting. The main product here is large tanker of 200,000 dwt.

The shipbuilding company B has also one major shipyard in northern region and the share of shipbuilding accounts for 88% of total annual sales in 1971. New construction was 94% of total shipbuilding sales in this year. The main

product in this company is small bulk-carriers from 25,000 tons to 28,000 tons in deadweight.

As for the cost items, Raw Material is including subcontractors and purchasing, Overhead is including the cost for capital components and salaries in general and administrative departments.

The distribution of costs in 1971 are shown in the Table 7-1, Raw Materials item accounts for about the half and Labour cost for slightly under 20%, whereas the Overhead is over 30%.

Table 9-1. The Distribution of Shipbuilding Costs compared with other Manufacturing Industries in Japan.
1971 (%)

Cost items Shipyards and Industries	Raw Mate- rials	Labours	Overhead charges	Total
Shipbuilding Co. A	49.1	19.8	30.9	100.0
Shipbuilding Co. B	50.4	15.8	33.6	100.0
Machinery Industry (except electrical)	60.3	16.9	22.8	100.0
Electrical Machinery for Industrial Use	51.8	21.1	27.1	100.0
Railway locomotives	60.3	16.9	22.8	100.0

SOURCE : Mitsubishi Research Institute, Kigyo
keiei no Bunseki (Financial Analysis
of Japanese Corporations),
No. 38, Dec, 1972.

Appendix H-1

Collection of Data

Appendix H-1.

Collection of Data

Explanatory Note to Table of Protection Facilities

- (1) The results of survey on rool installment

Table-1. Work environment with roofs

Type of workshop: No.1.

Table-2 do: No.2.

Table-3 do: No.3

Table-4 do: No.4

- (2) Table-5 Effects through "Indoorization" in *major* shipyards as of 1970.

- (3) The results of survey on protection facilities and devices

Table-6 Work environment-heat and cold protection facilities, Type of workshop: No.1.

Table-7 do: No.2

Table-8 do: NO.3

Tab2e-9 do: No.4

- (4) The results of survey on czane protection

Table-10 Protective equipment exclusively for cranes,

Type of crane No.2

Table-11 do: No.3

Table-12 do: No.4

Explanatory Note to Table of Protection facilities

Items	Definitions	Remarks
1. Type of Workshop	1. Block Assembly 2. Pre-Erection (Grand Assembly) 3. Erection 4. Coating	on dock or building berth
2. Type of Roof	1. Permanent building, wholly closed 2. " " , with travelling roof 3. Permanent building with roof, not wholly closed. 4. Travelling roof	
3. Covered Area	1. Covered ratio of Block Assembling Shop= $\frac{\text{Square meter of indoorized assembling surface}}{\text{Square meter of total of assembling surface}} \times 100$ 2. Covered ratio of Pre-Erection Shop= $\frac{\text{Square meter of indoorized pre-erection surface}}{\text{Square meter of total pre-erection surface}} \times 100$ 3. Covered ratio of Building Berth and Dock= $\frac{\text{Square meter of covered area}}{\text{Square meter of Building berth and Dock}} \times 100$	
4. Type of Acquisition (Roof)	1. Owened 2. Rental	
5. Capital Costs (Roof)	Building Construction Cost+ Civil Engineering Cost and - Cost for Auxiliary Facilities	

Explanatory Note (continued)

Items	Definitions	Remarks
6. Operating Cost	Yearly maintenance cost for particular covered area	
7. Type of Protection Devices.	1. Ventilating Fan. 2. Air Conditioner & Stoves 3. Water Cooler 4. Winter Cloth 5. Sunnet 6. Cool Suits.	
8. Type of Utilization	1. Supplied as standard equipment to workers 2. Lended when need arises	
9. Capital Cost (Devices)	Costs to introduce or purchase the devices	
10. Operating (Devices)	Yearly replacement costs	
11. Type of cranes	1. Overhead traveling crane 2. Bridge crane 3. Jib crane 4. Goliath crane	
12. Crane capacity	Lifting capacity	
13. Type of workshop	same as Item 1.	
14. Type of protection methods.	1. Rail clamping 2. Hooking 3. Pin drop 4. Guy wire	
Operating costs	Yearly main-tenance costs for particular protection method	

(1) The results of enquete on roof installment

Table 1. Work environment with roofs
Type of workshop: No.1

Shipyards	Floor space of work shop, ft ²	Covered space ft ²	Covered rate (%)	Type of covering	Type of acquisition	Capital costs \$ per ft ²	Operating costs \$ per year	Description of facilities code number of photos specification of structures
W	39,611	35,305	89	1		-		1.2. steel structure, galvanized iron sheet
X	85,357 143,697	85,357 143,697	100 100	1 1+3		14.55 14.12	6,004 8,260	1.2. 1.2.3. " "
Y	775,600	775,600	100	1		11.72		1.2. steel structure, colored iron sheet
W	27,986	27,986	100	2		15.88		4.5.6. steel structure, long colored iron sheet
V	25,833	25,833	100	2	1	14.12		4.5.6. steel structure, slated roof,
X	37,027	37,027	100	2		8.82	2,622	4.5.6. steel structure, galvanized iron sheet
Y	62,107	62,107	100	2		15.42		4.5.6. steel structure, colored iron sheet
W	91,008	59,944	66	4		3.53		7.8. Eslon(Corrugated vinylchloride resin sheet)
V	62,377	12,378	20	4		12.36		7.8. steel structure, galvanized iron sheet,
X	52,635	20,666	40	4		2.12	1,444	7.8. steel structure, galvanized iron sheet,
Y	-	-	-	-				readily movable bownet roof
total	1,403,238	1,285,905	92	The rise in productivity by covering in the cases amounts to 20 to 30 percent.				

table 2. Work environment with roofs
Type of workshop: No.2

Shipyard	Floor space of workshop ft ²	Covered space ft ²	Covered rate (%)	Type of covering	Type of acquisition	Capital/costs \$/ft ²	Operating costs \$ per year	Description of facilities	
								Code number of photos	specifi- cation of structure
Y	447,503	97,682	21	2	1	15.42	-	4.5.6.	steel structure, colored iron sheet
total	447,508	9,075	21						

table 3. Work environment with roofs
 Type of workshop: No. 3

Shipyard	Floor space of workshop ft ²	Covered space ft ²	Covered rate (%)	Type of covering	Type of acquisition	Capital costs \$/ft ²	Operating costs	Description of facilities	
							\$ per year	Code number of photos	specifi cation of structure
Y.	1,130,206	107,640	10	4	1	25.60	-	7.8	steel structure, colored iron sheet
total	1,113,206	107,640	10						

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table 4. Work environment with roofs
Type of workshop: No.4

Shipyard	Floor space of workshop ft ²	Covered space ft ²	Covered rate (%)	Type of covering	Type of acquisition	Capital costs \$/ft ²	Operating costs \$ per year	Description of facilities	
								Code number of photos	specifi cation of structure
Y.	80,730	80,730	100	1		9.00		4.5.6.	steel structure, colored iron sheet
X	35,520	35,520	100	2	1	15.88	2,508	9. 10	steel structure, galvanized iron sheet
Z	30,000	3,300	11	2		30.18	1,140	9. 10	" "
W	30,250	21,530	71	4		8.93	-	11. 12	"
total	176,500	141,080	80						

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(2) Table 5.

Effects through "Indoorization" in major shipyards as of 1970.

Region	Shipyard	Increase of floor use rate (%) (1)	Reduction of manhours (%) (2)	Remarks
North- ern	V	40	20	
	E	10-15	5 (only for outdoor works)	
Central	W	30	15	
	L	20-25	15	
	K	20	15	
	J	in some degree	10	plus improvement in working environment
Western	O	20	15	increase in safety and quality through improvement in working conditions.
	P	100 (in final assembling)	30	
	X	10	10	

Note: (1) ratio of fabricated steel in tons persquare meters of assembling yards. This ratio does not directly correspond to the annual increase rate of production capacity. By increasing floor use rate at particular workshop, additional works could be done, if other production factors, especially manpowers, were provided to carry out this additional works. Empirically, annual increase of production capacity rather corresponds to the rate of reduction of man-hour consumed.

(2) man-hours per tons of ships constructed.

Source: Nihon Zosen Kogyokai (Shipbuilders' Association of Japan)

(3) The results of survey on protection facilities and devices

Table 6. Work environment-heat and cold protection facilities

Type of workshop: No. 1

Workshop	Type of protection facilities	Standard of equipment (number of units per person)	Type of acquisition	Capital Costs			Operation Costs			Specification Code number of photos	remarks
				number of facilities (number of unit per person)	cost per unit / (\$ /unit)	total cost (\$)	number of supplied facilities (number of units per person)	cost per unit (\$)	cost per unit (\$ / person/year)		
X	1	0.25	1	0.249	357.2	52151.2	0.026	357.2	9.11	13.14	
Y		0.20		0.195	407.0	52320.0	-	-	-	13.13	
W		0.42		0.420	357.2	46793.2	0.176	38.0	6.70	13.14	
X	2	0.02	1	0.022	60.8	433.2	0.022	11.4	0.25	15	
V		0.20		0.199	60.8	2158.4	-	-	-	15	
W		0.04		0.036	190	3990.0	0.003	190.0	2.65	17	
X	3	0.03	1	0.027	247	5187.0	-	-	-	17	
Y		0.05		0.048	190	2850.0	0.048	19.0	0.91	17	
W		0.08		0.008	171	342	-	-	-	17	
Y	4	0.01	1	0.013	13.3	133.0	-	-	-	16	
W		0		0	-	-	-	-	-	18	
V		1.00		1.000	190	2660.0	-	-	-	10	
X	5	0.02	1	0.017	15.96	159.6	0.002	15.96	0.027	-	
W		0.03		0.032	15.96	159.6	-	-	-	-	
Y		0.14		0.136	38	3040.0	0.014	38.0	0.52	19	
Y	6	0.08	2	0.077	50.4	1824.0	-	-	-	19	
W		0		0	-	-	-	-	-	19	
W		0		0	-	-	-	-	-	19	

(3) The results of survey on protection facilities and devices

Table 7. Work environment-heat and cold protection facilities

Type of workshop: No.2

Workshop	Type of protection facilities	Standard of equipment (number of units per person)	Type of acquisition	Capital Costs			Operation Costs			specification Code number of photos	remarks
				number of facilities (number of unit per person)	cost per unit (\$/unit)	total cost (\$)	number of supplied facilities (number of units per person)	cost per unit (\$/unit)	cost per unit (\$/person/year)		
X	1	0.14	1	0.143	357.2	10716	0.014	357.2	2.33	13.14	
Y		0.19		0.194	368.6	12160	-	-	-	13.14	
Z	2	0.05	1	0.050	190.0	1140	0.042	190.0	0.95	15	
X	3	0.02	1	0.024	190.0	750	-	-	-	17	
Z		0.08		0.083	72.2	722	0.017	72.2	1.20	17	
Y	4	0.07	1	0.071	13.3	159.6	-	-	-	18	
Z		1.00	2	1.000	11.4	490.2	0.233	11.4	2.65	18	
X	5	0.04	1	0.048	15.96	159.6	0.005	15.96	0.076	-	
Z		0.27		0.267	15.96	500.2	0.083	15.96	1.33	-	
X	6	0.29	1	0.236	38.0	2280.0	0.029	38	1.09	19	

(3) The results of enquete on protection facilities and devices

Table 8. Work environment-heat and cold protection facilities

Type of workshop: No.3

Workshop	Type of protection facilities	Standard of equipment (number of units per person)	Type of acquisition	Capital Costs			Operation Costs			specification Code number of photos	remarks
				number of facilities (number of unit per person)	cost per unit (\$ /unit)	total cost (\$)	number of supplied facilities (number of units per person)	cost per unit (\$ /unit)	cost per unit (\$ / person/year)		
X	1	0.28	1	0.278	357.2	89300	0.028	357.2	9.94	14	
Y		0.17		0.168	541.9	109440	-	-	-	14	
W		0.30	2	0.302	357.2	57152	0.094	38	3.58	14	
V		0.31	1	0.310	342.0	40356	-	-	-	14	
X	2 cooler	0.02	1	0.016	11400.0	159600	-	-	-	16	
W		0.02	2	0.015	11400.0	91200	-	-	-	16	
V		0.05	1	0.052	38.0	760	-	-	-	15	
X	3	0.03	1	0.026	190	4370	0.002	190	0.42	17	
Y		0.02		0.023	247	6916	-	-	-	17	
W		0.03	1.2.	0.026	190	2660	0.026	19	0.50	17	
V		0.02	1	0.016	114	684	-	-	-	17	
Y	4	0.10		0.028	13.3	1569	4	-	-	18	
W		0.57	1	0.566	8.7	2622	-	-	-	18	
V		1.00		1.000	19	2869	-	-	-	18	
X	5	0.33	1	0.334	15.96	4788	0.033	15.96	0.53	-	
W		0.77		0.774	15.96	6543.6	-	-	-	-	
X	6	0.61		0.612	38	20900	0.061	38	2.33	19	
W		0.66	2	0.657	45.6	1368	-	-	-	19	

(3) The results of survey on protection facilities and devices

Table 9 . Work environment-heat and cold protection facilities

Type of workshop: No.4

Workshop	Type of protection facilities	Standard of equipment (number of units per person)	Type of acquisition	Capital Costs			Operation Costs			specification Code number of photos	remarks
				number of facilities (number of unit per person)	cost per unit (\$ /unit)	total cost (\$)	number of supplied facilities (number of units per person)	cost per unit (\$./unit)	cost per unit (\$ / person/year)		
Y	1	3.14	1	3.140	419.5	65,888.2	-	-	-	13.14	
W		0.80		0.800	950	15,200	-	-	-	13.14	
W	2	0.20	1	0.200	2,280	9,120	-	-	-	15.	
Y	3	0.06	1	0.060	247	741	-	-	-	17	
W		0.05		0.050	190	190	0.050	190	9.5	17	
Y	6	3.00	1	3.000	30.4	4,560	-	-	-	19	

(4) the results of survey on crane protection

Table.10 Protective equipment exclusively for cranes

Type of crane: No.5.

Workshop	Capacity of crane	Place of equipment	Type of protective equipment	Total of capital (\$)	Operating costs (\$ per year)	Protective code number of photos	equipment specification of structure
W	31T	1	1	775.2	26.6	20	steel
	40T		1.3.	615.6	26.6	20.23.24	"
	10T		3		26.6	23.24	"

(4) the results of survey on crane protection

Table 11. Protective equipment exclusively for cranes
Type of crane. No. 3

Workshop	Capacity of crane	Place of equipment	Type of protective equipment	Total of capital (\$)	Operating costs (\$ per year)	Protective code number of photos	equipment specification of structure
W	80T/40T	3	1.3	2,223.4	83.6	20.23.24	steel
	40T/15T	1	1.3.4.	2,356.0	304.0	20.23.24.25	"
	20T/10T	3	1.3.4.	2,247.0	250.8	20.23.24.25	"
	125T/25T		1.4.	965.2	250.8	20.25	"
X	80T	1	2	7,220	-	21.22	"
	60T			5,700	-	21.22	"
W	6T/3T	3	2.4.	836	197.0	21.22.25	"
Y	100T/50T	2		9,120	494.0	23.24	"
	35T/10T	3	3	13,490	190.0	" "	"
	20T/10T	2		9,120	133	" "	"
	10T/5T	3		13,300	133	" "	"
W	90T/45T	3		14,440	83.6	" "	"
	80T/35T	1. 3	3	11,400	-	" "	"
	10T			2,660	-	" "	"
Z	20T/7.5T	2	3	608	60.8	" "	"
	15T/7.5T			608	60.8	" "	"
V	80T			-	-	" "	"
	50T			-	-	" "	"
	40T	3	3	-	-	" "	"
	45T			-	-	" "	"
	25T			-	-	" "	"
	10T	1		-	-	" "	"

(3) the results of survey on crane protection

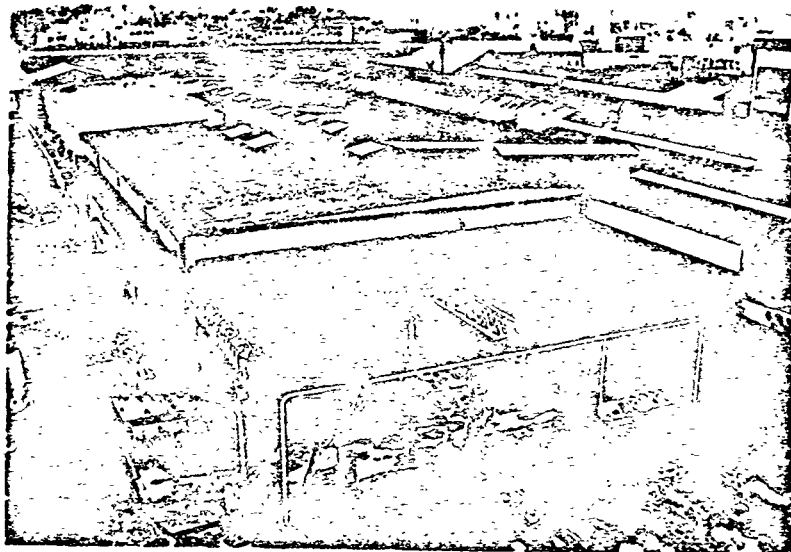
Table 12, Protective equipment exclusively for cranes
Type of crane: No.4

Workshop	Capacity of crane	Place of equip-ment	Type of protective equipment	Total of capital cost (\$)	Operating costs (\$ per, year)	Protective equipment	
						code number of photos	specification of structure
Y	600T	3	1.2.3.	98,800	912	20.21 22 23 24	steel
X	20T	2	2	4,180	-	21.22	"
	300T	3		23,560	-	"	"
	120T			9,652	-	"	"
	80T			8,170	-	"	"
Z	20T	2	4	1,026	49.4	25	"

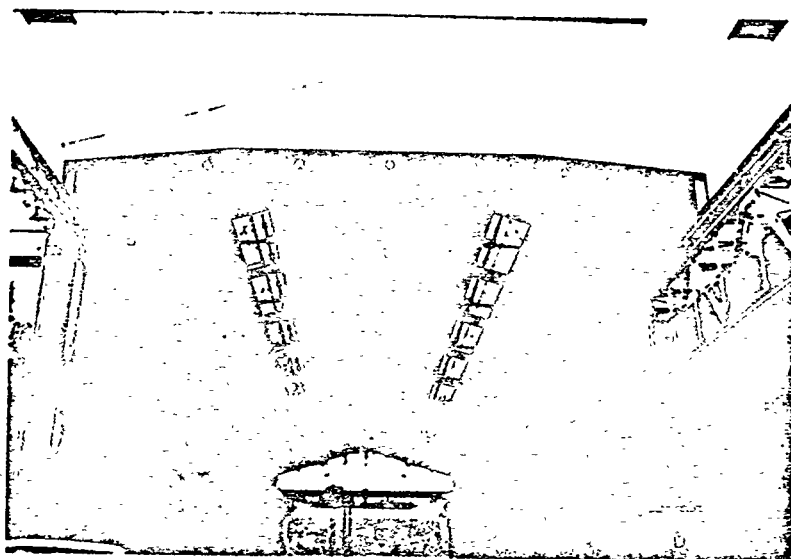
Appendix H-2

Photographed of Facilities and Devices.

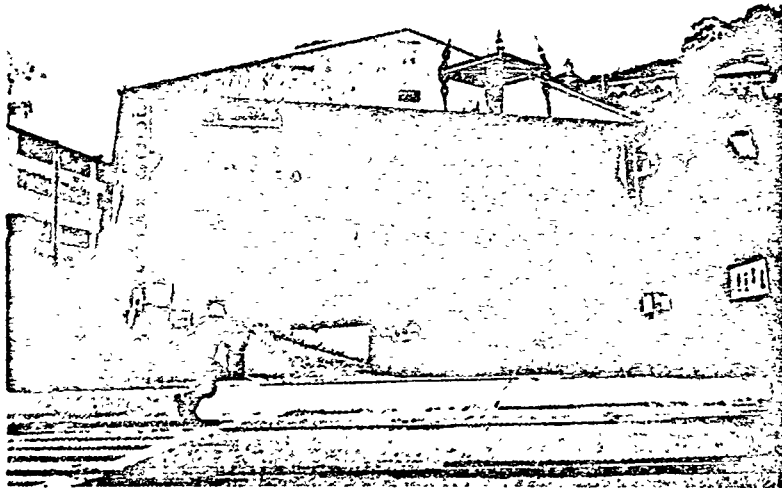
(Each number under pictures denote code number in the Tables in Appendix H-1, all pictures were taken during our survey on December and January 1973.)



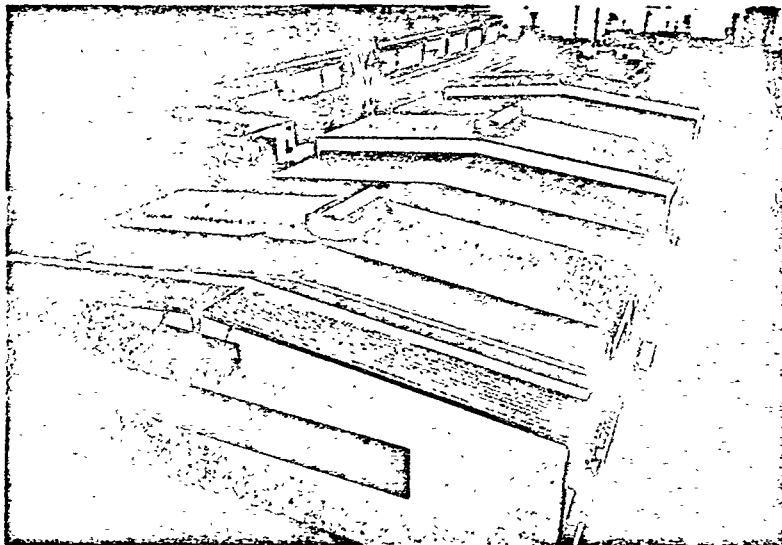
1. Roofed Block Assembly shop at Shipyard W in the Central region of Japan. Type of roof: permanent building, wholly closed.



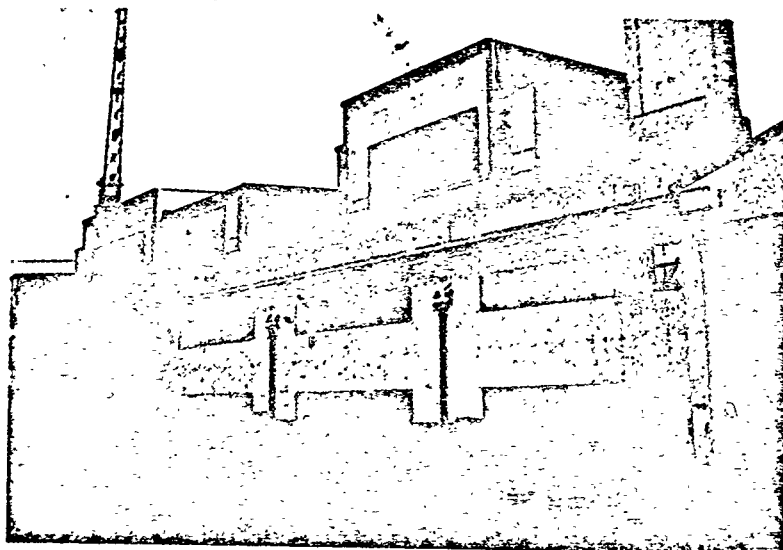
2. Roofed Block Assembly shop at Shipyard X in the Western region. Type of roof: same to 1.



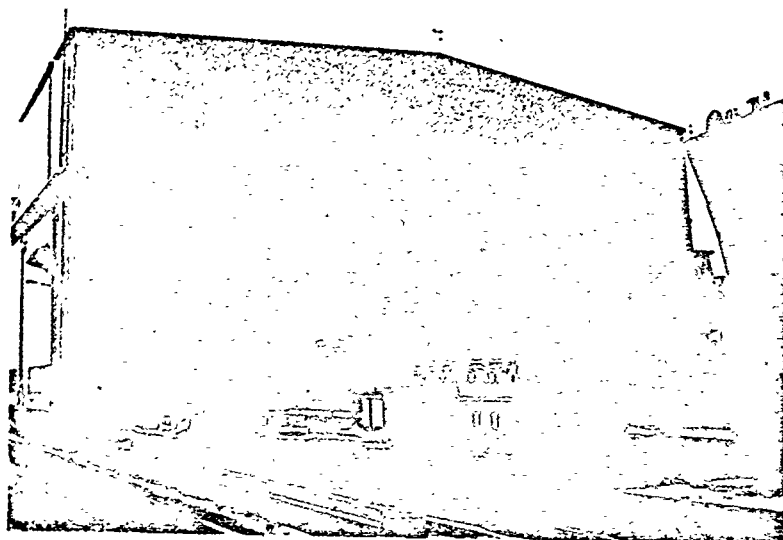
3. An assembled block is carried out from roofed Block Assembly shop at Shipyard X.



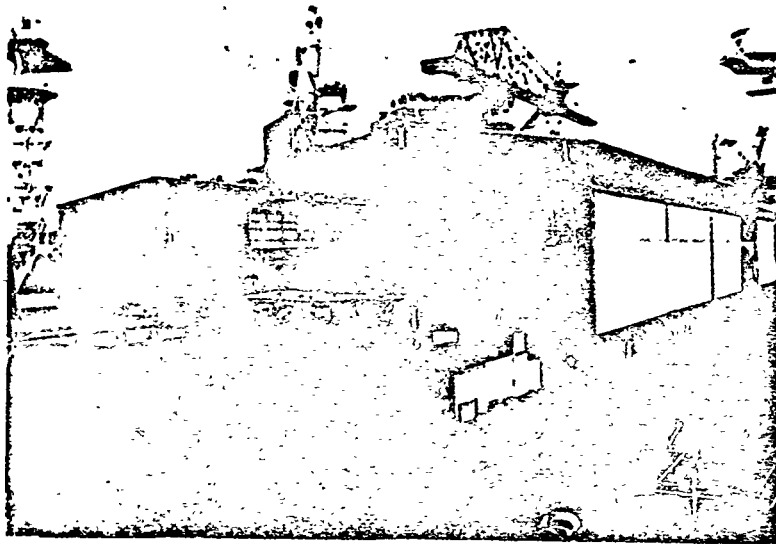
4. Block Assembly shop with travelling roof at Shipyard X. Type of roof: permanent building, wholly closed, with travelling roof.



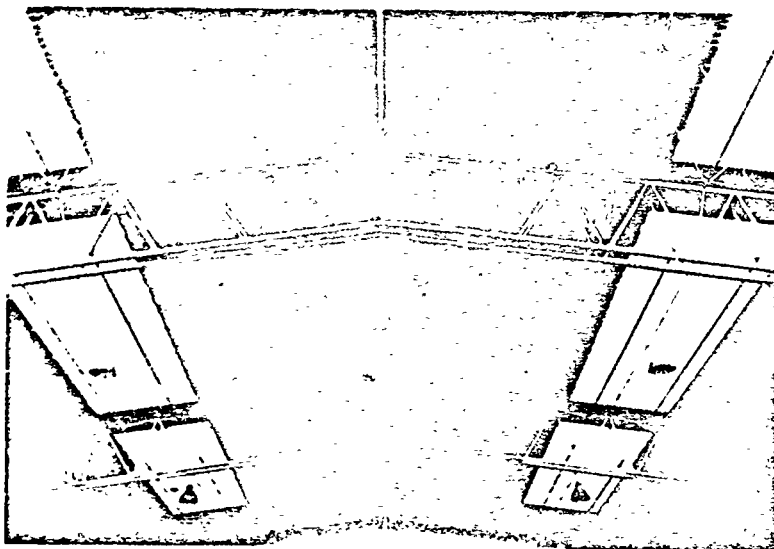
5. Block Assembly shop with travelling roof at Shipyard X. Type of roof: permanent building, wholly closed, with travelling roof.



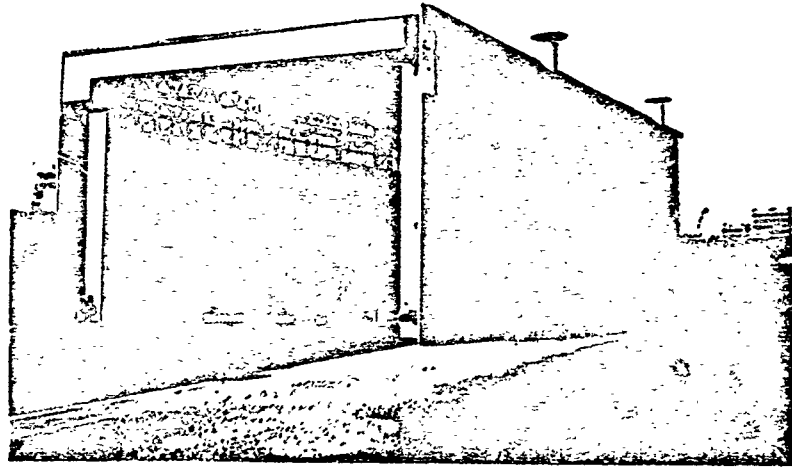
6. Block Assembly shop with travelling roof at Shipyard W.



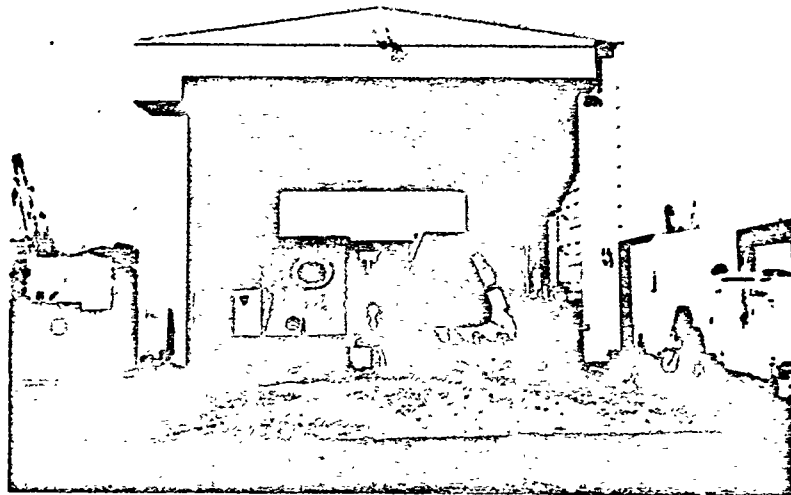
7. Block Assembly shop with travelling roof at Shipyard W. Type of roof: wholly travelling roof.



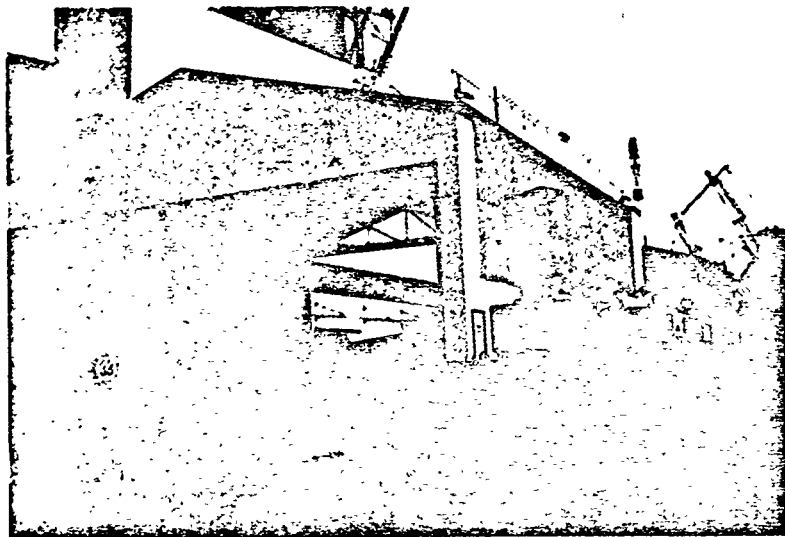
8. Block Assembly shop with travelling roof at Shipyard W. Type of roof: wholly travelling roof.



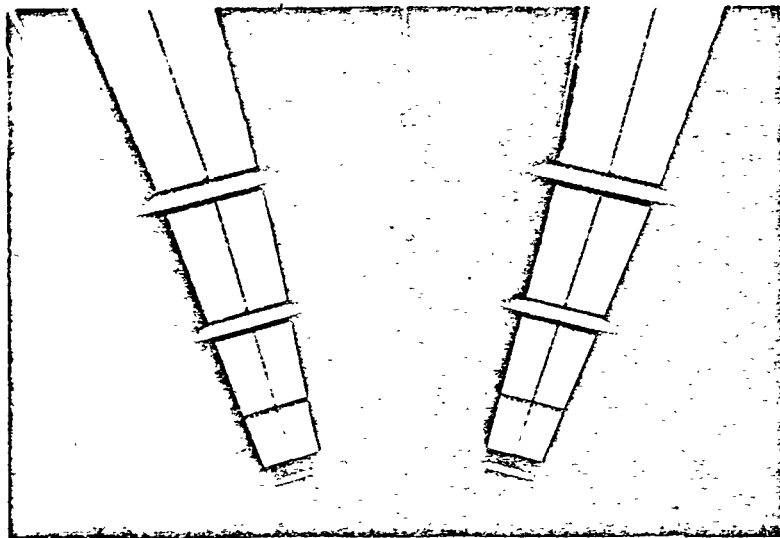
9. Painting/Coating shop at Shipyard X in the Western region.
Type of roof: permanent building, wholly closed, with travelling roof.



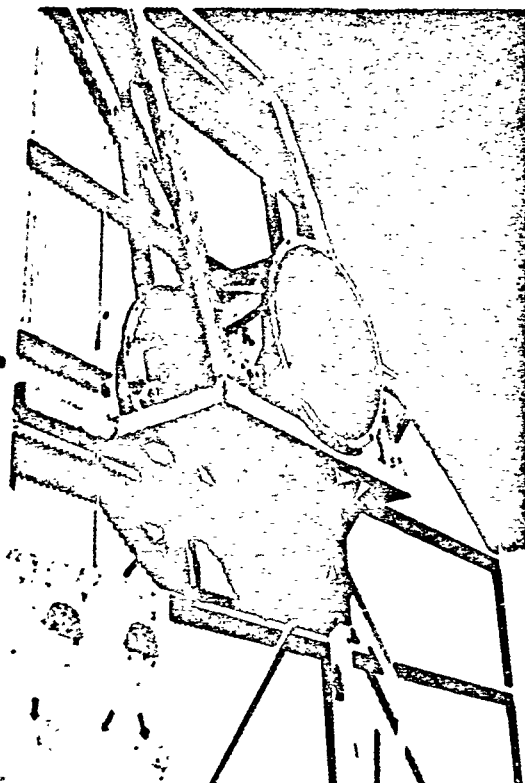
10. Painting/Coating shop at Shipyard X in the Western region.
Type of roof: permanent building, wholly closed, with travelling roof.



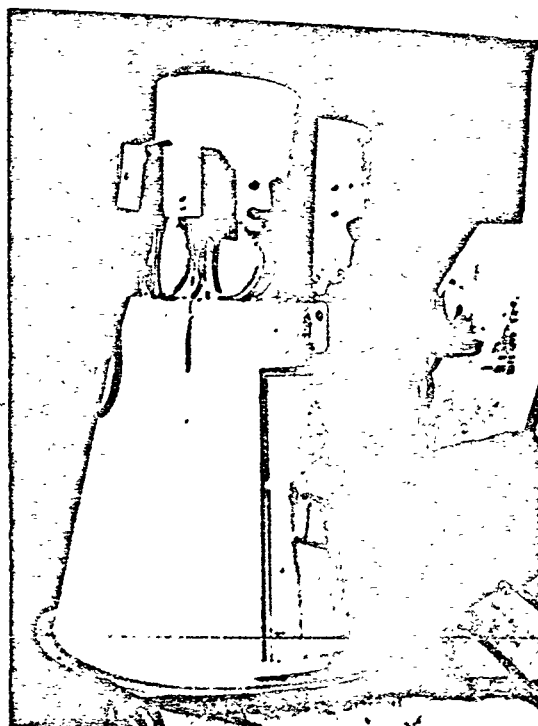
11. Painting/Coating shop at Shipyard W. Type of roof: Travelling roof.



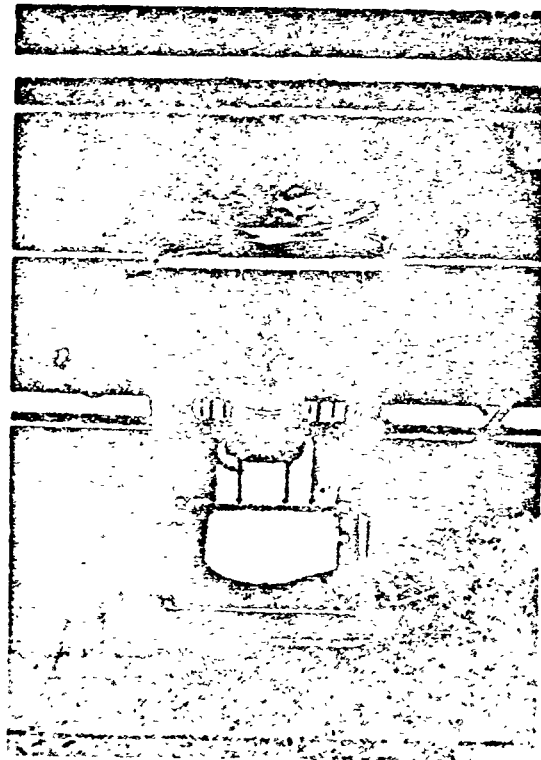
12. Painting/Coating shop at Shipyard W. Type of roof: Travelling roof.



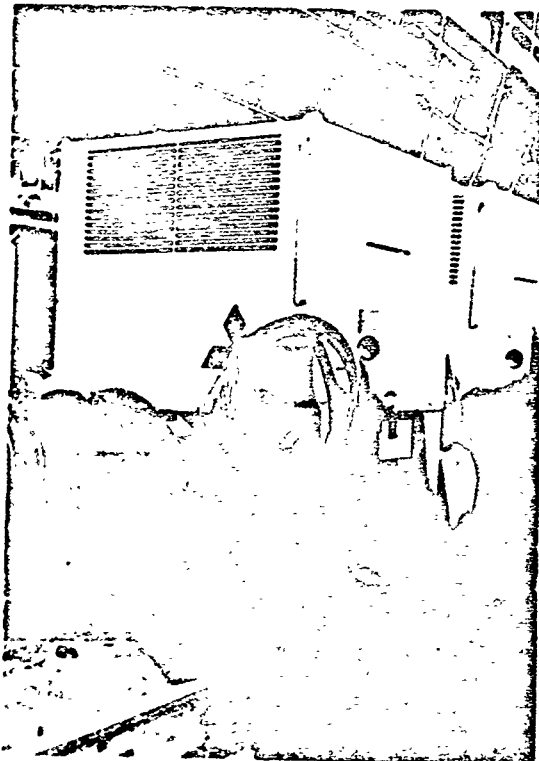
13. Ventilating Fan.



14. Ventilating Fan.

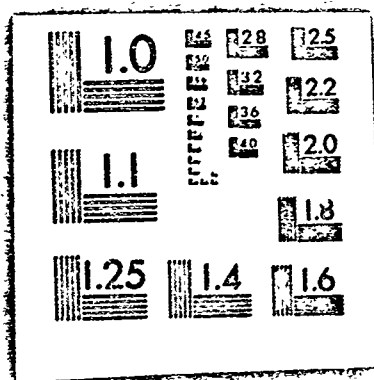


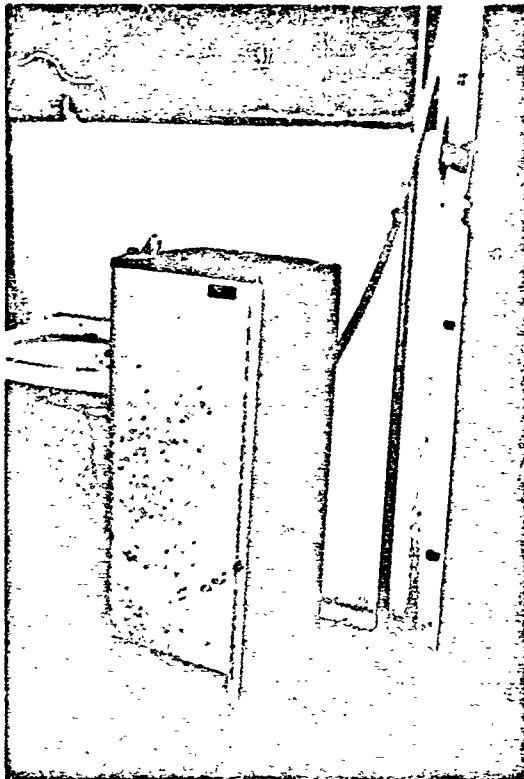
15. Gas Stove.



16. Air Conditionning Unit on the dock.

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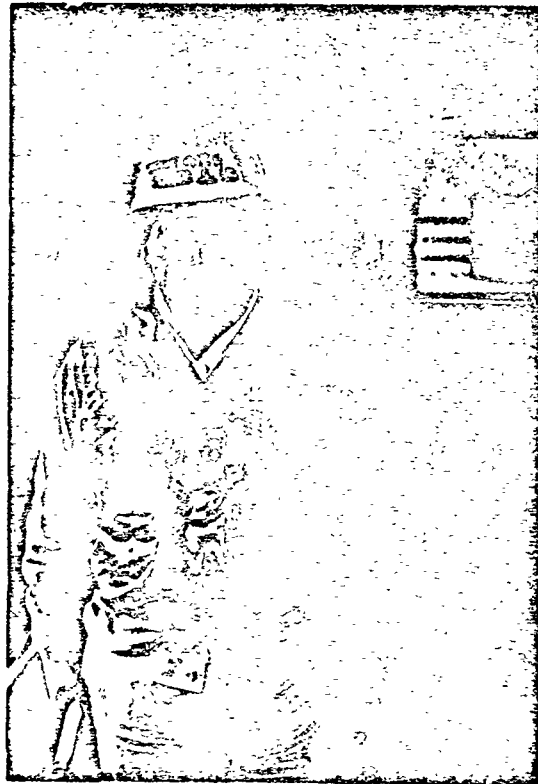




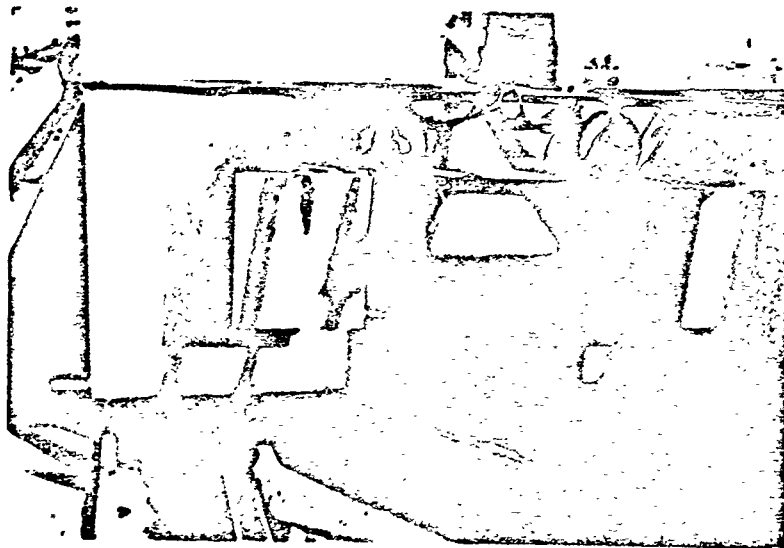
17. Water Cooler.



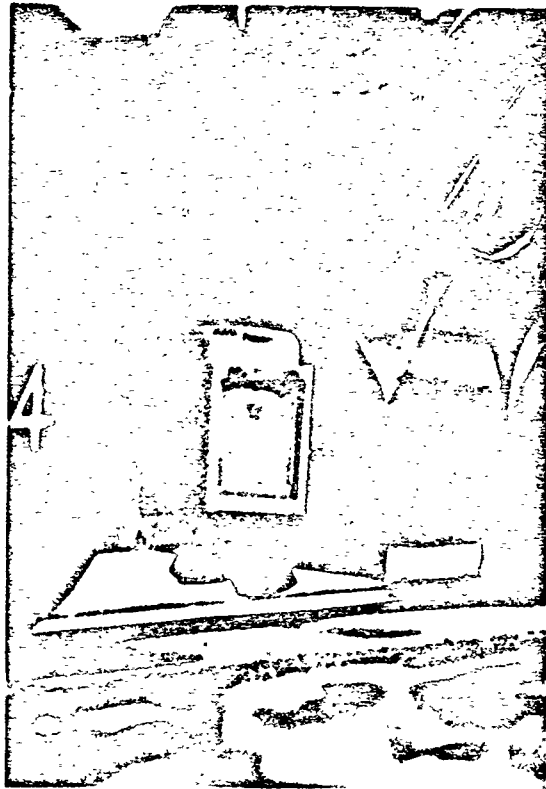
18. Winter Clo.,



19. A foreman wearing Cool Suits.



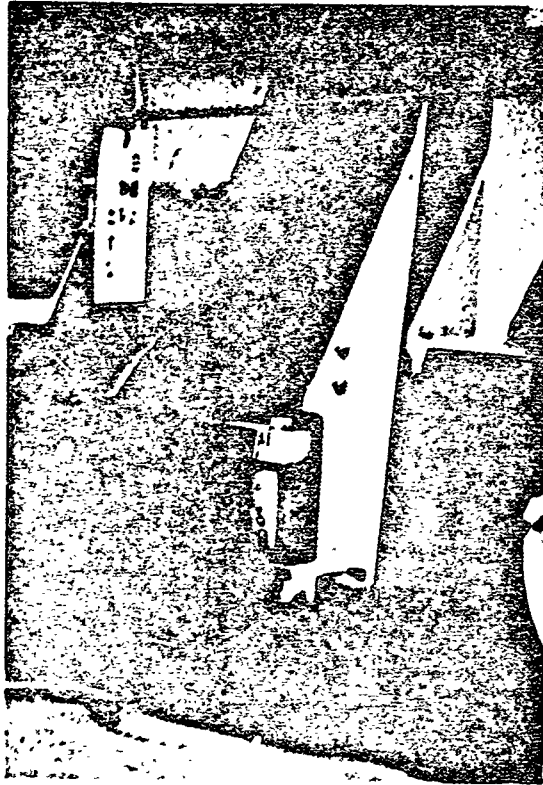
20. Rail clamping device for Bridge crane.



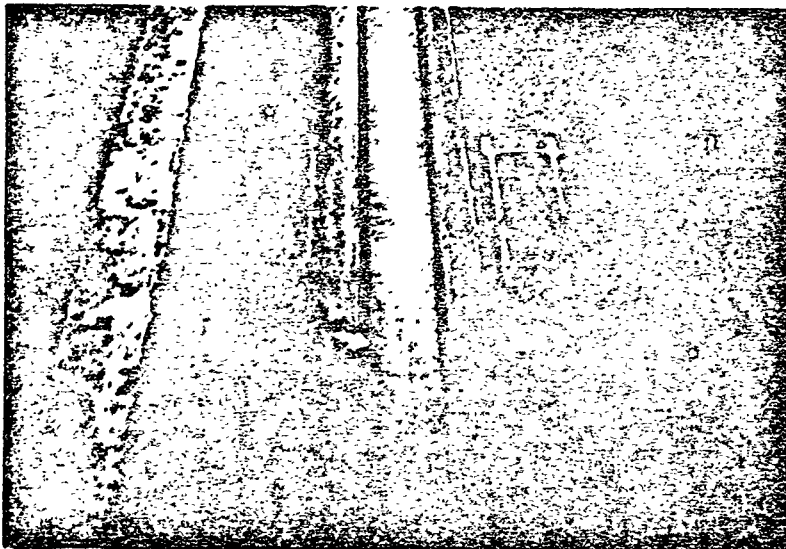
21. Hooking device for Goliath crane.



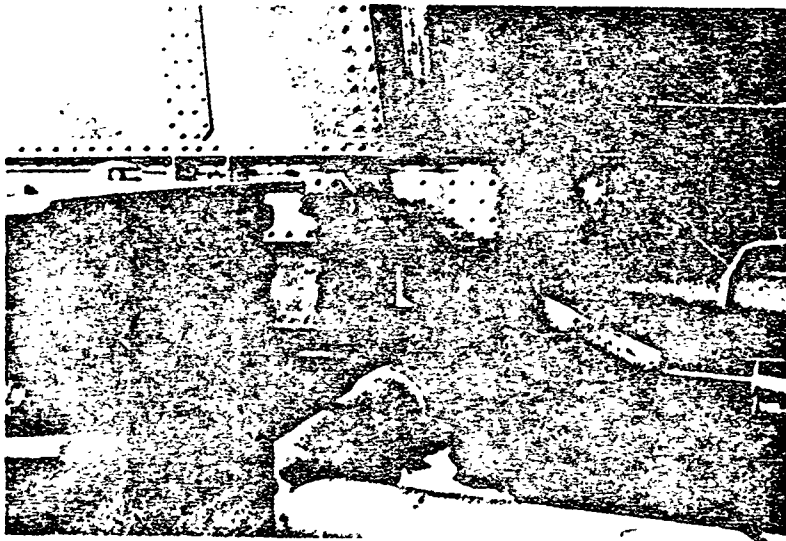
22. Hooking device for Goliath crane.



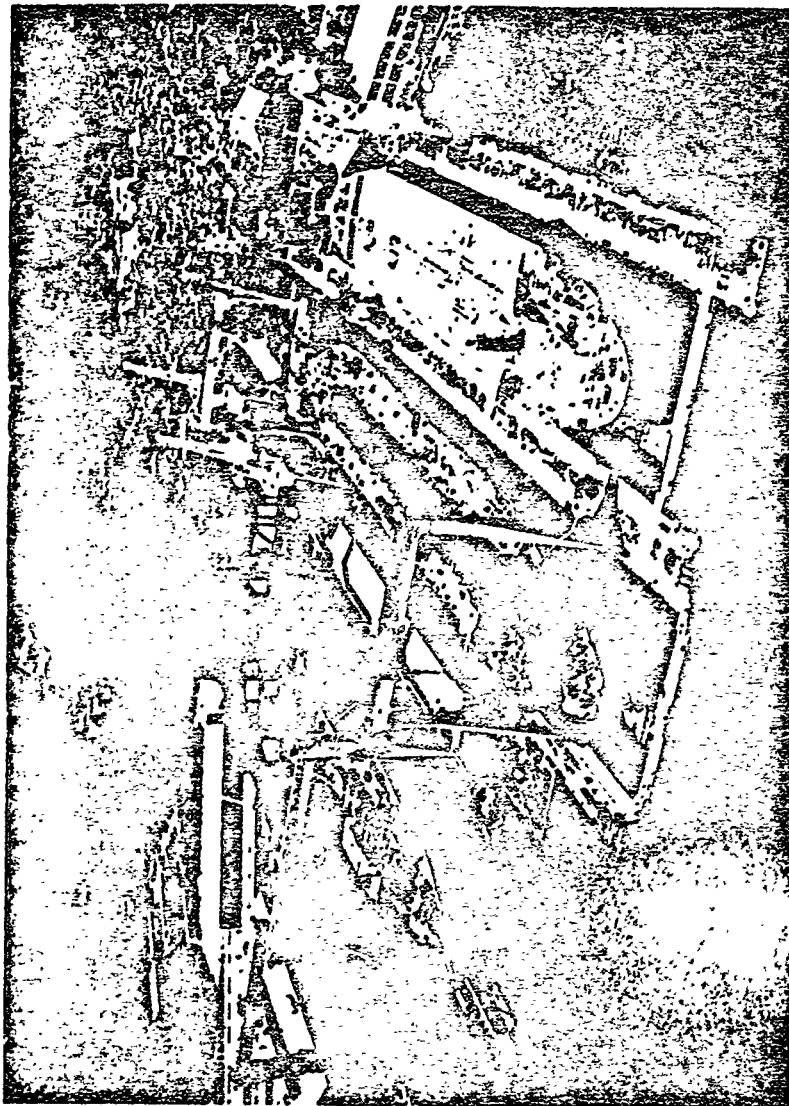
23. Pin drop device for Bridge crane.



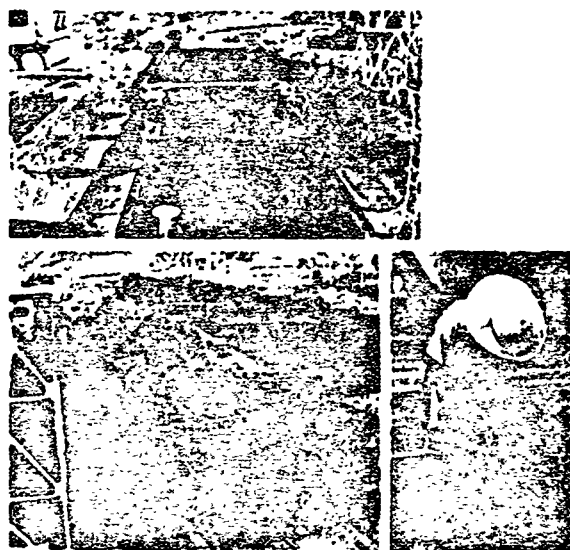
24. Pin drop device for Bridge crane.



25. Guy wire for Jib crane.



26. Goliath cranes at Shipyard X, each has carrying capacity 300 tons.



27. Sunnets over upper deck on the dock.

APPENDIX I
STATE-OF-THE-ART IN HEATHER PROTECTION
FACILITIES IN THE EUROPEAN SHIPBUILDING INDUSTRY

Battelle-Frankfurt Laboratories, Frankfurt, Germany conducted a study, "Heather Protection Facilities at European Shipyard", under a subcontract to Battelle-Northwest a part of this study. That report is reproduced here.

The report includes estimates of increases of productivity and actual increases of productivity for working with weather protection facilities along with capital and operating costs of several structures.

Reference is made on Page 12 of the report to English summaries of articles written in German. These are attached following the appendix section of the report. Photographs of movable "halls" and a hoarding panel system used in Germany are included at the end of the report.

Weather Protection Facilities
at European Shipyards

February 1973

A. Introduction

It is the intention of this report to describe the different types of weather protection facilities used at European yards and to demonstrate the improvements in working productivity and costs.

Literature reviews could only furnish a small part of the information required for the study- 50 special questionnaires were sent out to selected European shipyards and in addition, some German shipyards were contacted by telephone.

Unfortunately the results of these activities were not sufficient because most of the shipyards were not willing to cooperate-

Therefore the following information, especially the quantitative figures, can not be representative for the European shipbuilding industry.

Nevertheless, the figures delivered by questionnaires of two German, one Dutch and one Swedish shipyard, have been included in this report to give at least an order of magnitude. The report arrangement, which has been proposed by BNW, has been taken over as far as possible.

B. Designs, costs and effects of weather protection facilities

1. Permanent and portable weather Protection facilities used at European shipyards

1.1 Facility designs

The following weather protection facilities of different types and dimensions and for several shipbuilding activities are in use:

- halls with fixed roof

construction: steel or reinforced concrete with
overhead travelling cranes

used for: marking, burnings welding. erecting
of panels and sections

- halls with traversing roof

construction: steel or reinforced concrete with
overhead traveling cranes or other
cranes. working from outside through
the open roof

- used for: marking, burning, welding, erecting
of panels and sections
- movable halls
construction: steel frame; steel- or other
material-plating
moved by: vehicle, workmen
used for: marking, burning, welding, erecting
of panels and sections, assembling
 - sheds
construction: steel
used for: sandblasting, painting, storage,
general purpose
 - shacks
construction: wood
used for: storage, general purpose
 - portable roofs
construction: steel frame with corrugated plate
moved by: crane
used for: marking, burning, welding, painting
 - tarpaulin shelters, tents
used for: burning, welding, painting, storage,
general purpose
 - weather protection clothes
used against: rain, wind, ice, snow, coldness

1.2. Capital and operation related costs

The capital and operation related costs of some weather protection facilities are specified in table 1.

For better comparison, the costs are given in US dollars per square foot of floor area, too.

Table 1: Capital costs and operation related costs of some weather protection facilities

type of weather protection facility	floor area sq. ft.	capital costs related to 1972		operation related costs per year						
		US \$	US \$ per sq. ft.	repairing US \$	main-tenance US \$	hea-ting US \$	illu-minat. US \$	insu-rance US \$	total US \$	US \$ per sq. ft.
hall with fixed roof	15,000	95,000	6.33	2,400	1,250	2,400	500	320	6,870	0.46
hall with traversing roof	14,500	170,000	11.72	2,500	1,750	2,400	450	520	7,620	0.53
movable hall	3,200	10,000	3.13	930	310	-	160	125	1,525	0.48
portable roof	900	1,500	1.67	130	40	-	-	-	170	0.19
weather protection clothes (for 50 workmen)	-	1,550	-	160	-	-	-	-	160	-

NOTE: The above costs are for individual buildings and are not necessarily representative of capital and operating costs for buildings.

2. Methods and procedures of weather protection for personnel and material in the European heavy construction industry. Improvements in productivity and costs.

A special analysis of this branch has not been made, because many of the European shipyards build not only ships, but also docks, heavy steel constructions, apparatus, machines, etc.

Thus the conditions for the use of weather protection facilities are nearly the same.

3. Effects of weather protection facilities on productivity and costs in the European shipbuilding industry.

- Advantages and disadvantages in the use of weather protection facilities -

3.1 Advantages

- better working conditions
- better working quality
- no interruption of work by adverse weather conditions
- lower uncertainty in work planning
- no schedule delays
- increase of working efficiency
- lower production costs

- no removal of rain water, snow, ice
- less or no removal of dirt, dust, rust
- less or no preheating (when welding high tensile steel or painting)
- longer life span of shipbuilding tools and apparatus
- lower accident rate
- lower sickness rate
- possibility of working without daylight
- possibility of welding high tensile steels
- possibility of sand blasting
- possibility of using automatic devices
(e.g. submerged arc welding or gas-shielded arc welding)
- better possibility of control

3.2 Disadvantages

- narrow working space
- low height of crane hook (in halls with overhead travelling cranes)
- draft
- more heat
- more noise
- more welding and burning gases in the air
- more dust in the air during cleaning work

4. Increases of worker productivity obtained in the European shipbuilding industry by the use of weather protection.

4.1 Productivity per shift and worker

		without weather protection facilities in adverse weather conditions (snow, ice, rain, storm)	with Weather protection facilities
		<u>linear ft.</u>	<u>linear ft.</u>
welding	manual	65	120
	automatic	240	430
burning	manual	180	360
	automatic		570
		<u>Sq. ft.</u>	<u>Sq. ft.</u>
painting (including pre- liminary work such as derusting etc.)			
	manual	220	480
	with spray gun	380	760

The shipyards took the above figures from their production records.

Since thin plates afford a larger, and thick plates a smaller welding and burning productivity measured in linear ft., an average plate thickness has been assumed.

Figures for welding were assumed to be one run of welding.

Figures for painting were assumed for one coat film of the average thickness.

The significant difference between working productivities with and without weather protection facilities will of course decrease if better weather conditions are anticipated (see 4.2).

4.2. Productivity.per year

(basis for productivity without weather protection facilities = 100)

	without weather protection facilities	with weather protection facilities
marking	100	150
burning	100	165
assembling includixxg tack welding	100	140
welding	100	165
painting including preliminary work	100	170
other shipbuilding activities	100	135

The above figures have been estimated by the shipyards.

5. Additional work requirements and costs in European shipbuilding caused by environmental extremes

removal of

- - dirt
- - dust
- scale
- - rust
- - rainwater
- - snow
- - ice

- proheating for
 - - welding
 - - painting

more loss and repairing and maintenance of shipbuilding tools and apparatus

more loss of materials, e.g. welding electrodes and welding wire

- arrangement of safety devices to prevent damage by wind, storm, etc.

6. Secondary cost effects on worker productivity resulting from environmental extremes

6.1 Accident rates

(basis for accident rate without weather protection facilities = 100)

	<u>without weather protection facilities</u>	<u>with weather protection facilities</u>
in summer	100	95
in winter	100	75
throughout the year	100	85

6.2 Sickness rates

(basis for sickness rate without weather protection
facilities = 100)

	<u>without weather protection facilities</u>	<u>with weather protection facilities</u>
in summer	100	95
in winter	100	75
throughout the year	100	85

The above figures have been estimated by the shipyards.

C. Conclusion

Shipbuilding in Europe is shifting to an increasing extent
from non-protected open-air space to weather protected areas.

Weather protected facilities ensure improvements in working
productivity and working conditions.

Especially small and middle sized shipyards with adverse
climate conditions, e.g. Amels, IHC-Smit and Linz shipyards
(see literature), have erected and put into operation halls

for shipbuilding activities, which had been done in open air space before. In some cases even building docks and slip way areas have been covered by weather protection devices.

Most of the larger shipyards in Northwest Europe however, could not, or only partly, realize this idea of total inside shipbuilding up to now, because the capital costs for such great halls, covering the whole building areas, are too high in relation to the attainable output. The shipyards, in many cases, also have not got enough orders to justify such investments.

D. Literature about Weather Protection

1. "Überdachtes Baudock bei der Amels-Werft in Makkum"
- HANSA 1971, Nr. 21. p. 2096 -
2. "Binnenschiffbau in der Halle"
- Schiff und Hafen 1972, Nr. 4, p. 247 - 249
3. "Überdachte Helling bei IHC Smit"
- HANSA 1972, Nr. 24, p. 2270 - 2271
4. "Reconstruction of Öresundsvärvet"
- Schiff und Hafen, 1970, Nr. 11, p. 1038 - 1040

Copies of these articles are attached, additional English summaries of articles 1, 2, and 3.

Überdachte Helling bei IHC Smit

- Hansa 1972, No. 24, p. 2270 - 2271

Roofed Building Slip at IHC Smit Shipyard (Netherlands)

(English Summary)

The former shipyards L. Smit and J. + K. Smit, Kinderdijk, have been united to one shipyard within the IHC-Group since 1967.

The different situated local workshops require a reorganization of the entire shipyard and also the way of production. Shipbuilding should be accomplished without the influence of adverse weather conditions and rationalized to a high degree so that personnel savings can be obtained. Workmen are no longer willing to do shipbuilding work at unprotected and narrow places.

The new shipbuilding hall, existing of three naves, was finished in October 1972. Consequently the whole steel shipbuilding up to launching can be accomplished inside the hall.

The third nave covers the building slip, which has a bulkheading against the outside water in form of a pontoon. Ships with the dimensions of 459.2 ft. x 75.4 ft. can be built on the building slip.

The dimensions of the hall are 551.0 ft. x 167.3 ft. x 111.5 ft.

Ventilation is obtained through two ventilation channels, respectively 14 exhaustors, which are fixed within the roof. The hall can be heated by infra-red heating devices.

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Überdachtes Baudock bei der Amels-Werft in Makkum

- Harsa 1971, No. 21, p. 2096

Roofed Building Dock at Amels Shipyard, Makkum (Netherlands)

In 1968 Makkum Shipyard started a large program of modernization. The first part of this program was completed in November 1971.

The main investments are a roofed building dock with the dimensions of 393.6 ft. x 62.3 ft. x 23.0 ft. and a hall of 413.3 ft. x 121.4 ft. x 93.5 ft. Thus, all shipbuilding works can be accomplished without the influence of adverse weather conditions. The dock floor is situated 16.4 ft. below the outside water level, so even ships which are nearly fully fitted out, can be floated up inside the hall.

The hooks of the overhead travelling hall cranes are 72.2 ft. above the floor of the hall, respectively 95.1 ft. above the floor of the building dock.

At both ends of the hall there are sliding doors with a clear width of 60.7 ft. installed. The doors are driven electrically and tele-controlled.

Above the sliding doors, which reach up to the crane track, there are wing doors installed. When these wing doors are opened, the overhead travelling cranes can roll out of the hall on crane tracks nearly 45.9 ft.

The hall is illuminated by 125 mercury vapour lamps of 1000 watt each and through plastic windows of 21.3 ft. breadth in the walls. Ventilators are installed within the roof of the hall. The hall can be heated in the winter.

It is planned to lengthen the building dock 262.4 ft. and the hall 426.4 ft.

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Reg. (2)

Binnenschiffbau in der Halle

- Schiff und Hafen 1972, No. 4, p. 247 - 249

Building of River Vessels inside Halls

(English Summary)

On March 11, 1972, the Linz Shipyard (Austria) put into service a new shipbuilding hall (see plan, Hall No. IV).

There were several reasons for building the hall and altering the conventional procedure of shipbuilding:

- Shipbuilding should be accomplished without the influence of adverse weather conditions. It is very difficult to obtain qualified workmen who are willing to do the hard shipbuilding job in unprotected open air space.
- Increasing building costs should be stopped as far as possible by more productivity.
- There should be no uncertainty in work planning, which is very often the result of adverse weather conditions.
- Better quality of work should be achieved.
- The conditions of competition should be improved.

Technical data of the shipbuilding hall:

Dimensions:

Length: 328.0 ft; breadth: 114.8 ft; height: 78.7 ft.

Cranes: Two overhead travelling cranes of 40/10 t each, one crane of 10 t. Height of crane hook: 46.6 ft.

Sliding doors:

Dimensions:

west doors: 39.4 ft. x 3.8 ft; 39.4 ft. x 51.2 ft.

east door: 23.0 ft. x 52.5 ft.

Heating: 20 air heating devices of 353,149 cu. ft./hour.

The dimensions of the halls allow to build two river vessels of European type (Europa-Type) (278.8 ft. x 31.2 ft.) side by side.

The ships are completely outfitted in the hall and then brought out by rail cars.

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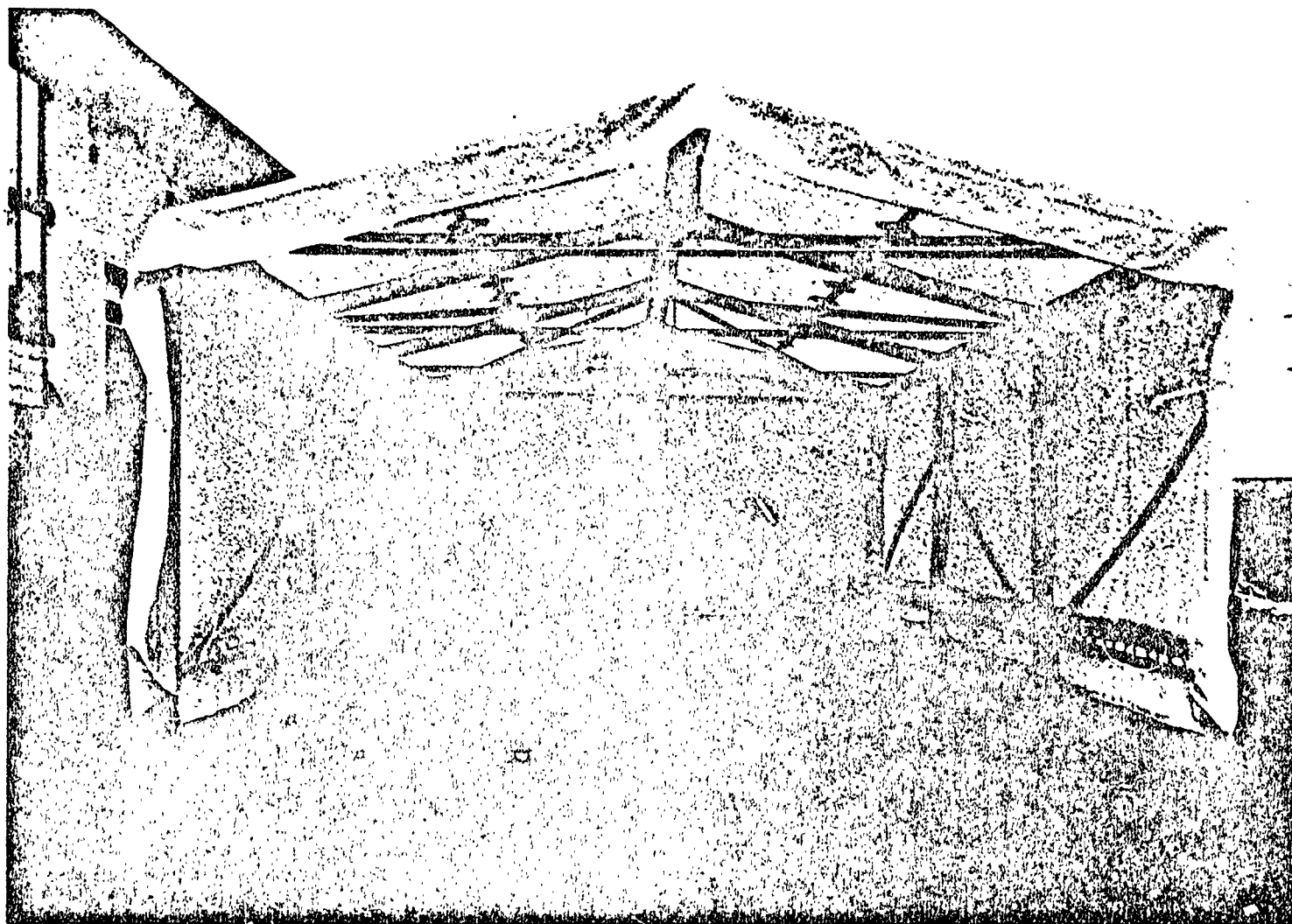


Figure I-1 - Lightweight canvas-covered portable shelter supported on rubber tired wheels. These unique wheeled buildings are manufactured by Josef Wirtz and Co. GmbH in Germany and have seen use in European shipyards.

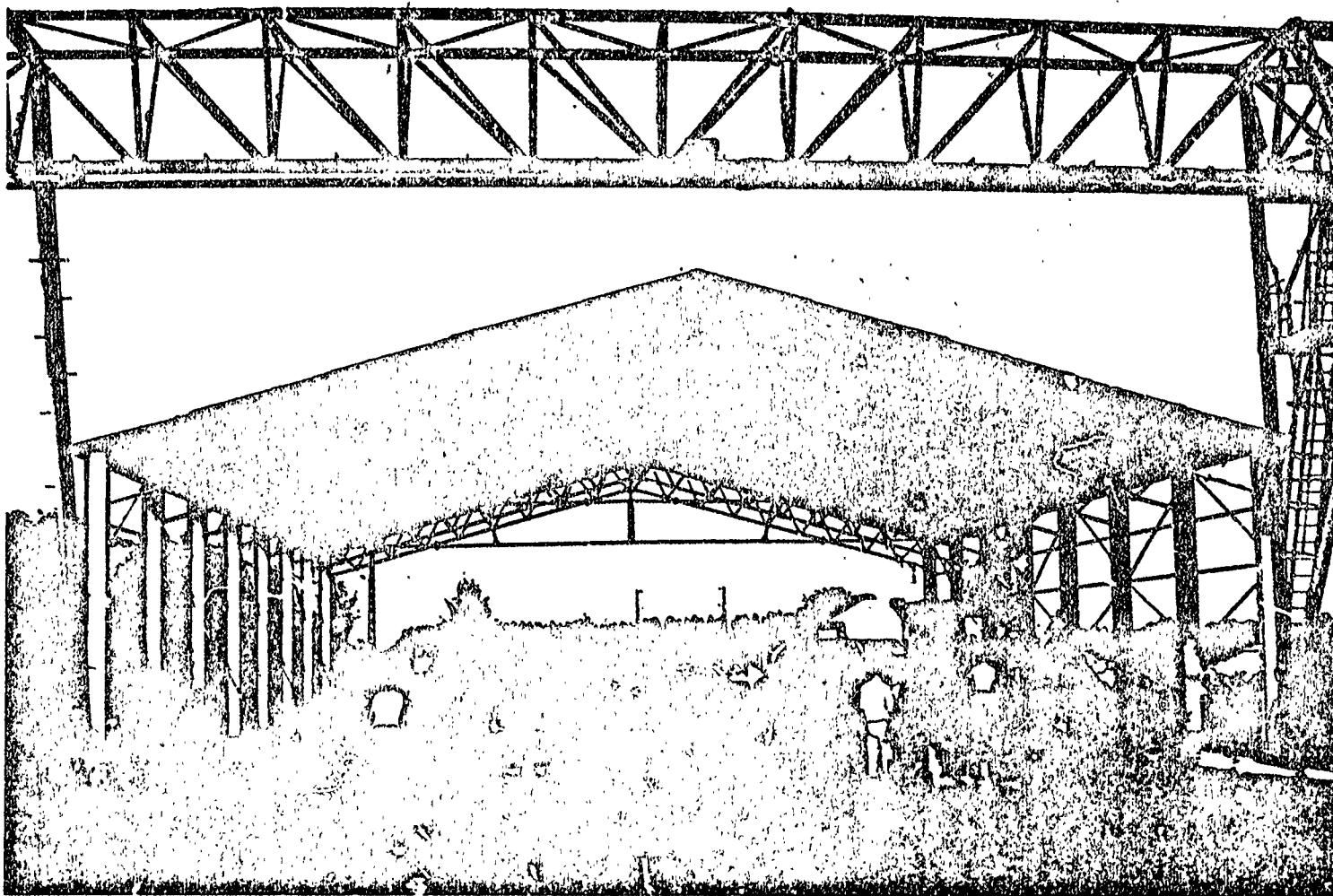


Figure I-2 - A movable hall, supported on wheels. These wheeled buildings may have sheet metal or canvas sides or ends, or be open as shown. They are manufactured by Josef Wirtz and Co. GmbH, Germany and have been used in European Shipyards and construction industry.

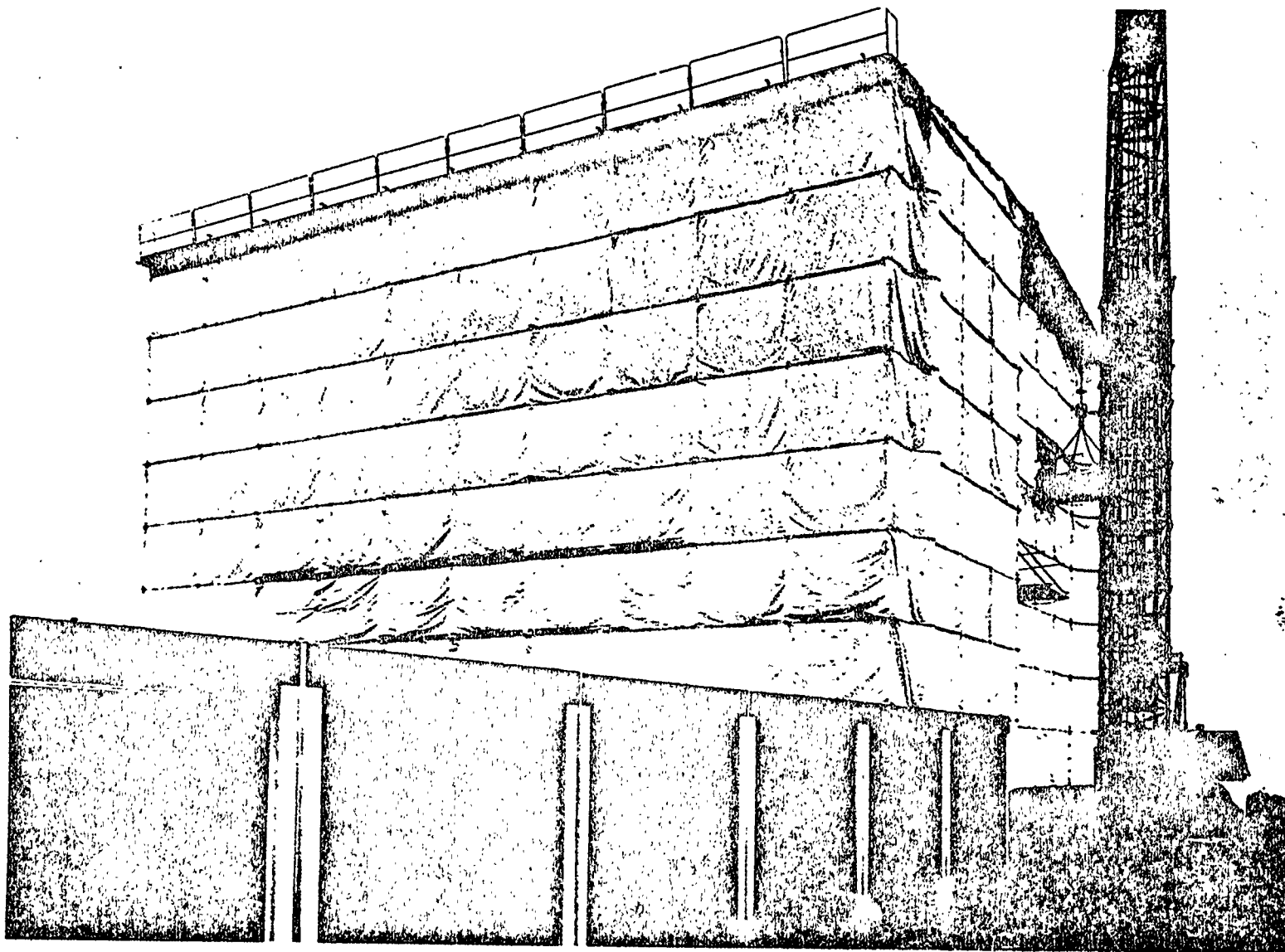


Figure I-3 - An example of the use of hoarding panels for weather protection in heavy construction in Germany. Note the access for materials delivery. These are called CENO plastic tilts and Carl Nolte, Germany is the patentee of this particular system. The fabric is reinforced PVC and is translucent.

APPENDIX J

DESCRIPTION OF THE STANDARD SHIPYARD

General

The productivity models were applied to a hypothetical "Standard" shipyard to obtain estimates of the cost effectiveness of various categories of weather protective structures. The purpose of the standard shipyard was to provide a yardstick against which anticipated benefits of this and other R&D programs could be measured. The standard shipyard description was provided by J. J. McMullen Associates as a part of a study on "Ship i'roductivity - Determination of Task Priorities." It describes both a "standard" shipyard and a "standard" ship.

The standard ship is a "Panamax" type of tanker with an overall length of 820 feet, a breadth of 105 ft, a depth of 60 ft and a displacement of 91,250 tons. Other particulars of the ship and its construction which are pertinent to this study are shown in tables in the following sections.

It should be pointed out that the "standard" shipyard is entirely synthetic having been created from a number of basic production requirements constrained by a number of typical environmental factors; although it is intended to be a standard United States shipyard, rather than a foreign one, any resemblance to any other shipyard, whether existing or defunct, is purely coincidental. It should be kept in mind that it is a tool for comparative analyses and is not intended to be an "optimum" shipyard.

The descriptions of the standard ship and the shipyard which follow are extracted from the J. J. McMullen Associates report.

The Standard Ship

The principal particulars of the standard ship, a "Panamax" tanker, are given in Table J-1. It is a traditionally high quality, subsidized construction vessel built to American Bureau of Shipping rules and conforming to all the usual requirements for U.S. flag operation.

A simplified breakdown of construction cost is presented in Table J-2 and expanded in Table J-3. Both of these exhibits display the elements of cost as percentages of the total: Table 5 converts the detailed data of Table J-3 to dollars, assuming that the total price for one ship in a continuous series is \$26,750,000 in mid-1973.

The weight breakdown of the seven steel classifications has been derived separately and is shown in Table J-5.

The Standard Shipyard

In formulating the standard shipyard, it was assumed that the standard shipyard, although built before World War II, has modernized its facilities to the fullest extent possible given its geographical and structural limitations.

It was also assumed that the shipyard has an annual steel throughput of approximately 40,000 tons, equivalent to three standard ships a year.

Table J-1

DESIGN FEATURES OF A STANDARD 75,000 DWT TANKER

Length Overall	820' - 0"
Length B.P.	780' - 0"
Breadth	105' - 0"
Depth	60' - 0"
Draft, full load	45' - 0"
Steel weight, tons	13,500
Outfit weight, tons	1,750
Machinery weight, tons	1,000
Lightship, tons	16,250
Deadweight, tons	75,000
Displacement, tons	91,250
Machinery	Geared steam turbine
SHP	20,000
Propellers	1
Speed, design, knots	16
Bunkers, tons	5,000
Endurance, miles	15,000
Pumps	3
Pump size, GPM	6,500
Cargo tanks	7
Accommodation	Aft
Classification	ABS
Registry	US
Crew	30

TOTAL PRICE BREAKDOWN

(Simplified)

	1. 26.31 %
Direct Material	<u>50.00</u>
Total Direct Cost	76.31
Indirect	5.26
Engineering	<u>2.63</u>
Construction Cost	84.20
overhead	<u>15.80</u>
Total Cost	100.00
Profit	<u>12.63</u>
Total Price	112.63 %

Table J-3

TOTAL PRICE BREAKDOWN
(Detailed)

<u>DESCRIPTION</u>	<u>MATERIAL</u> \$	<u>LABOR</u> \$
Shell Plating	5.31	4.25
Bulkheads and Pillars	4.56	3.08
Frames	6.64	5.14
Deck Plating and Beams	4.24	2.05
Superstructure	.55	1.55
Foundations	.14	.85
Castings	.70	.21
Total Steel	<u>22.14</u>	<u>17.13</u>
Masts and Rigging	.09	.05
Hatch Covers and Beams	---	---
Anchor, Cables and Hawsers	.75	.03
Hull Attachments and Joinerwork	3.05	.71
Generators and Distribution	2.15	.97
Reefer and Air Conditioning	.30	.07
Deck Auxiliaries	2.15	.19
Navigation and Steward's Outfit	.45	.16
Hull Plumbing	3.65	1.86
Ventilation	.40	.47
Paint	2.51	2.35
Total Outfit	<u>15.50</u>	<u>6.86</u>
Main Engine and Shafting	5.08	.23
Boilers, Fuel and Steam Systems	4.76	1.51
Pumps and Compressors	1.56	.07
Engineroom Outfit	.96	.51
Total Machinery	<u>12.36</u>	<u>2.32</u>
Total Labc-		26.31
Total Material		50.50
Total Direct Cost		<u>76.31</u>
Indirect		5.26
Engineering		2.63
Construction Cost		<u>84.20</u>
Depreciation	2.11	
Fringe Benefits	6.32	
Other	7.37	
Total Overhead		<u>15.80</u>
Total Cost		<u>100.00</u>
Profit		<u>12.63</u>
Total Price		112.63

Table J-4

TOTAL PRICE BREAKDOWN

DESCRIPTION	MATERIAL \$	LABOR \$
Shell Plating	1,262,500	1,010,000
Bulkheads and Pillars	1,085,000	732,500
Frames	1,577,500	1,220,000
Deck Plating and Beams	1,007,500	487,500
Superstructure	130,000	367,500
Foundations	32,500	202,500
Castings	165,000	50,000
Total Steel	<u>5,260,000</u>	<u>4,070,000</u>
Mast and Rigging	22,500	12,500
Hatch Covers and Be.ms	--	--
Anchors, Cables and Hawser	177,500	7,500
Hull Attachments and Joinerwork	725,000	167,500
Generators and Distribution	510,000	230,000
Reefer and Air Conditioning	70,000	17,500
Deck Auxiliaries	510,000	45,000
Navigation and Steward's Outfit	107,500	37,500
Hull Plumbing	867,500	442,500
Ventilation	95,000	112,500
Paint	595,000	557,500
Total Outfit	<u>3,680,000</u>	<u>1,630,000</u>
Main Engine and Shafting	1,207,500	55,000
Boilers, Fuel and Steam Systems	1,130,000	357,500
Pumps and Compressors	370,000	17,500
Engineroom Outfit	227,500	120,000
Total Machinery	<u>2,935,000</u>	<u>550,000</u>
Total Labor		6,250,000
Total Material		<u>11,875,000</u>
Total Direct Cost		<u>18,125,000</u>
Indirect		1,250,000
Engineering		<u>625,000</u>
Construction Cost		20,000,000
Depreciation	509,000	
Fringe Benefits	1,500,000	
Other	<u>1,750,000</u>	
Total Overhead		<u>3,750,000</u>
Total cost		<u>23,750,000</u>
Profit		<u>3,000,000</u>
Total Price		\$26,750,000

Table J-5

STEELWEIGHT BREAKDOWN

	<u>TONS</u>
Shell plating	3,375
Bulkheads and pillars	2,862
Frames	3,888
Deck plating and beams	2,660
Superstructure	500
Foundations	108
Castings	<u>107</u>
	13,500

The direct labor requirements of this rate of production are given in Table J-6. The direct labor costs in dollars from Table J-4 have been converted into manhours using an average rate of \$4.60, the projected average hourly rate for the United States shipbuilding industry at mid-1973, and the results have been multiplied by three to reflect the assumed output of three ships a year. In the second column, these manhours have been expressed as a percentage of total direct labor manhours~ and in the third column they have been divided by 2000 to arrive at the equivalent number of direct labor employees required. The total in this column shows an average direct labor requirement of 2038 workers.

The required direct labor workforce shown in Table J-6 is presented again in Table J-7 in such a way as to demonstrate the distribution of manpower both by function and work location.

It was further assumed that the standard shipyard is engaged in merchant ship construction only and all,naval and repair work is contained within a separate and distinct organization.

Although virtually all United States shipyards are involved simultaneously in both merchant and naval shipbuilding and ship-repairing, the impacts of cost reduction tasks on commercial ship costs can only be effectively evaluated if those costs are isolated from the shipyard's other activities. The implication of this assumption for the definition of the standard shipyard is that the labor force is perfectly balanced and fully occupied, a condition that can only be true in a shipyard building a single Product, a standard ship, since variations in product mix inevitably result in variations in labor function requirements.

Table J-6

LABOR REQUIREMENTS

<u>CLASSIFICATION</u>	<u>Annual Direct Labor Manhours</u>	<u>% of Total Direct Labor</u>	<u>Equivalent # of Men</u>
Shell Plating	658,700	16.2	329
Bulkheads and Pillars	477,700	11.7	239
Frames	795,600	19.5	398
Deck Plating and Beams	317,900	7.8	159
Superstructure	239,700	5.9	120
Foundations	132,100	3.2	66
Castings	32,600	.8	16
Total Steel	2,654,300	65.1	1,327
Masts and Rigging	8,200	.2	4
Hatch Covers and Beams	--	--	--
Anchors, Cables and Hawser	4,900	.1	2
Hull Attachments and Joiner Work	109,200	2.7	55
Generators and Distribution	150,000	3.7	75
Reefer and Air Conditioning	11,400	.3	6
Deck Auxiliaries	29,300	.7	15
Navigation and Stewards Outfit	24,400	.6	12
Hull Plumbing	288,600	7.1	144
Ventilation	73,400	1.8	37
Paint	363,600	8.9	182
Total Outfit	1,063,000	26.1	532
Main Engine and Shafting	35,900	.9	18
Boilers, Fuel and Steam Systems	233,100	5.7	116
Pumps and Compressors	11,400	.3	6
Engineroom Outfit	78,300	1.9	39
Total Machinery	358,700	8.8	179
TOTAL	4,076,000	100.0	2,038

Table J-7
DIRECT LABOR DISTRIBUTION

Location Function	Steel Fabrication & Related Shops	Steel Assembly Shops and Areas	Departmental Shops	Machinery Assembly Shops	Shipway	Outfitting Wharf	Totals
Steelwork	200	400	---	7	700	20	1327
Electrical	---	10	8	2	35	20	75
Piping	4	20	74	8	24	14	144
Sheetmetal	---	10	14	2	20	4	50
Joinerwork	---	---	10	--	15	20	45
painting	4	40	4	--	110	24	182
Machinery	---	20	12	40	48	59	179
Other	---	---	4	--	20	12	36
Totals	208	500	126	59	972	173	2038

The support workforce required by a standard shipyard with a direct labor workforce of 2038 was defined as 458 additional employees (for a total of 2496).

This proportion represents the position of the standard shipyard as an approximately average yard in the spectrum of United States shipbuilding. Indirect, engineering and overheads, which include the cost of the support workforce are shown in Table J-8.

Facilities and Production Processes in the Standard Shipyard

Steel arrives by rail and is unloaded and sorted by a gantry magnet crane in a stockyard of about 60,000 square feet, employing a horizontal storage and having a capacity for one shipset of steel. The standard plate size is 45 feet by 10 feet, although the maximum could be 48 by 12. This standard size is directly related to the design of the standard ship, 45 feet being one half of the tank length, and hence to the panel construction method.

The steel is fed by conveyor, via a surface preparation line involving the usual cleaning, mangling, blasting, painting and drying processes, into a fabrication shop of about 40,000 square feet, divided into four bays equipped for sections, flat panel material, shaped panel material and the remainder. The fabrication shop is equipped with the conventional cold forming machinery, template-controlled, and automatic burning machinery, optically-controlled. There is no numerical control. An overhead crane of 15 tons spans each bay.

Table J-8

INDIRECT, ENGINEERING AND OVERHEAD COSTS

(MARAD GROUPINGS)

	% of Costs	Cost in \$.	Equivalent # of Men
<u>Indirect Costs</u>			
Insurance and bond premia, fees for classification and testing, royalties of a general nature.	.26	\$ 187,500.	--
Drydocking, launching trials and delivery costs, including supplies, catering, trials personnel, pilots, tugs, calibration, etc.	.79	562,500	--
Miscellaneous labor for ship cleaning, toolrooms, watchmen, materials handling, supervision, industrial engineering functions.	2.63	\$1,875,000.	200
Sundry other items, including travel, temporary services, weather protection, fire prevention, gasfreeing and analysis, photography.	1.58	\$1,125,000.	20
	5.26	\$3,750,000	220
<u>Engineering Costs</u>			
Drawings, calculations, yard liaison, purchase requisitions, tests, microfilming, model testing, outside professional services.	2.63	\$1,875,000	80
<u>Overhead Costs</u>			
Depreciation, insurance and taxes.	2.11	\$1,500,000.	--
Maintenance and repair of all property, buildings, machinery and equipment, fixed or portable.	2.11	\$1,500,000.	18
Wages and salaries of all other personnel, including management, departmental supervision, clerical staff, maintenance personnel, crane operators, storekeepers, drivers, production planning, welfare services and administration.	2.63	\$1,875,000.	100
Supplies of services and maintenance and administrative requirements.	1.58	\$1,125,000.	--
Fringe benefits, including vacation and holiday pay, bonuses, social security, life insurance, unemployment tax, workmen's compension, sick benefits, excused time, etc.	6.32	\$4,500,000	--
Miscellaneous other costs, including accidents, losses, welfare, travel, R and D, estimating, advertising, etc.	1.05	\$ 750,000.	40
	15.80	\$11,250,000.	158
Total indirect, engineering and overhead:	23.69	\$16,875,000	458

The section and flat panel material bays lead into a flat panel assembly shop of about 20,000 square feet, featuring eight working areas, of 2,500 square feet each, for the construction of flat panels of plating with associated longitudinal and transverse framing, up to a maximum size of 48 feet by 30 feet, and averaging 60 tons each. Welding is semi-automatic, both of plate-butts and of stiffening, and material is moved and positioned using three overhead cranes, two of 75 tons and one of 15 tons. Average panel construction time is four to five days. The other two fabrication bays lead into a shaped panel assembly shop, also of about 20,000 square feet, where working areas are laid out as required for the more complex shaped panels. Welding is semi-automatic or manual and material is moved and positioned by means of similar cranes to the flat panel shop. Average panel construction time is eight to ten days.

All completed steel assemblies are moved outside to a paint shop where welds are cleaned and painted and then to storage areas or directly to the shipways: multi-wheel heavy-load transporters are used for these movements.

Machinery and outfit materials are received both by road and by rail and held in conventional warehousing and other storage areas until required. Machinery and outfit "work packages" are put together in various shops, mostly of an earlier generation, and delivered to work stations by truck or forklift. "These packages are normally but not necessarily trade-oriented: they may include material for several different operations planned to take place in the same work place. Limited panel outfitting takes place in the

steel assembly shops, being confined to the fitting of attachments for piping, cable trays and ventilation ducting.

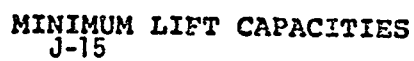
Ship erection is carried out on one of two shipways, starting with stern panels and working forward and upward. Each shipway is big enough for the standard ship with a working margin of five feet on each side and thirty feet on the length but no more. Each is served by four whirley cranes:

- two of 50 tons max. lift at 75 feet max. outreach
- one of 35 tons max. lift at 75 feet max. outreach
- one of 25 tons max. lift at 75 feet max. outreach

as shown in the sketch presented as Figure J-1. Average erection time is eight months at an average work rate of approximately one panel per day.

After launching, each ship is moved to a single outfit wharf where its stay averages four months.

DECEMBER



Outdoor Operations in the Standard Shipyard

The indoor operations and facilities and the outdoor shipways are described in the preceding pages.

The approximate uses and areas for outdoor operations which could be covered for weather protection were assumed to be in the ranges shown below:

<u>Description</u>	<u>Area</u>
Steel stockyard operation	60,000 sq.ft.
Machinery and outfit storage areas for bulky items of a non-weather-sensitive nature	As required
Cleaning and painting of welds on steel assemblies	10,000 Sq.ft. minimum
Panel storage (or module assembly, if desired) with associated pre-outfitting (if not completed in the assembly shop) or further pre-outfitting following module assembly including fitting of as many of the following items as seems appropriate to the shipyard management: pipes valves and other pipefittings ventilation ducts cable trays cable runs doors manholes skylights hull openings heating coils interior painting exterior painting machinery room outfit accommodation fitting to the extent that it is possible.	20,000 Sq.ft. minimum, up to 80,000 sq.ft.

DIRECT LABOR DISTRIBUTION IN THE STANDARDS SHIPYARD

The distribution of direct labor in the standard shipyard by craft and location is shown in Tables J-9 through J-11 for steel work, machinery work and outfit work. This distribution was used in the productivity model.

Table J-9
DIRECT LABOR DISTRIBUTION FOR STEEL WORK

Location Function	Steel Fabrication & Related Shops	Steel Assembly Shops & Areas	Departmental Shops	Machinery Assembly Shops	Shipway	Outfitting Wharf	Totals
Burners & Welders	a:60	160 { a:80 b:80	-	a:4	287 { b:110 c:177	30 { b:8 c:22	541
Blasters & Painters	10 { a:5 b:5	b:10	-	0	25 { b:20 c:5	15 { b:7 c:8	60
Fitters	a:107	187 { a:87 b:100	-	a:2	285 { b:113 c:172	25 { b:6 c:19	606
Riggers	20 { a:18 b:2	40 { a:20 b:20	-	a:1	39 { b:14 c:25	8 { b:2 c:6	108
Other Crafts	a:3	b:3	-	0	b:4	c:2	12
TOTALS	200	400	-	7	640	80	1327

a. In the shop
b. Outside not protected from weather
c. " but " by ship structure

J-18

Table J-10
DIRECT LABOR DISTRIBUTION FOR: MACHINERY WORK

Location Function	Steel Fabrication & Related Shops	Steel Assembly Shops & Areas	Departmental Shops	Machinery Assembly Shops	Shipway	Outfitting Wharf	Totals
Burners & Welders					b:1/c:1	c:6	8
Blasters & Painters					c:1	c:3	4
Fitters							
Riggers					b:6/c:2	c:4	12
Other:							
Pipefitters			a:15		b:6/c:22	c:40	83
Electricians			a:4		c:12	c:24	40
Machinists				a:6	b:8/c:4	c:6	24
Sheet Metal Wkrs.			a:1		c:2	c:5	8
TOTALS	-	-	20	6	65	88	179

a. In the shop
b. Outside not protected from weather
c. " but " by ship structure

Table J-11
DIRECT LABOR DISTRIBUTION FOR: OUTFIT WORK

J-20

Location Function	Steel Fabrication & Related Shops	Steel Assembly Shops & Areas	Departmental Shops	Machinery Assembly Shops	Shipway	Outfitting Wharf	Totals
Burners & Welders	a:4	a:8			b:10/c:30	b:18/c:36	106
Blasters & Painters		a:1	a:1		b:3/c:7	b:15/c:15	42
Fitters	a:2	a:6			b:7/c:14	b:11/c:24	64
Riggers		a:1	a:3		b:4/c:8	b:13/c:13	42
Other:							
Pipefitters			a:35		b:8/c:52	b:10/c:30	135
Electricians			a:6		b:1/c:9	b:6/c:62	84
Machinists					b:2	b:4	6
Sheet Metal Wkrs.			a:13		c:4	b:2/c:34	53
TOTALS	6	16	58	-	159	293	532

- a. In the shop
b. Outside not protected from weather
c. " but " by ship structure

APPENDIX K

ANALYSIS OF COSTS FOR THE STANDARD SHIPYARD

COSTS AFFECTED BY LABOR PRODUCTIVITY

Lower labor productivity and lost time can increase shipbuilding costs in several ways (Table K-1). The potential magnitude of these costs for the standard shipyard are described and calculated in this section.

TABLE K-1. Increased Costs Caused by Lost Time or Lower Productivity

- A. Shipyard capacity not fully realized.
 - 1. Land is occupied longer than needed.
 - 2. Building space is occupied longer than needed.
 - 3. Equipment and facilities not used to capacity.
 - 4. Inventory costs for work-in-process are higher.
 - 5. Overhead cost allocated over a reduced production.
 - 6. Extra capacity is required to meet peak operating rates.
- B. Unit labor costs increase.
 - 1. Payments for idle time not worked.
 - 2. Lower output/man-hour.
 - 3. Reject and rework cost.
 - 4. Premium pay for call-in or overtime.

The cost distribution for the standard shipyard was shown in Table J-6 and Table J-8, Appendix J. The total annual costs for the standard shipyard are \$80,210,000. The overhead costs were distributed into material-related, labor-related, related to selling price, and fixed period costs as shown in Tables K-2 and K-3. The costs related to selling price in Table K-3 were redistributed proportionally to the other three. After this redistribution, the percentage breakdown of costs in the model shipyard were: labor-related, 37.4%; material-related, 54.2%; and fixed, 8.4%.

TABLE K-2. Distribution of Indirect and Overhead Costs

<u>Indirect Cost</u>	<u>% of Costs</u>	<u>Nature of Variability</u>
Insurance & Bond Premium, etc.	0.26	Fixed percentage of selling price
Drydocking, etc.	0.79	Fixed percentage of selling price
Misc. Labor, etc.	2.63	1/2 Variable with direct labor cost - 1/2 fixed annual
Sundry Other Items, etc.	1.58	3/4 Fixed annual expense - 1/4 to direct labor
<u>Engineering Costs</u>	2.63	Fixed percentage of selling price
<u>Overhead Costs</u>		
Depreciation, etc.	2.11	Fixed annual expense (varies with capital investment)
Maintenance, etc.	2.11	Fixed annual expense (varies with capital investment)
Wages, etc.	2.63	Fixed percentage of selling price
Supplies, etc.	1.58	Fixed percentage of selling price
Fringe Benefits, etc.	6.32	Variable with direct labor cost
Misc. Other, etc.	1.05	Fixed annual expense
<u>Profit</u>	12.63	Fixed percentage of selling price

K-2

TABLE K-3. Distribution of Annual Costs in the Standard Shipyard

Construction Schedule = 3 ships 1 year			
Expense	One Ship	Three Ships	%
Direct Labor	6,250,000	18,750,000	24
Labor Burden	1,910,000	5,730,000	7
Direct Material	11,875,000	35,600,000	44
Fixed Annual	1,840,000	5,520,000	7
Related to Selling Price	<u>4,870,000</u>	<u>14,610,000</u>	<u>18</u>
	26,675,000	80,210,000	100

Only the labor-related costs, 37.4% of the annual shipyard costs, vary directly with labor productivity. This percentage was used to determine the minimum cost savings achieved through productivity gains. The minimum cost does not include any extra provisions for hiring or training costs. The maximum cost savings are derived from the elimination of overtime premium pay and are calculated at 60% of the annual shipyard costs.

Intermediate cost savings would result from an increase in the production rate of the shipyard. Fixed costs per unit of production would be reduced. Interest expense on working capital would be reduced since the production schedule would be shortened. The calculation below of interest expense on working capital assumes reduction of four months covering 90% of the costs, since a large fraction of the costs, primarily for steel, are committed early in the shipbuilding schedule.

CALCULATIONS OF THE EFFECT OF LABOR PRODUCTIVITY ON SHIPBUILDING COSTS

Costs to regain lost productivity are calculated below for three different assumptions. The typical shipyard experience is probably a mixture of all these cases with some additional cost factors not specifically included here.

Maximum Cost Case

1. If the productivity deficit is made up by overtime - assuming minimum pay of time-and-one-half: then the increased cost to achieve the required output would be 1-1/2 times the straight time labor-related costs, or

$$0.374 \times \frac{1-\text{productivity}}{\text{productivity}} \times 1\frac{1}{2} = 0.561 \times \frac{1-\text{productivity}}{\text{productivity}}$$

Since some premium pay would be at double time, we used 60% for the maximum cost case.

For example, if the average annual productivity in the shipyard was 90% (0.90), then the maximum annual cost for regaining this lost productivity through overtime would be:

$$0.60 \times \frac{1 - 0.90}{0.90} \times \$80,210,000 = \$5,350,000.$$

Minimum Cost Case

2. If the productivity deficit is made up with an increased work force, then the annual increased cost for straight time pay only would be, using the preceding example:

$$0.374 \times \frac{1-\text{productivity}}{\text{productivity}} \times \$80,210,000 = \$3,330,000.$$

Intermediate Cost Case

3. If the productivity deficit results in a longer schedule (reduced capacity), then the annual increased cost would be:

- a) $.084 \times \frac{1 - \text{productivity}}{\text{productivity}}$ (Fixed Cost)
- b) $.90 \times \frac{4}{12} \times 0.12 \times \frac{(1 - \text{productivity})}{\text{productivity}} = .036 \times \frac{1 - p}{p}$ (Interest on Working Capital)

assuming 90% of the costs are committed for four less months at 12% interest on working capital.

- c) $.374 \times \frac{1 - p}{p}$ (Straight Time Labor Cost)
- d) total = $(.084 + .036 + .374)$ or $0.492 \times \frac{1 - p}{p}$

and the total dollar cost using the preceding examples would be:

$$0.492 \times \frac{1 - 0.9}{0.9} \times \$80,210,000 = \$4,390,000$$

APPENDIX L

LISTING OF THE COMPUTER PROGRAM FOR THE SHIPYARD

PRODUCTIVITY MODEL

APPENDIX L

COMPUTER PROGRAM FOR THE SHIPYARD PRODUCTIVITY MODEL

The Program is Written in Fortran V for the UNIVAC 1108.

DEFINITION OF VARIABLES USED IN COMPUTER PROGRAM

PRODET	RELATIVE PRODUCTIVITY FOR EFFECTIVE TEMPERATURE CATEGORIES
PRODAT	RELATIVE PRODUCTIVITY FOR DRY BULB TEMPERATURE CATEGORIES
PRODWS	RELATIVE PRODUCTIVITY FOR WIND CATEGORIES
PRODPR	RELATIVE PRODUCTIVITY FOR PRECIPITATION CATEGORIES
FGP	RELATIVE PRODUCTIVITY FOR FOG CATEGORIES
PRODSH	RELATIVE PRODUCTIVITY FOR SHADE CATEGORIES
RTTIO	RATIO CRAFTSMEN AT OTHER LOCATIONS TO OUTSIDE CRAFTSMEN OR SHOP CRAFTSMEN TO IN-SHIP CRAFTSMEN
RAINPR	FRACTION SHIFT WORKED DURING PRECIPITATION PERIODS
NAM	SHIPYARD LOCATION
DT	DRY BULB TEMPERATURE CATEGORIES
ET	EFFECTIVE TEMPERATURE CATEGORIES
WIND	WIND VELOCITY CATEGORIES
SUN	FRACTION OF SHIFT WITH SUNSHINE
FOG	FRACTION OF SHIFT WITH FOG
PREC	PRECIPITATION CATEGORIES
RH	RELATIVE HUMIDITY CATEGORIES
PT	CORRECTION OF EFFECTIVE TEMPERATURE FOR PAINTERS
EPROD	AVERAGE ANNUAL PRODUCTIVITY FOR EFFECTIVE TEMPERATURE CATEGORIES
APROD	AVERAGE ANNUAL PRODUCTIVITY FOR DRY BULB TEMPERATURE CATEGORIES
WPROD	AVERAGE ANNUAL PRODUCTIVITY FOR WIND CONDITIONS
PRPROD	AVERAGE ANNUAL PRODUCTIVITY FOR PRECIPITATION (RELATIVE HUMIDITY FOR PAINTERS) CONDITIONS
FOGPR	AVERAGE ANNUAL PRODUCTIVITY FOR FOG CONDITIONS
SUNPR	AVERAGE ANNUAL PRODUCTIVITY FOR SUN CONDITIONS
GW	IDEAL WEATHER OUTSIDE
AGW	IDEAL WEATHER IN-SHIP
BGW	EXCESS IDEAL WEATHER IN-SHIP OVER OUTSIDE
TPROD	TOTAL ANNUAL PRODUCTIVITY FOR EACH TEMPERATURE CATEGORY
PCT	DISTRIBUTION OF WORKMEN BETWEEN SHIFTS
ICRAFT	NUMBER OF WORKMEN OF EACH CRAFT AT EACH LOCATION
JCRAFT	NUMBER OF WORKMEN OF EACH CRAFT AT EACH LOCATION ON EACH SHIFT
LCRAFT	FRACTION OF TOTAL WORKMEN ON EACH SHIFT AND LOCATION
ADDER	INCREASE IN PRODUCTIVITY ACHIEVABLE THROUGH TRANSFER OF CRAFTSMEN TO OUTSIDE WORK DURING IDEAL WEATHER
SADDER	INCREASE IN PRODUCTIVITY ACHIEVABLE THROUGH TRANSFER OF SHOP CRAFTSMEN TO IN-SHIP WORK DURING IN-SHIP IDEAL WEATHER (SEE DEFINITION FOR BGW)
SPRD	AVERAGE SHIFT PRODUCTIVITY
TPRD	AVERAGE CRAFT PRODUCTIVITY

APPENDIX L (contd)

YARD	AVERAGE PRODUCTIVITY AT EACH WORK LOCATION
YARDT	AVERAGE ANNUAL SHIPYARD PRODUCTIVITY
TOPAY	VARIABLES ORIGINALLY USED FOR ANNUAL WAGE PAYMENT CALCULATIONS RELATED TO TRANSFER AND PASS OUT CONDITIONS. THIS PART OF THE PROGRAM WAS DISCARDED WHEN THE VARIATION IN WAGE PAYMENTS WAS FOUND TO BE INSIGNIFICANT
ZPAY	
TTPAY	
YDPAY	

LISTING OF THE COMPUTER PROGRAM FOR THE SHIPYARD PRODUCTIVITY MODEL

```

*IT FR5 SHIPS,SHIPS
  DIMENSION PRODET(5,8),PRODAT(5,8),RTTIO(5,3),
1PRODWS(2,5,3),PRODPR(2,5,4),FGP(5),
2PRODSH(2),RAINPR(4),NAM(8),DT(3,8),ET(3,8),WIND(3,3),SUN(3),
3PREC(3,4),RH(3,2),PT(3,4),EPROD(5,3,8),APROD(5,3,8),WPROD(2,5,3),
4PRPROD(2,5,3),FOGPR(5),SUNPR(2,3),GW(3,5),AGW(3,5),BGW(3,5),
5TPROD(3,5,3,8),PCT(3),ICRAFT(5,3),JCRAFT(5,3,3),DCRAFT(5,3,3),
6ADDER(3,5),SADDER(3,5),SPRD(3,5,3),TPRD(3,5),YARD(3),TOPAY(3,5,3)
7,ZPAY(4,5),TTPAY(3,5),YDPAY(3)
  SUN(3)=0.0
  DATA((PRODET(I,J),J=1,8),I=1,5) / .3,.56,.75,.92,1.0,.84,.48,.15,.
175,.51,.7,.92,1.0,.79,.48,.15,.25,.56,.75,.92,1.0,.84,.53,.27,.25,.5
31,.70,.92,1.0,.34,.53,.2,.3,.56,.75,.92,1.0,.84,.53,.2/
  DATA((PRODAT(I,J),J=1,8),I=1,5) / 3*0.0,.7,1.0,.79,.48,.15,.3,.56,.75
1,2*1.0,.74,.43,.1,.3,.56,.75,.9,1.0,.79,.48,.15,.3,.56,.75,.92,1.0,.7
39,.48,.15,.3,.56,.75,.92,1.0,.79,.48,.15/
  DATA PRODWS / 1*1.0,.7,1.0,.8,1.0,.9,1.0,.95,1.0,.0,.8,.1,.8,.15,
1.8,.2,.8,.4,.8/
  DATA PRODPR / 1*1.0,.2*0.0,.8,1.0,.95,1.0,.95,1.0,.95,1.0,.3*0.0,.95,.85,.9
15,.85,.95,.9,.95,3*0.0,.8,.4,.8,.4,.8,.5,.8/
  DATA (FGP(J),J=1,5) / 2*1.0,.2*5.1,/
  DATA (PRODSH(L),L=1,2) / .7,.95/
  DATA(RAINPR(I),I=1,4) / 1.0,1.0,.875,.875 /
205 FORMAT (16F5.0)
206 FORMAT (12F10.3)
207 FORMAT (8A6,32X)
  3 READ 200,(NAM(I),I=1,8)
  PRINT 200,(NAM(I),I=1,8)
  IL=-1
  DO 20 I=1,3
  READ 205,(DT(I,J),J=1,8)
  IF (DT(I,5) .LT. .001) GO TO 999
  PRINT 206,(DT(I,J),J=1,8)
  READ 205,(ET(I,J),J=1,8)
  PRINT 206,(ET(I,J),J=1,8)
  READ 205,((WIND(I,J),J=1,3),(PREC(I,J),J=1,4),(RH(I,J),J=1,2))
  PRINT 206,((WIND(I,J),J=1,3),(PREC(I,J),J=1,4),(RH(I,J),J=1,2))
  READ 205,(PT(I,J),J=1,4)
  PRINT 206,(PT(I,J),J=1,4)
  IF (I.GT.1) GO TO 20
  READ 205, SUN(1),SUN(2),FOG
  PRINT 206, SUN(1),SUN(2),FOG
20 CONTINUE
21 CONTINUE
  IF(IL.GE.0) PRINT 847
847 FORMAT (' THIS MODEL DOES NOT PERMIT TRANSFER BETWEEN LOCATIONS')
C TEMPERATURE PRODUCTIVITY CALCULATIONS
DO 52 L=1,2
DO 50 J=1,5

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DO 40 K=1,3
WPROD(L,J,K)=0.
PRPROD(L,J,K)=0.
CHECK=RH(K,1)+RH(K,2)
IF (CHECK.GT.1.01.OR.CHECK.LT..99)PRINT 803,K,K,K
CHECK=0.
CHECL=0.
DO 30 I=1,8
PC=0.
CHECK=CHECK+ET(K,I)
CHECL=CHECL+DT(K,I)
IF (J.EQ.1.AND.I.LE.4)PC=PT(K,I)
FPROD(J,K,I)=PRODET(J,I)*(ET(K,I)-PC)
APROD(J,K,I)=PRCDAT(J,I)*DT(K,I)
30 CONTINUE
210 FORMAT (3I5,2F10.3)
IF (CHECK.GT.1.01.OR.CHECK.LT..99)PRINT 803,L,J,K
IF (CHECL.GT.1.01.OR.CHECL.LT..99)PRINT 803,L,J,K
803 FORMAT (' ERROR IN SUM CHECK' 3I5)
CHECK=0.
CHECL=0.
C WIND PRODUCTIVITY CALCULATIONS
DO 35 I=1,3
CHECK=CHECK+WIND(K,I)
35 WPROD(L,J,K)=WPROD(L,J,K)+(PRODWS(L,J,I)*WIND(K,I))
IF (CHECK.GT.1.01.OR.CHECK.LT..99)PRINT 803,L,J,K
C PRECIPITATION AND HUMIDITY PRODUCTIVITY CALCULATIONS
IF (J.EQ.1) GO TO 41
DO 36 I=1,4
CHECL=CHECL+PREC(K,I)
IF (PRODPR(L,J,I).EQ..0) GO TO 37
PRPROD(L,J,K)=PRPROD(L,J,K)+PREC(K,I)*PRODPR(L,J,I)*RAINPR(I)
GO TO 39
37 PRPROD(L,J,K)=PRPROD(L,J,K)+PREC(K,I)*.075
39 CONTINUE
36 CONTINUE
IF (CHECL.GT.1.01.OR.CHECL.LT..99)PRINT 803,L,J,K
GO TO 42
41 PRPROD(L,J,K)=PRPROD(L,J,K)+(1.*RH(K,1)+RH(K,2)*.075)
42 CONTINUE
C IDEAL WEATHER OUTSIDE
GW(K,J)=ET(K,5)*WIND(K,1)*PREC(K,1)
IF (J.EQ.1)GW(K,J)=GW(K,J)*RH(K,1)/PREC(K,1)
IF (J.EQ.3.OR.J.EQ.4) GW(K,J)=GW(K,J)*(1-FOG)
C FOG AND SHADE EFFECTS
SUNPR(L,K)=1.00*(1-SUN(K))+PRODSH(L)*SUN(K)
C IDEAL WEATHER IN SHIP
AGW(K,J)=DT(K,5)*(WIND(K,1)+WIND(K,2))*(PREC(K,1)+PREC(K,2))
IF (J.EQ.1) AGW(K,J)=AGW(K,J)*RH(K,1)/(PREC(K,1)+PREC(K,2))
IF (J.EQ.3.OR.J.EQ.4) AGW(K,J)=AGW(K,J)*(1-FOG)

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      AGW(K,J)=AGW(K,J)-GW(K,J)
40  CONTINUE
      FOGPR(J)=1.00*(1-FOG)+FGP(J)*FOG
50  CONTINUE
52  CONTINUE
C    TOTAL PRODUCTIVITY CALCULATIONS
      DATA (PCT (K) , K = 1,3) / . 65, . 30, . 05/
      KTOTAL = 2738
      DATA ((ICRAFT (J,L), J = 1,5), L = 1,3) / 60, 227,
161, 237, 57, 39, 272, 58, 229, 308, 7, 156,
243, 204, 87
      DO 90 L = 1,3
      DO 90 J = 1,5
      ZPAY(L,J)=0.
      TPRD(L,J)=0.
      DO 90 K = 1,3
      DO 89 I=1,8
      SC=1.
      IF (I.GE.6) SC=SUNPR(L,K)
      IF (L.EQ.2) GO TO 80
      IF (L.EQ.3) GO TO 82
C    OUTSIDE PRODUCTIVITY
      TPROD (L,J,K,I) = FPROD (J,K,I) * WPROD (L,J,K) * PRPROD (L,J,K)
1*FOGPR(J)*SC
      GO TO 88
C    INSIDE PRODUCTIVITY
80  CONTINUE
      TPROD (L,J,K,I) = APROD (J,K,I) * WPROD (L,J,K) * PRPROD (L,J,K) *
1*FOGPR(J)*SC
      GO TO 88
82  TPROD (L,J,K,I)=1.*DT(K,I)
88  CONTINUE
      CTOT=CTOT+TPROD(L,J,K,I)
89  CONTINUE
      PRINT 12,CTOT,L,J,K
      CTOT=0.
12  FORMAT (' TOTAL PRODUCTIVITY IS'F7.3,' AT LOCATION' I3,' FOR CRAFT'
1I3,' AND SHIFT' I3)
C    DISTRIBUTION OF WORKERS
      JCRAFT (J,L,K) = ICRAFT (J,L) * PCT (K) + .5
      DCRAFT (J,L,K) =FLOAT( JCRAFT (J,L,K))/ FLOAT(KTOTAL)
90  CONTINUE
C    IDEAL WEATHER ADDER
      DO 111 J = 1,5
      RTTIO (J,2) =FLOAT(ICRAFT(J,3))/FLOAT(ICRAFT(J,2) )
111 RTTIO (J,1) =FLOAT(I CRAFT (J, 2) + I CRAFT (J,3))/ FLOAT(ICRAFT (
1J,1))
      YARDT=0.
      DO 188 LY= 1,3
      L=LY

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YARD(L)=0.
YDPAY(L)=0.
DO 187 J = 1,5
  TTPAY(L,J)=0.
DO 186 K = 1,3
  SPRD(L,J,K)=0.
  IF (L.GE.2) GO TO 183
C THIS STATEMENT PROHIBITS TRANSFERS BETWEEN LOCATIONS
  IF (L.GE.0) GO TO 183
  DO 128 I=1,8
  IF (J.GT.1) GO TO 127
  PAINT = RH (K,2) * (.7*(ICRAFT(J,1)+ICRAFT(J,2)))/ICRAFT(J,3)
  TPROD (3,1,K,I) = TPROD (3,1,K,I)*(1+ PAINT )
127 CONTINUE
  IF (J.NE.2) GO TO 128
  WELD = (PREC(K,3) + PREC(K,4))*(.7*ICRAFT(J,1))/ICRAFT(J,2)
  TPROD (2,2,K,I) = TPROD (2,2,K,I)*(1+WELD)
128 CONTINUE
  ADDER (K, J) = GW (K, J) * (RTTIO (J,1))
  TPROD (1,J,K,5) = TPROD (1,J,K,5) +ADDER (K,J)
  TPROD (2,J,K,5) = TPROD (2,J,K,5)-GW(K,J)
  TPROD (3,J,K,5) = TPROD (3,J,K,5)-GW(K,J)
C IN SHIP ADDER
  SADDER (K,J) = BGW (K,J) * ( RTTIO (J,2))
  TPROD (2,J,K,5) = TPROD (2,J,K,5) + SADDER (K,J)
  TPROD (3,J,K,5) = TPROD (3,J,K,5) - BGW (K,J)
183 CONTINUE
DO 185 I = 1,8
185 SPRD (L,J,K) = SPRD (L,J,K) + TPROD (L,J,K,I)
PRINT 313, L, J, K, SPRD (L,J,K)
313 FORMAT ( ' TOTAL SHIFT PRODUCTIVITY' 315, F 10.3)
186 TPRD (L,J) = TPRD (L,J) + SPRD (L,J,K)*PCT(K)
  IF (TPRD(L,J).GT.1) GO TO 273
  GO TO 274
273 XY=TPRD(L,J)-1.
  ZPAY(L,J)=ZPAY(L,J)-XY
  LL=L+1
  IF (LL.EQ.4) LL=1
  IF (TPRD(LL,J).EQ.1.) LL=LL+1
  PY=(XY*ICRAFT(J,L))/ICRAFT(J,LL)
  ZPAY(LL,J)=ZPAY(LL,J)+PY
  TPRD(L,J)=1.
  TPRD(LL,J)=TPRD(LL,J)+PY
  PRINT 917,XY,L,LL,PY
917 FORMAT (F7.3,'EXCESS PRODUCTIVITY TRANSFERRED FROM LOCATION'13,'
EQUIVALENT PRODUCTIVITY GAIN AT'13,' IS'F7.3)
  IF (TPRD(LL,J).LE.1.) GO TO 274
  XY=TPRD(LL,J)-1.
  ZPAY(LL,J)=ZPAY(LL,J)-XY

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      TPRD(LL,J)=1.
      LO=LL+1
      IF (LO.EQ.4) LO=1
      PY=(XY*ICRAFT(J,LL))/ICRAFT(J,LO)
      TPRD(LO,J)=TPRD(LO,J)+PY
      ZPAY(LO,J)=ZPAY(LO,J)+PY
      PRINT 917,XY,LL,LO,PY
274  CONTINUE
      PRINT 314, L, J, TPRD (L,J)
314  FORMAT (' CRAFT PRODUCTIVITY: 215 , F10.3)
187  YARD (L) = YARD (L) +(TPRD (L,J) *ICRAFT(J,L))/KTOTAL
      PRINT 315, L, YARD (L)
315  FORMAT (' LOCATION' 15, F10.3)
188  YARDT = YARDT + YARD (L)
      PRINT 316, YARDT, (NAM (I), I = 1,8)
316  FORMAT (' YARD PRODUCTIVITY', F 10.3, 5X, 8A6)
      RX=1.-YARDT
      CX=BX/YARDT
      DX=.374*CX
      PRINT 319,DX
319  FORMAT (' EXCESS STRAIGHT TIME LABOR COST',F6.3)
      IL=IL+1
      IF (IL.GE.7) GO TO 599
      IF (IL.EQ.0) GO TO 21
      GO TO (591,593,594,592,601,611),IL
591  PRODSH(1)=1.
      PRODSH(2)=1.
      PRINT 595
595  FORMAT (' PRODUCTIVITY WITH SHADE PROVIDED')
      GO TO 21
592  DO 757 L=1,2
      DO 757 J=1,5
      DO 757 K=1,3
      PRODWS(L,J,K)=1.
757  CONTINUE
      PRODET(1,1)=0.
      PRODET(1,2)=0.
      PRODET(1,3)=0.
      PRODET(1,4)=.7
      DO 609 K=1,3
      DO 609 I=1,8
      IF (I.LE.4) PT(K,I)=0.
609  FT(K,I)=DT(K,I)
      PRINT 596
596  FORMAT (' PRODUCTIVITY WITH WIND PROTECTION')
      GO TO 21
593  DO 758 L=1,2
      DO 758 J=1,5
      DO 758 K=1,4

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      PRODP(R(L,J,K))=1.
758  CONTINUE
      RAINPR(3)=1.
      DRAINPR(4)=1.
      PRINT 597
597  FORMAT (' PRODUCTIVITY WITH RAIN PROTECTION')
      GO TO 21
594  CONTINUE
      DO 602 K=1,3
      RH(K,1)=1.
602  PH(K,2)=0.
      PRINT 598
598  FORMAT (' PRODUCTIVITY WITH DEHUMIDIFIERS')
      GO TO 21
601  DO 604 J=1,5
      DO 604 I=6,8
      PRODET(J,I)=1.
604  PRODAT(J,I)=1.
      PRINT 606
606  FORMAT (' PRODUCTIVITY WITH COOLING PROVIDED')
      GO TO 21
611  DO 613 J=1,5
      DO 613 I=1,4
      PRODET(J,I)=1.
      PRODAT(J,I)=1.
613  CONTINUE
      PRINT 615
615  FORMAT (' PRODUCTIVITY WITH HEATING PROVIDED')
      GO TO 21
599  CONTINUE
      GO TO 3
999  CONTINUE
      STOP
      END
* XOT SHIPS
  SAN DIEGO
    .0 .0 .0 .001 .963 .033 .003 .0
    .0 .0 .0 .018 .946 .033 .003 .0
.8638.1350.0025 .983 .006 .007 .004.9862.0138
    .0 .0 .0 .0
.6765.2750 .01
    .0 .0 .0 .0 .986 .013 .0 .0
    .0 .0 .0 .016 .971 .013 .0 .0
.9638.0350.0013 .981 .006 .010 .003.9512.0488
    .0 .0 .0 .0
    .0 .0 .0 .0 .991 .008 .0 .0
    .0 .0 .001 .018 .973 .008 .0 .0
.9800.0200.0013 .975 .009 .013 .003.8275.1725
    .0 .0 .0 .0

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XQT SHIPS
 PHILADFLPHIA
 .0 .021 .070 .167 .629 .097 .017 .000
 .019 .105 .144 .150 .473 .093 .016 .000
 .6188.3613.0175 .935 .018 .036 .011.9062.0938
 .019 .079 .052 .012
 .4275.1925 .01
 .0 .017 .064 .172 .659 .077 .011 .0
 .016 .096 .150 .158 .493 .077 .011 .0
 .7425.7475.0100 .929 .020 .037 .014.8800.1200
 .016 .073 .055 .015
 .0 .013 .048 .171 .719 .046 .004 .0
 .011 .071 .145 .168 .555 .046 .004 .0
 .8188.1788.0063 .923 .020 .039 .018.7137.2863
 .011 .050 .053 .019

END
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